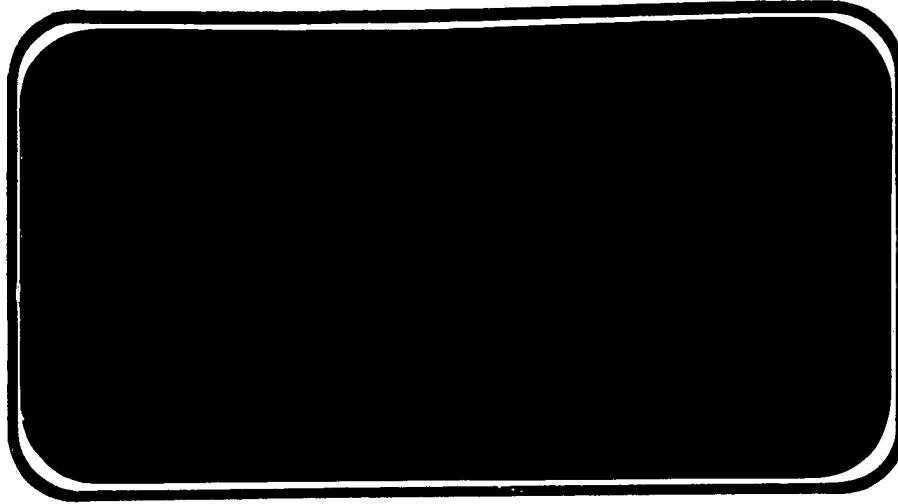


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(NASA-CR-128754) HYPERSONIC AERODYNAMIC
CHARACTERISTICS OF NR-ATP ORBITER, ORBITER
WITH EXTERNAL TANK, AND ASCENT
CONFIGURATION (Chrysler Corp.) 123 p HC
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SPACE SHUTTLE

AEROTHERMODYNAMIC DATA REPORT

MANNED SPACECRAFT CENTER

HOUSTON, TEXAS

DATA MANAGEMENT SERVICES

SPACE DIVISION  CHRYSLER
CORPORATION

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HYPersonic AERODYNAMIC CHARACTERISTICS
OF NR-ATP ORBITER, ORBITER WITH
EXTERNAL TANK, AND ASCENT CONFIGURATION

By

George C. Ashby, Jr., NASA/LaRC

Prepared under NASA Contract Number NAS9-13247

by

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New Orleans, La. 70189

for

Aerodynamics Section
Flight Technology Branch
Engineering Analysis Division

Manned Spacecraft Center
National Aeronautics and Space Administration
Houston, Texas

WIND TUNNEL TEST SPECIFICS

Test Number: LaRC 22"-409
NASA Series No.: MA2
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HYPersonic AERODYNAMIC CHARACTERISTICS
OF NR-ATP ORBITER, ORBITER WITH
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ABSTRACT

A .0045 scale model of the North American Rockwell ATP Orbiter with and without the external tank has been tested in the Langley 22-Inch Helium Tunnel at Mach 20 and a Reynolds number based on model length, of 2.14×10^6 . Longitudinal and lateral-directional data were determined for the orbiter alone while only longitudinal characteristics and elevon roll effectiveness were investigated for the orbiter/tank combination. Oil flow and electron beam flow visualization studies were conducted for the orbiter alone, orbiter with external tank and the ascent configuration.

TABLE OF CONTENTS

	PAGE
ABSTRACT	iii
INDEX OF MODEL FIGURES	2
INDEX OF DATA FIGURES	5
NOMENCLATURE	6
SUMMARY	10
CONFIGURATIONS INVESTIGATED	12
TEST FACILITY DESCRIPTION	13
TEST CONDITIONS	14
DATA REDUCTION	14
REFERENCES	16
TABLES	
I DATA SET COLLATIONS	17
II MODEL COMPONENT DIMENSIONS	18
FIGURES	
MODEL	29
DATA	87
APPENDIX - TABULATED SOURCE DATA	

INDEX OF MODEL FIGURES

<u>FIGURE</u>	<u>TITLE</u>	<u>PAGE</u>
1	North American Rockwell Baseline (.0045 scale) Delta-Wing Orbiter (ATP) with .0047 Scale Wing Superimposed	30
2	NR-ATP Baseline Orbiter with External Tank	31
3	SRB General Arrangement	32
4	Photograph of .0045 Scale NR (ATP) Orbiter Configuration: A) Left Side View B) Top View C) Bottom View D) Rear Oblique View	33 34 35 36
5	Photograph of .0045 Scale NR (ATP) Orbiter with External Tank Configuration A) Left Side View B) Top View C) Bottom View D) Rear Oblique View	37 38 39 40
6	Photograph of .0045 Scale NR (ATP) Ascent Configuration A) Left Side View B) Top View C) Bottom View D) Rear Oblique View	41 42 43 44
7	Photograph of Oil Flow Pattern after Tunnel Shutdown on the .0045 Scale NR (ATP) Orbiter @ $M = 20.3$ and $\alpha = 51^\circ$, $\delta_e = 0^\circ$ A) Left Side View B) Top View C) Bottom View	45 46 47
8	Photograph of Oil Flow Pattern after Tunnel Shutdown on the .0045 Scale NR (ATP) Orbiter @ $M = 20.3$ and $\alpha = 51^\circ$, $\delta_e = -40^\circ$ A) Right Side View B) Bottom View C) Right Side Rear Oblique View	48 49 50
9	Photograph of Oil Flow Pattern after Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank @ $M = 20.3$ and $\alpha = 0^\circ$ A) Side View B) Top View	51 52

INDEX TO MODEL FIGURES (Continued)

<u>FIGURE</u>	<u>TITLE</u>	<u>PAGE</u>
9 (Continued)	C) Bottom View D) Oblique Front Side View E) Oblique Top Side View	53 54 55
10	Photograph of Oil Flow Pattern after Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank @ $M = 20.3$ and $\alpha = -5^\circ$ A) Side View (Rolled) B) Top View C) Bottom View D) Front Oblique View E) Top-Side Oblique View F) Top Oblique View	56 57 58 59 60 61
11	Photograph of Oil Flow Pattern after Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = +5^\circ$ A) Side View B) Side View (Rolled) C) Top View D) Bottom View E) Front-Lower Surface View F) Top Oblique View	62 63 64 65 66 67
12	Photograph of Oil Flow Pattern after Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration @ $M = 20.3$ and $\alpha = 0^\circ$ A) Left Side View B) Top View C) Bottom View D) Front Oblique View	68 69 70 71
13	Photograph of Oil Flow Pattern after Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration @ $M = 20.3$ and $\alpha = -5^\circ$ A) Left Side View (Rolled) B) Top View C) Bottom View D) Front Oblique View	72 73 74 75
14	Photograph of Oil Flow Pattern after Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$ and $\alpha = +5^\circ$ A) Left Side View B) Left Side View (Rolled)	76 77

INDEX TO MODEL FIGURES (Continued)

<u>FIGURE</u>	<u>TITLE</u>	<u>PAGE</u>
14 (Continued)	C) Top View D) Top View Close-up E) Bottom View F) Front Oblique View	78 79 80 81
15	Photograph of Electron Beam Illuminated Oil Flow Pattern on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = 0^\circ$	82
16	Photograph of Electron Beam Illuminated Oil Flow Pattern on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = -5^\circ$	83
17	Photograph of Electron Beam Illuminated Oil Flow Pattern on a .0045 Scale NR (ATP) Ascent Configuration @ $M = 20.3, \alpha = +5^\circ$	84
18	Photograph of Electron Beam Illuminated Oil Flow Pattern on a .0045 Scale NR (ATP) Ascent Configuration @ $M = 20.3, \alpha = -5^\circ$	85
19	Axis System	86

INDEX TO DATA FIGURES

<u>TITLE</u>	<u>COEFFICIENT SCHEDULE</u>	<u>PAGE</u>
Effect of Elevator Deflection on Longitudinal Characteristics of Baseline Orbiter	A	1-4
Lateral-Directional Characteristics of Baseline Orbiter	B	5
Effect of External Tank on Orbiter Longitudinal Characteristics	A	6-9
Aileron Effectiveness for Orbiter with External Tank	C	10
Effect of Aileron Deflection on Longitudinal Characteristics of Modified Orbiter	A	11-14
Effect of Body Flap on Longitudinal Characteristics of Modified Orbiter	A	15-18

COEFFICIENT SCHEDULES:

- A) CN, CL, CDF, L/DF, CAF vs ALPHA: CN, CL vs CLM; CDF vs CL
- B) DCY/DB, DCYNDB, DCBLDB vs ALPHA
- C) DCY/DA, DCYNDA, DCBLDA vs ALPHA

NOMENCLATURE
General

<u>SYMBOL</u>	<u>SADSAC SYMBOL</u>	<u>DEFINITION</u>
a		speed of sound; m/sec, ft/sec
C_p	CP	pressure coefficient; $(p_1 - p_\infty)/q$
M	MACH	Mach number; V/a
p		pressure; N/m ² , psf
q	Q(NSM) Q(PSF)	dynamic pressure; $1/2\rho V^2$, N/m ² , psf
RN/L	RN/L	unit Reynolds number; per m, per ft
V		velocity; m/sec, ft/sec
α	ALPHA	angle of attack, degrees
β	BETA	angle of sideslip, degrees
ψ	PSI	angle of yaw, degrees
ϕ	PHI	angle of roll, degrees
ρ		mass density; kg/m ³ , slugs/ft ³

Reference & C.G. Definitions

A _b		base area; m ² , ft ²
b	BREF	wing span or reference span; m, ft
c.g.		center of gravity
$\frac{l}{c}$ _{REF}	LREF	reference length or wing mean aerodynamic chord; m, ft
S	SREF	wing area or reference area; m ² , ft ²
	MRP	moment reference point
	XMRP	moment reference point on X axis
	YMRP	moment reference point on Y axis
	ZMRP	moment reference point on Z axis

SUBSCRIPTS

b	base
l	local
s	static conditions
t	total conditions
∞	free stream

NOMENCLATURE (Continued)

Body-Axis System

<u>SYMBOL</u>	<u>SADSAC SYMBOL</u>	<u>DEFINITION</u>
C_N	CN	normal-force coefficient; $\frac{\text{normal force}}{qS}$
C_A	CA	axial-force coefficient; $\frac{\text{axial force}}{qS}$
C_Y	CY	side-force coefficient; $\frac{\text{side force}}{qS}$
C_{A_b}	CAB	base-force coefficient; $\frac{\text{base force}}{qS}$ $-A_b(p_b - p_\infty)/qS$
C_{A_f}	CAF	forebody axial force coefficient, $C_A - C_{A_b}$
C_m	CIM	pitching-moment coefficient; $\frac{\text{pitching moment}}{qS\ell_{\text{REF}}}$
C_n	CYN	yawing-moment coefficient; $\frac{\text{yawing moment}}{qSb}$
C_l	CBL	rolling-moment coefficient; $\frac{\text{rolling moment}}{qSb}$

Stability-Axis System

C_L	CL	lift coefficient; $\frac{\text{lift}}{qS}$
C_D	CD	drag coefficient; $\frac{\text{drag}}{qS}$
C_{D_b}	CDB	base-drag coefficient; $\frac{\text{base drag}}{qS}$
C_{D_f}	CDF	forebody drag coefficient; $C_D - C_{D_b}$
C_Y	CY	side-force coefficient; $\frac{\text{side force}}{qS}$
C_m	CIM	pitching-moment coefficient; $\frac{\text{pitching moment}}{qS\ell_{\text{REF}}}$
C_n	CLN	yawing-moment coefficient; $\frac{\text{yawing moment}}{qSb}$
C_l	CSL	rolling-moment coefficient; $\frac{\text{rolling moment}}{qSb}$
L/D	L/D	lift-to-drag ratio; C_L/C_D
L/D_f	L/DF	lift to forebody drag ratio; C_L/C_{D_f}

NOMENCLATURE (Continued)

ADDITIONS TO STANDARD LIST

<u>SYMBOL</u>	<u>PLOT SYMBOL</u>	<u>DEFINITION</u>
$C_{Y\beta}$	DCY/DB	side force coefficient derivative with respect to beta. Algebraic difference of the side force coefficient of two runs divided by the algebraic difference of the side slip angle of the runs; per degree.
$C_{n\beta}$	DCYNDB	yawing moment coefficient derivative with respect to beta. Algebraic difference of the yawing moment coefficient of two runs divided by the algebraic difference of the side slip angle of the runs; body axis system; per degree.
$C_{\lambda\beta}$	DCBLDB	rolling moment coefficient derivative with respect to beta. Algebraic difference of the rolling moment coefficient of two runs divided by the algebraic difference of the side slip angle of the runs; body axis system; per degree.
$C_{Y\delta_a}$	DCY/DA	side force coefficient derivative with respect to total aileron deflection. Algebraic difference of the side force coefficients of two runs divided by the algebraic difference of the total aileron deflection angle of the runs; per degree.
$C_{n\delta_a}$	DCYNDA	yawing moment coefficient derivative with respect to total aileron deflection. Algebraic difference of the yawing moment coefficient of two runs divided by the algebraic difference of the total aileron deflection angle of the runs; body axis system, per degree.
$C_{\lambda\delta_a}$	DCBLDA	rolling moment coefficient derivative with respect to total aileron deflection. Algebraic difference of the rolling moment coefficient of two runs divided by the algebraic difference of the total aileron deflection angle of the runs; body axis system; per degree.
δ_e	ELEVTR	elevator deflection, degrees; determined by: $(\delta_{eL} + \delta_{eR})/2$
δ_a	AILRON	aileron deflection, degrees; determined by: $(\delta_{eL} - \delta_{eR})/2$

NOMENCLATURE (Concluded)

ADDITIONS TO STANDARD LIST

<u>SYMBOL</u>	<u>PLOT SYMBOL</u>	<u>DEFINITION</u>
δ_r	RUDDER	rudder deflection angle, degrees; positive direction trailing edge left.
δ_{BF}	BDFLAP	body flap deflection, degrees; positive direction trailing edge down.
δ_{eL}	ELVN-L	left elevon deflection, degrees; positive direction trailing edge down.
δ_{eR}	ELVN-R	right elevon deflection, degrees; positive direction trailing edge down.
$\Delta\beta$	DLTBTA	incremental difference in sideslip angle between two test runs; degrees.
$\Delta\delta_a$	DLTALN	incremental difference in aileron deflection angle between two test runs; degrees.

HYPersonic AERODYNAMIC CHARACTERISTICS
OF NR-ATP ORBITER, ORBITER WITH
EXTERNAL TANK, AND ASCENT CONFIGURATION

By

George C. Ashby, Jr.

SUMMARY

A .0045 scale model of the North American Rockwell ATP orbiter with and without the external tank has been tested in the Langley 22-inch helium tunnel at Mach 20 and a Reynolds number based on model length, of 2.14×10^6 . Six component aerodynamic force and moment data were recorded over an angle of attack range from -1.5° to 54° for the orbiter alone and $\pm 15^\circ$ for the orbiter/tank configuration. Both longitudinal and lateral-directional data were determined for the orbiter alone. For the orbiter/tank combination only the longitudinal characteristics and elevon roll effectiveness were investigated.

Additionally, oil flow and electron beam flow visualization studies were conducted on the orbiter alone, orbiter with external tank, and orbiter with external tank and solid rocket boosters (ascent configuration).

The orbiter attains the design L/D of 1.32 at $\alpha = 34^\circ$; however, it has nearly neutral stability at trim and requires an entry c.g. somewhat rearward of design (65% λ) for minimum up elevon/maximum C_L at trim. A slight pitchup occurs for up elevons ($\delta_e = -20^\circ$ and -40°) beyond angles of attack of about 45° . Reference 1 shows a similar result for a delta

wing with a full span trailing-edge flap at $M = 6.8$ and $\alpha = 50^\circ$ to 55° in air. A companion publication of reference 1, reference 2, shows the effects to be caused by flow overexpansion on the flap. It should be noted, however, that the 5° angle of attack difference between the angle where the pitchup occurs at $M = 6.83$ in air (reference 1) and $M = 20$ in helium is also the difference in conical shock detachment angle for the two cases.

The directional instability ($-C_n$) and positive dihedral effect ($-C_{\ell\beta}$) observed in this test are similar to the results obtained for other delta-wing orbiter designs.

The orbiter-external tank combination data are referenced to the orbiter geometric parameters and can be somewhat misleading. For instance, the instability of the combination about the orbiter c.g. is reduced when the tank fuel c.g. is taken into account. It is interesting to note that the orbiter and orbiter/tank combination have the same level of normal force from $\alpha = 0^\circ$ to 12° . The roll control of the orbiter elevon for the orbiter/tank combination was determined for the setting, $\delta_{eL} = 0^\circ$ and $\delta_{eR} = -40^\circ$; it shows a proverse yawing moment which is equal to or greater than 50 percent of the rolling moment.

The orbiter was originally tested with a .0047 scale wing on the .0045 body. Comparison of the data to that of the .0045 wing/body with both reduced on the smaller wing geometric parameters, showed only the lift and drag values to be significantly different. The L/D and trim characteristics were approximately the same. Because of these similarities, roll effectiveness and the effect of body flap deflection were not

obtained for the .0045 wing/body. Those data obtained for the .0047 wing/.0045 body are presented herein based on .0045 wing geometric parameters.

CONFIGURATIONS INVESTIGATED

These tests utilized a .0045 scale model of the NR-ATP space shuttle orbiter, external tank and solid rocket boosters. Force tests were conducted on the orbiter alone (figure 1) and on the orbiter with external tank (figure 2). Several initial investigations, aileron effectiveness and body flap deflection tests, were made with a .0047 scale model wing on a .0045 scale model body (figure 1).

The oil flow and electron beam flow visualization studies were conducted on the .0045 scale model orbiter alone (figure 4), orbiter with external tank (figure 5) and orbiter with external tank and solid rocket boosters (ascent configuration, figure 6).

Orbiter dimensions were obtained from NR lines drawing VL70-000001 while external tank and solid rocket booster lines and assembly locations were scaled from NR sketch 102SSV319.

The model components tested are listed below. Pertinent dimensional information for these components is given in table II. Table I delineates the various configurations these components were tested in during this investigation.

ORBITER:

B₁ - basic ATP fuselage

C₁ - canopy

D₁ - manipulator arm housing
F₁ - body flap
M₁ - orbital maneuvering system pod
W₁ - basic delta wing (.0045 scale)
W_{1X} - basic delta wing (.0047 scale)
E₁ - full span elevons for W₁
V₁ - basic fuselage centerline mounted vertical tail
K₁ - cooling air inlet
R₁ - rudder for vertical tail V₁

External tank:

T₁ - orbiter external fuel tank

Solid rocket booster:

S₁ - two 156 inch diameter solid rocket boosters attached to
the external tank

TEST FACILITY DESCRIPTION

The LaRC 22-inch helium tunnel is a blowdown-type tunnel with a normal operational time of 30 seconds for aerodynamic force and moment tests. Studies are conducted in the 22-inch diameter test section at Mach numbers from 19 to 22.2 at stagnation pressures from 500 to 3000 psi, and at stagnation temperatures from 520° to 960°R. These test conditions allow Reynolds number variations from 2.5×10^6 to 11.5×10^6 per foot. Operational characteristics of the contoured nozzle flow characteristics are available in reference 3.

TEST CONDITIONS

For this report, all tests were conducted at a stagnation pressure of 1000 psi gage and at a stagnation temperature of 85°F. These test conditions resulted in a Mach number of 20.3 and a Reynolds number of 2.14×10^6 based on model length (5.977 in.)

The technique used for the surface oil-flow studies was to splatter a mixture of lamp black and silicone oil onto a light colored model that had been initially coated with a thin film of clear silicone oil. Simultaneous photographs of the oil-flow patterns and the electron-beam illuminated flow field were then made during a run. Additional photographs of the oil-flow patterns were taken after the models were removed from the tunnel. Although a model shield device was used, these patterns were subjected to flow shut-down disturbances. These disturbances have been observed to be small, but they can cause a slight rearward movement in heavy oil accumulation regions such as along separation lines.

DATA REDUCTION

The aerodynamic forces and moments have been reduced to coefficients by using the following reference values:

$$S_{ref} = \text{total or theoretical wing projected area} = 60.58 \text{ cm}^2 = .06524 \text{ ft}^2$$

$$l_{ref} = \text{wing MAC} = 5.9436 \text{ cm} = 2.34 \text{ in.}$$

$$b_{ref} = \text{wing span (projected)} = 11.52 \text{ cm} = 4.535 \text{ in.}$$

The moments have been reduced about a center of gravity located at a fuselage station which is .65 body length.

The angles of attack, -1.5° to 54° , were measured by an optical method using a prism mounted in the model to reflect light from a point (located adjacent to the test-section window) onto electric eyes set at calibrated intervals. Sideslip angles tested were 0° , -2.25° and -4.47° .

All axial force and drag data have been corrected for base pressure. The measured base pressures are unavailable for this report. All data calculations and axis system conversions used the corrected values of axial force and drag.

REFERENCES

1. Fetterman, David E., and Neal, Luther Jr.: An Analysis of the Delta-Wing Hypersonic Stability and Control Behavior at Angles of Attack Between 30° and 90°. NASA TN D-1602, March 1963.
2. Neal, Luther Jr., and Fetterman, David E.: Control-Surface Interaction Effects on Delta-Wing Windward Pressure at a Mach Number of 6.83 at High Angles of Attack. NASA TN D-2332, June 1964.
3. Arrington, James P., Joiner, Roy C., Jr., and Henderson, Arthur, Jr.: Longitudinal Characteristics of Several Configurations at Hypersonic Mach Numbers in Conical and Contoured Nozzles. NASA TN D-2489, 1964.

TABLE I.
TEST 22⁶He - 409 DATA SET COLLATION SHEET

PRETEST

~~POSTTEST~~

1 7 13 19 25 31 37 43 49 55 61 67 75 76

COEFFICIENTS:

a or β
SCHEDULES

A) $18^\circ \rightarrow 54^\circ$, $\Delta\alpha = 3^\circ$ D) $18^\circ \rightarrow 33^\circ$
 B) $-1.5^\circ \rightarrow 26^\circ$ E) $-15^\circ \rightarrow 12^\circ$
 C) $-1.5^\circ \rightarrow 18^\circ$ F) $-15^\circ \rightarrow 15^\circ$

→ IDPVAR(1) IDPVAR(2) NDV

TABLE II. MODEL DIMENSIONAL DATA

MODEL COMPONENT : BODY - Bl

GENERAL DESCRIPTION : Basic Delta Wing Fuselage per NAR Lines,

Dwg. VL70-000001

Model Scale = .0045

DRAWING NUMBER : VL000001

DIMENSIONS :	FULL SCALE	MODEL SCALE
Length	<u>1328.33</u>	<u>5.977</u>
Max Width	<u>237.96</u>	<u>1.0708</u>
Max Depth	<u>238.00</u>	<u>1.0710</u>
Fineness Ratio	<u>5.527</u>	<u>.0249</u>
Area		
Max. Cross-Sectional	<u>326.0</u>	<u>.0066</u>
Planform	<u>--</u>	<u>--</u>
Wetted	<u>--</u>	<u>--</u>
Base	<u>--</u>	<u>--</u>

MODEL DIMENSIONAL DATA

MODEL COMPONENT : BODY - CANOPY - C1

GENERAL DESCRIPTION : Canopy used with Basic Delta Wing Fuselage per
NAR Lines, Dwg. VL70-000001

Model Scale = .0045

DRAWING NUMBER : VL70-000001

DIMENSIONS :	FULL SCALE	MODEL SCALE
STA Fwd Bulkhead - in.	<u>340.00</u>	<u>1.530</u>
STA Trailing Edge - in.	<u>560.00</u>	<u>2.520</u>
Max Depth	<u> </u>	<u> </u>
Fineness Ratio	<u> </u>	<u> </u>
Area	<u> </u>	<u> </u>
Max. Cross-Sectional	<u> </u>	<u> </u>
Planform	<u> </u>	<u> </u>
Wetted	<u> </u>	<u> </u>
Base	<u> </u>	<u> </u>

Windshield Consists of Six (6) Panels
 Pilots Eye is at the Following Points:

Fus. STA - in.	408.00	1.836
B.P. - in.	24.00	.108
W.P. - in.	455.00	2.0475
View Angle Available:		
Deg Upward	20.00	
Deg Downward	24.00	

MODEL DIMENSIONAL DATA

MODEL COMPONENT : BODY - MANIPULATOR HOUSING - D1

GENERAL DESCRIPTION : _____

Model Scale = .0045

DRAWING NUMBER : VL70-000001

DIMENSIONS :	FULL SCALE	MODEL SCALE
Length - in.	<u>967.00</u>	<u>4.351</u>
Max Width - in.	<u>53.32</u>	<u>.2399</u>
Max Depth - in.	<u>20.00</u>	<u>.0900</u>
Fineness Ratio	<u>--</u>	<u>--</u>
Area	<u> </u>	<u> </u>
Max. Cross-Sectional	<u>--</u>	<u>--</u>
Planform	<u>--</u>	<u>--</u>
Wetted	<u>--</u>	<u>--</u>
Base	<u>--</u>	<u>--</u>

MODEL DIMENSIONAL DATA

MODEL COMPONENT : BODY - ORBITAL MANEUVERING SYSTEM POD-M1

GENERAL DESCRIPTION : _____

Model Scale = .0045

DRAWING NUMBER : VL70-000001

DIMENSIONS :	FULL SCALE	MODEL SCALE
Length - in.	<u>290.67</u>	<u>1.3080</u>
Max Width - in.	<u>67.33</u>	<u>.3030</u>
Max Depth - in.	<u>104.00</u>	<u>.4680</u>
Fineness Ratio	<u>--</u>	<u>--</u>
Area		
Max. Cross-Sectional	<u>--</u>	<u>--</u>
Planform	<u>--</u>	<u>--</u>
Wetted	<u>--</u>	<u>--</u>
Base	<u>--</u>	<u>--</u>

TABLE II. MODEL COMPONENT DIMENSIONS - Continued

MODEL COMPONENT: WING - W1

GENERAL DESCRIPTION: DELTA WING WITH -5° TWIST & ROUNDED WING TIPS. WING BENDS INTO BODY, FOLLOWS NAR LINES, V70-000001. EQUIV. SPAN IS 78.604% OF THEORETICAL
DELTA WING MODEL SCALE = 0.0045

DRAWING NUMBER:VL70-000001DIMENSIONS:FULL-SCALEMODEL SCALETOTAL DATA

Area in. (in. R.P.) - Ft ²		
Planform	<u>3221.92</u>	<u>.06524</u>
Wetted	<u>--</u>	<u>--</u>
Span (equivalent)	<u>1007.8</u>	<u>4.535</u>
Aspect Ratio	<u>2.144</u>	<u>2.144</u>
Rate of Taper	<u>1.191</u>	<u>1.191</u>
Taper Ratio	<u>0.219</u>	<u>0.219</u>
Diehedral Angle, degrees	<u>3.500</u>	<u>3.500</u>
Incidence Angle, degrees	<u>3.000</u>	<u>3.000</u>
Aerodynamic Twist, degrees	<u>-5.00</u>	<u>-5.00</u>
Toe-In Angle	<u>3.00</u>	<u>3.00</u>
Cant Angle	<u>-2.00</u>	<u>-2.00</u>
Sweep Back Angles, degrees		
Leading Edge	<u>49.910</u>	<u>49.910</u>
Trailing Edge	<u>-0.183</u>	<u>-0.183</u>
0.25 Element Line	<u>41.675</u>	<u>41.675</u>
Chords:		
Root (Wing Sta. 0.0)	<u>760.56</u>	<u>3.4225</u>
Tip, (equivalent)	<u>159.72</u>	<u>.7187</u>
MAC	<u>525.4</u>	<u>2.364</u>
Fus. Sta. of .25 MAC	<u>1132.98</u>	<u>5.098</u>
W.P. of .25 MAC	<u>304.55</u>	<u>1.370</u>
B.L. of .25 MAC	<u>196.09</u>	<u>.8824</u>
Airfoil Section		
Root	<u>--</u>	<u>--</u>
Tip	<u>--</u>	<u>--</u>

EXPOSED DATA

Area in (W.R.P) - Ft ²	<u>2203.0</u>	<u>0.0446</u>
Span, (equivalent)	<u>795.86</u>	<u>3.5814</u>
Aspect Ratio	<u>1.966</u>	<u>1.966</u>
Taper Ratio	<u>0.260</u>	<u>0.260</u>
Chords		
Root	<u>641.57</u>	<u>2.887</u>
Tip	<u>166.68</u>	<u>.7501</u>
MAC	<u>450.63</u>	<u>2.028</u>
Fus. Sta. of .25 MAC	<u>1190.82</u>	<u>5.359</u>
W.P. of .25 MAC	<u>305.47</u>	<u>1.375</u>
B.L. of .25 MAC	<u>260.80</u>	<u>1.174</u>
Leading Edge Cuff		
Planform Area (W.F.P.) - Ft ²	<u>271.39</u>	<u>.00549</u>
Leading Edge Intersects Fus ML @ STA. - in.	<u>540.00</u>	<u>2.430</u>
Leading Edge Intersects Fus ML @ Sta. - in.	<u>1114.0</u>	<u>5.013</u>

TABLE II. MODEL COMPONENT DIMENSIONS - Continued

MODEL COMPONENT: ELEVON - E1 (DATA FOR 1 of 2 SIDES)GENERAL DESCRIPTION: FULL SPAN CONSTANT CHORD ELEVON LOCATED ON WING - W1

MODEL SCALE = 0.0045

DRAWING NUMBER: VL70-000001

<u>DIMENSIONS:</u>	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Area (True) - Ft^2	<u>347.2</u>	<u>.0070</u>
Span (equivalent) - in.	<u>384.0</u>	<u>1.728</u>
Inb'd equivalent chord - in.	<u>134.38</u>	<u>.6047</u>
Outb'd equivalent chord	<u>134.38</u>	<u>.6047</u>
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord	<u>0.209</u>	<u>0.209</u>
At Outb'd equiv. chord	<u>0.805</u>	<u>0.805</u>
Sweep Back Angles, degrees		
Leading Edge	<u>-0.183</u>	<u>-0.183</u>
Tailing Edge	<u>-0.183</u>	<u>-0.183</u>
Hingeline	<u>-0.183</u>	<u>-0.183</u>
Area Moment (Normal to hinge line) - Ft^3	<u>4164.4</u>	<u>.00038</u>
(Product of Area & Mean Chord)		

TABLE II. MODEL COMPONENT DIMENSIONS - Continued

MODEL COMPONENT: VERTICAL TAIL - V1

GENERAL DESCRIPTION: CENTERLINE VERTICAL DELTA WING CONFIGURATION

MODEL SCALE = 0.0045

DRAWING NUMBER: VL70-000001

DIMENSIONS: FULL-SCALE MODEL SCALETOTAL DATA

Area - Ft ²	415.25	.0084
*Void (Included Above)	1.29	.00003
Blanketed (Included Above)	19.93	.00040
Span (equivalent)	323.9	1.4575
Aspect Ratio	1.675	1.675
Rate of Taper	0.504	0.504
Taper Ratio	0.424	0.424
Diehedral Angle, degrees	--	--
Incidence Angle, degrees	--	--
Aerodynamic Twist, degrees	--	--
Toe-In Angle	0.0	0.0
Cant Angle	0.0	0.0
Sweep Back Angles, degrees		
Leading Edge	45.00	45.00
Trailing Edge	26.361	26.361
0.25 Element Line	41.150	41.150
Chords:		
Root (Wing Sta. 0.0)	275.52	1.240
Tip, (equivalent)	111.4	.5013
MAC	205.0	.922
Fus. Sta. of .25 MAC	1462.2	6.580
W.P. of .25 MAC	639.0	2.876
B.L. of .25 MAC	0.0	0.0
Airfoil Section 5° Half Angle		
Root Double Wedge with		
Tip Rounded L.E.		

EXPOSED DATA

Area		
Span, (equivalent)		
Aspect Ratio		
Taper Ratio		
Chords		
Root		
Tip		
MAC		
Fus. Sta. of .25 MAC		
W.P. of .25 MAC		
B.L. of .25 MAC		

*Void Area Located at the Lower
Aft Portion of the Surface

TABLE II. MODEL COMPONENT DIMENSIONS - Continued

MODEL COMPONENT: RUDDER - R1GENERAL DESCRIPTION: RUDDER ON CENTER LINE VERTICALMODEL SCALE = 0.0045DRAWING NUMBER: VL70-000001

<u>DIMENSIONS:</u>	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Area - Ft^2	<u>117.7</u>	<u>.00238</u>
Span (equivalent) - in.	<u>226.0</u>	<u>1.017</u>
Inb'd equivalent chord - in.	<u>97.09</u>	<u>.4369</u>
Outb'd equivalent chord - in.	<u>52.02</u>	<u>.2341</u>
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord	<u>0.400</u>	<u>0.400</u>
At Outb'd equiv. chord	<u>0.400</u>	<u>0.400</u>
Sweep Back Angles, degrees		
Leading Edge	<u>34.889</u>	<u>34.889</u>
Tailing Edge	<u>26.361</u>	<u>26.361</u>
Hingeline	<u>34.889</u>	<u>34.889</u>
Area Moment (Normal to hinge line) - Ft^3	<u>647.71</u>	<u>.00006</u>
(Product of Chord and Mean Chord)		

TABLE II. MODEL COMPONENT DIMENSIONS - Continued

MODEL COMPONENT: BODY - T₁GENERAL DESCRIPTION: EXTERNAL TANK (BASELINE DIAMETER) WITH 30° HALF
ANGLE NOSE CONE AND RETROROCKET

DRAWING NUMBER

<u>DIMENSION:</u>	<u>FULL SCALE</u>	<u>MODEL SCALE</u>
Length	<u>2184 in.</u>	<u>9.828 in.</u>
Max Width	<u>318 in.</u>	<u>1.431</u>
Max Depth	<u>318 in.</u>	<u>1.431</u>
Fineness Ratio	<u>6.87</u>	<u>6.87</u>
Area		
Max Cross-Sectional	<u>551.54 ft²</u>	<u>.011169 ft²</u>
Planform	<u>--</u>	<u>--</u>
Wetted	<u>--</u>	<u>--</u>
Base	<u>551.54 ft²</u>	<u>.011169 ft²</u>

TABLE II. MODEL COMPONENT DIMENSIONS - Continued.

MODEL COMPONENT: BODY - S₁GENERAL DESCRIPTION: SOLID ROCKET MOTOR (BASELINE DIAMETER) WITH
HOLDDOWN ARMS

DRAWING NUMBER

<u>DIMENSION:</u>	<u>FULL SCALE</u>	<u>MODEL SCALE</u>
Length	<u>2217 in.</u>	<u>9.976 in.</u>
Max Width	<u>156 in.</u>	<u>.702 in.</u>
Max Depth	<u>156 in.</u>	<u>.702 in.</u>
Fineness Ratio	<u>14.21</u>	<u>14.21</u>
Area		
Max Cross-Sectional	<u>132.5 ft²</u>	<u>.002683 ft²</u>
Planform	<u>--</u>	<u>--</u>
Wetted	<u>--</u>	<u>--</u>
Base	<u>132.5 ft²</u>	<u>.002683 ft²</u>

TABLE II. MODEL DIMENSIONAL DATA - Concluded.

MODEL COMPONENT : Body Flap, F1

GENERAL DESCRIPTION : Rectangular body flap located on lower aft
portion of body and extending aft of body.

DRAWING NUMBER : _____

DIMENSIONS :

FULL SCALE MODEL SCALE

Length, in. _____ 1.08186

Max Width, in. _____ .41242

Max Depth _____ _____

Fineness Ratio _____ _____

Area _____ _____

Max. Cross-Sectional _____ _____

Planform _____ _____

Wetted _____ _____

Base _____ _____

MODEL FIGURES

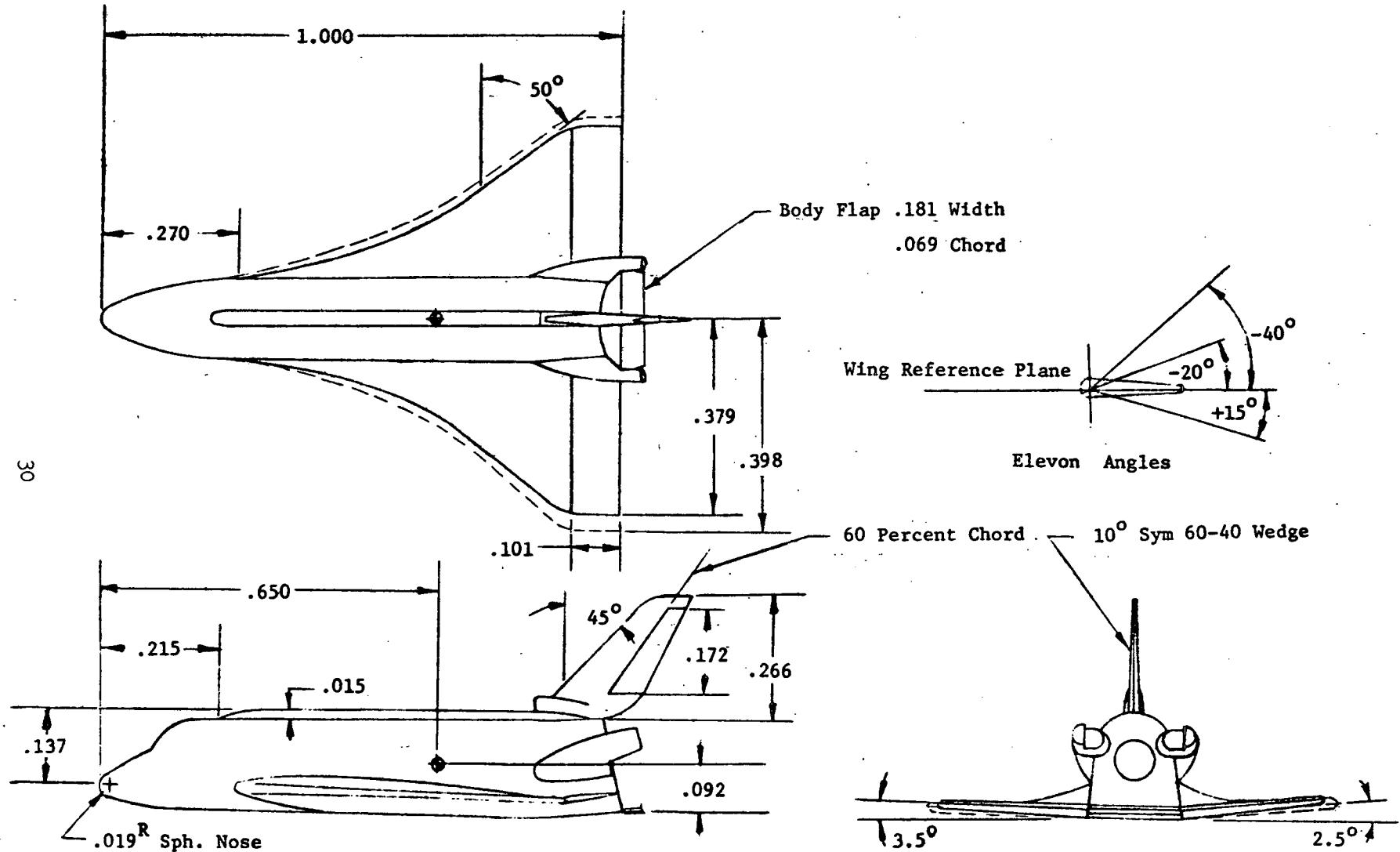


Figure 1. North American Rockwell baseline (.0045 scale) delta-wing orbiter (ATP) with .0047 scale wing superimposed. All linear dimensions are in terms of orbiter body length (15.182cm).

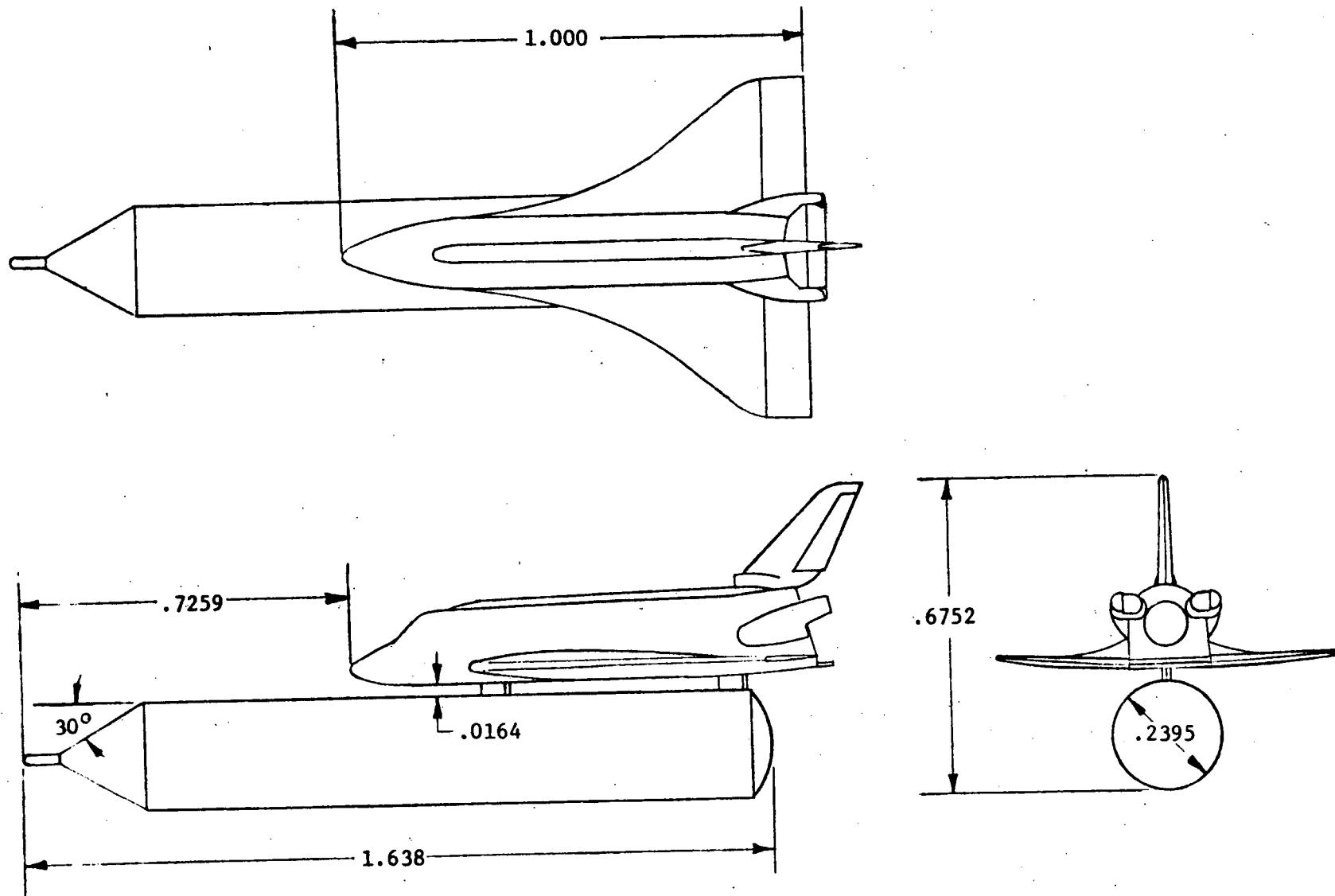
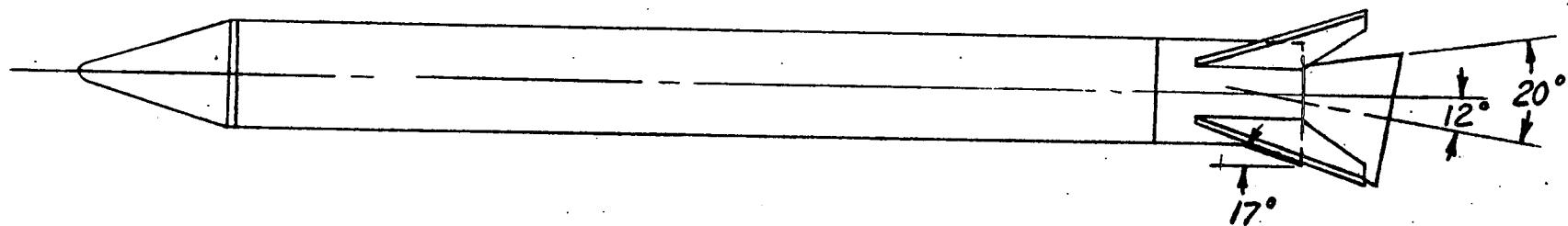


Figure 2. NR-ATP baseline orbiter with external tank (.0045 Scale). All dimensions are in terms of orbiter body length (15.182 cm)



32

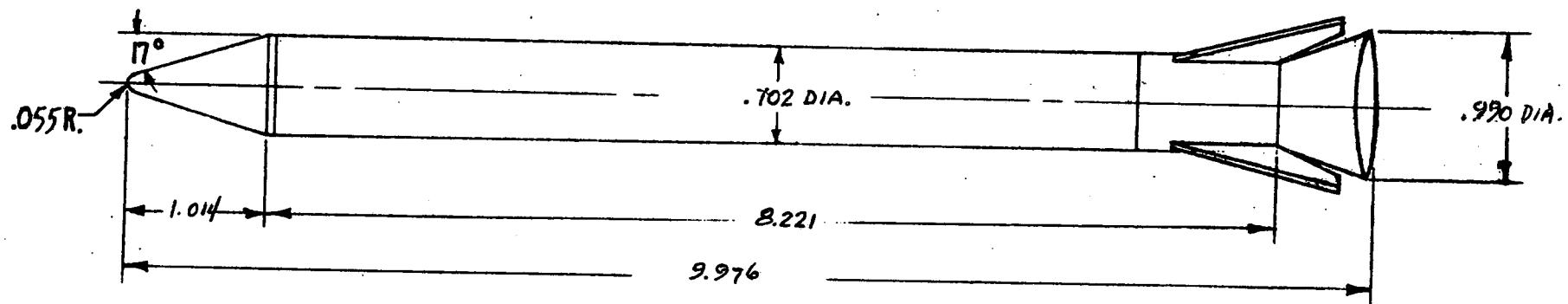
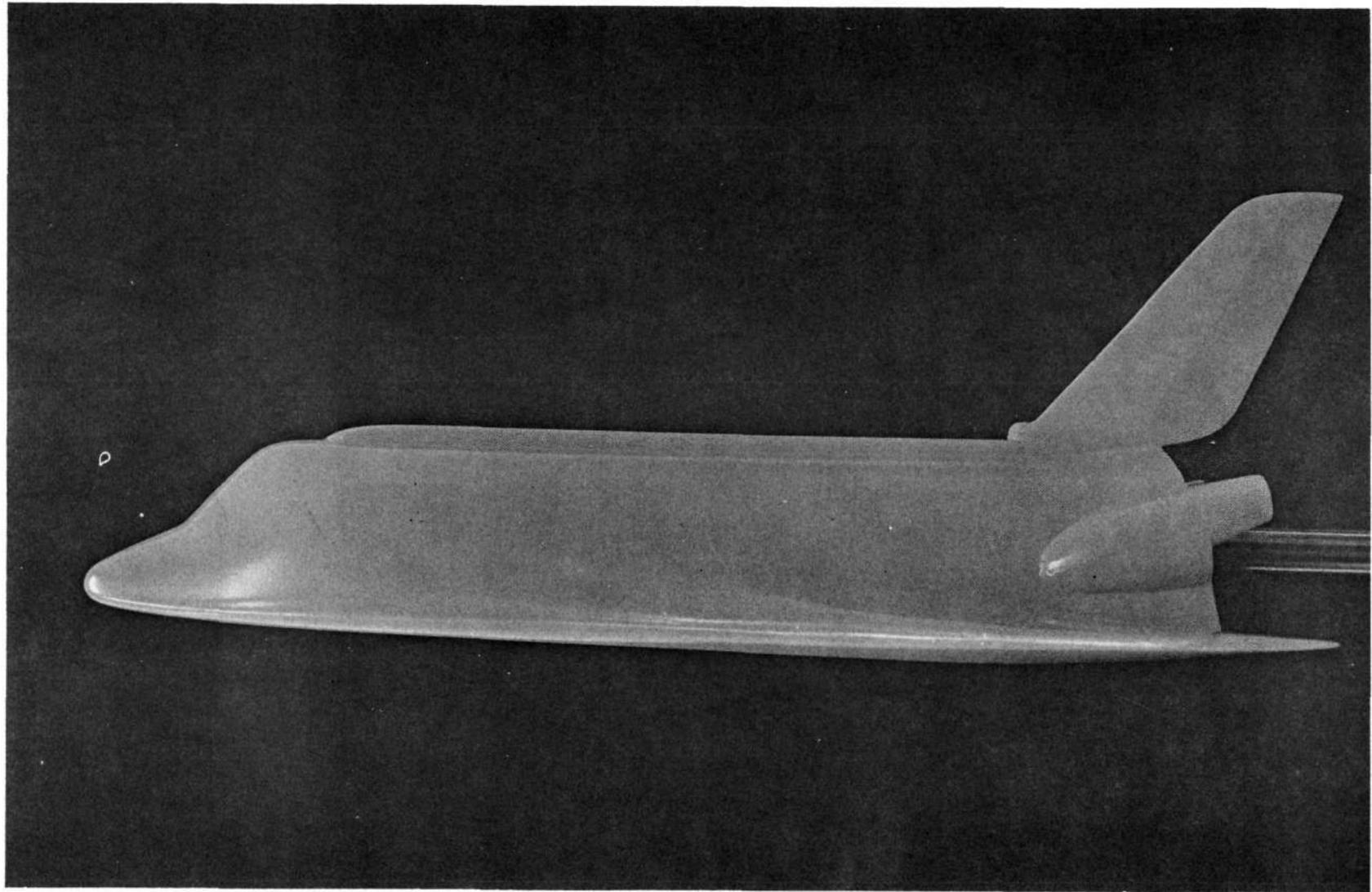
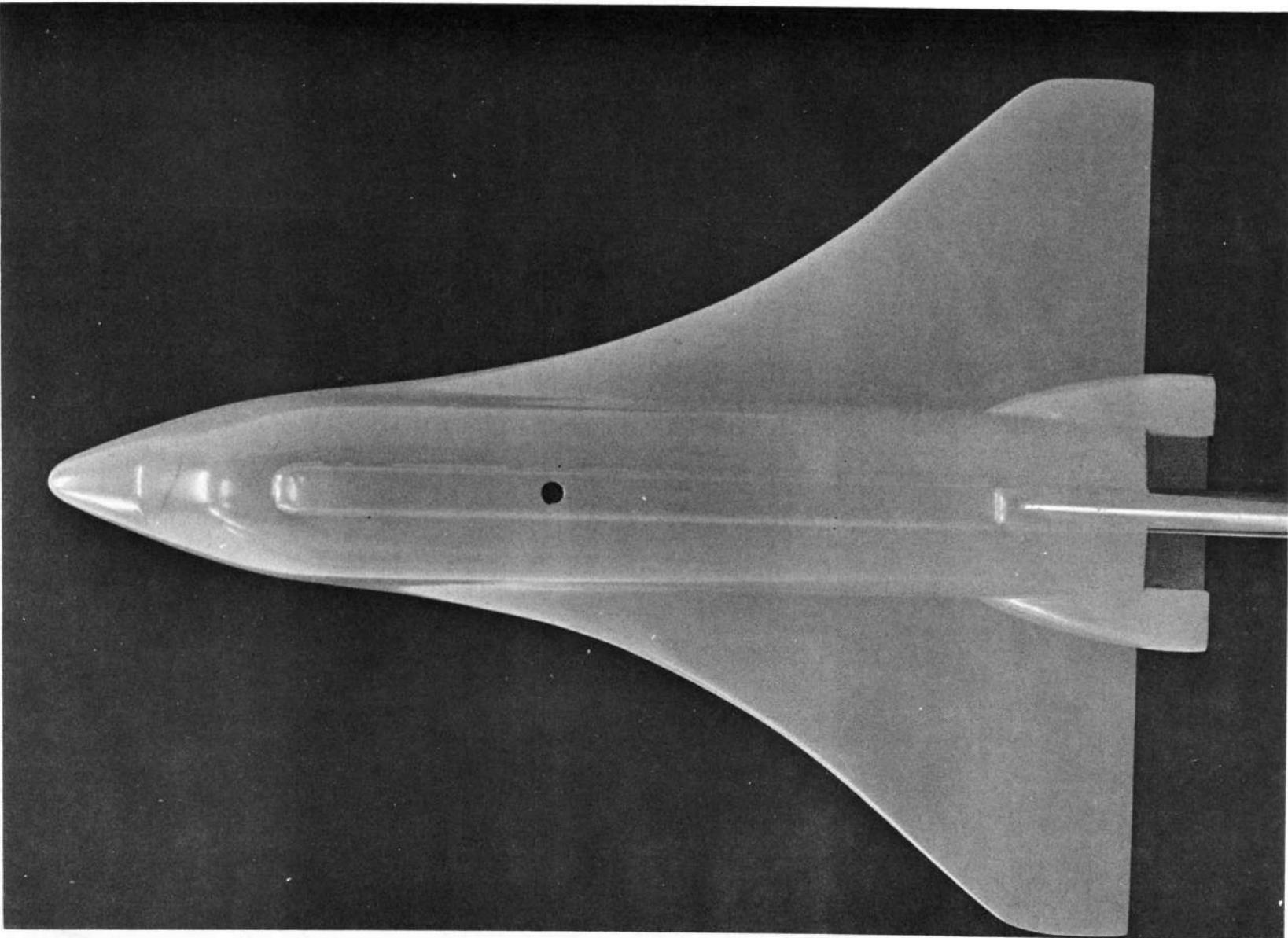


Figure 3. SRB general arrangement.
All dimensions are in inches.



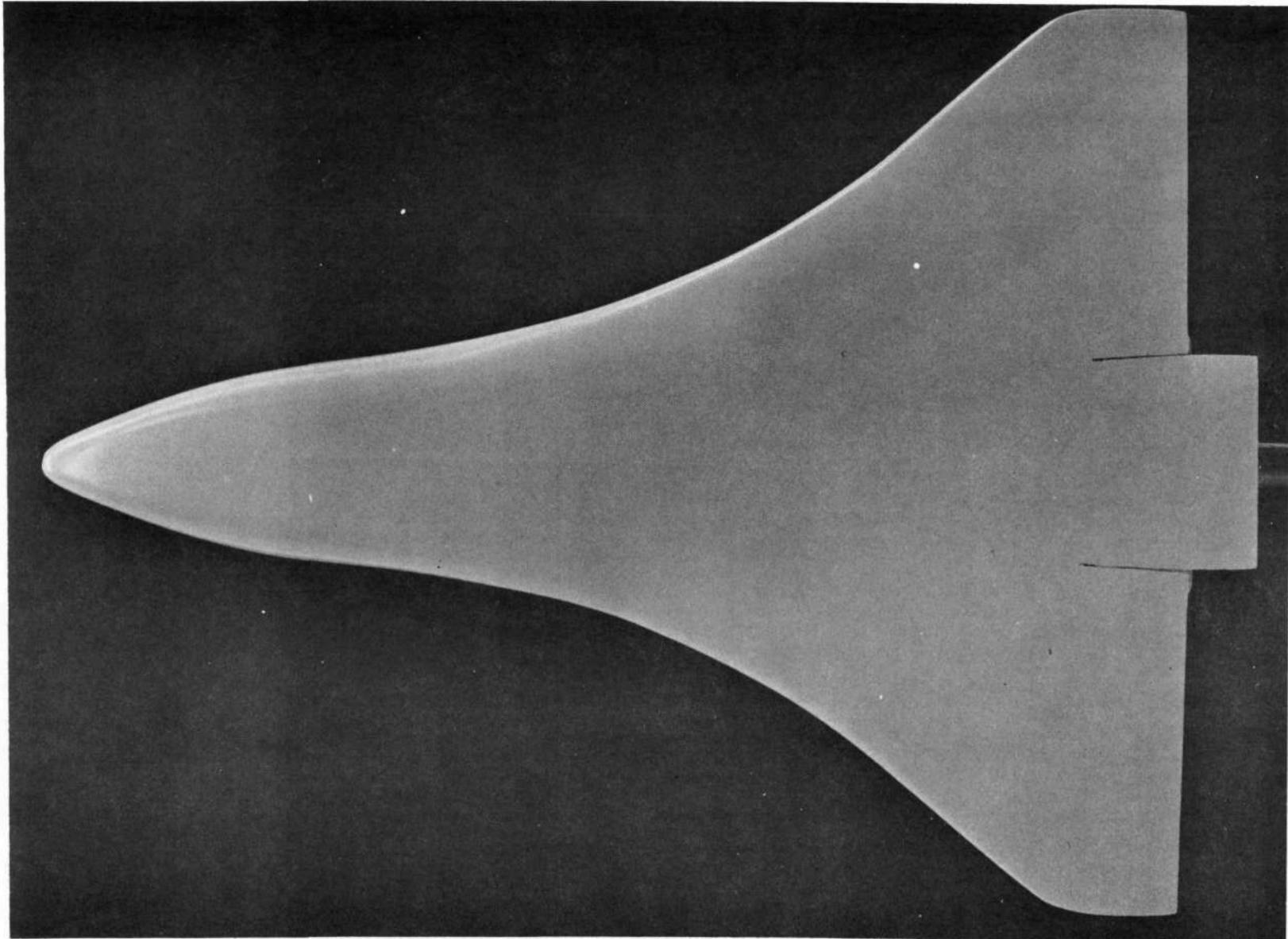
A) Left side view

Figure 4. - Photograph of .0045 Scale NR (ATP) Orbiter Configuration.



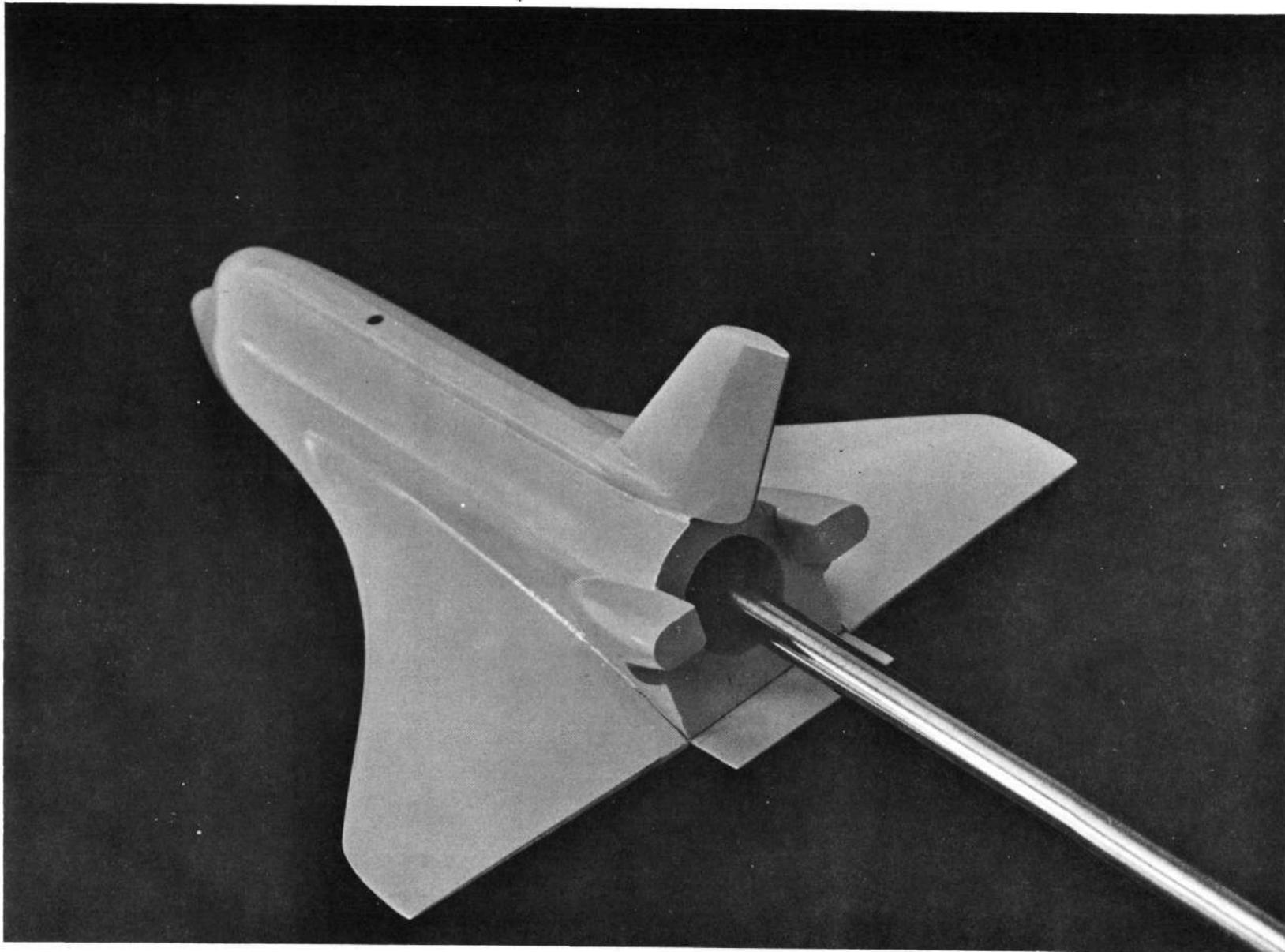
B) Top view

Figure 4. - Photograph of .0045 Scale NR (ATP) Orbiter Configuration.



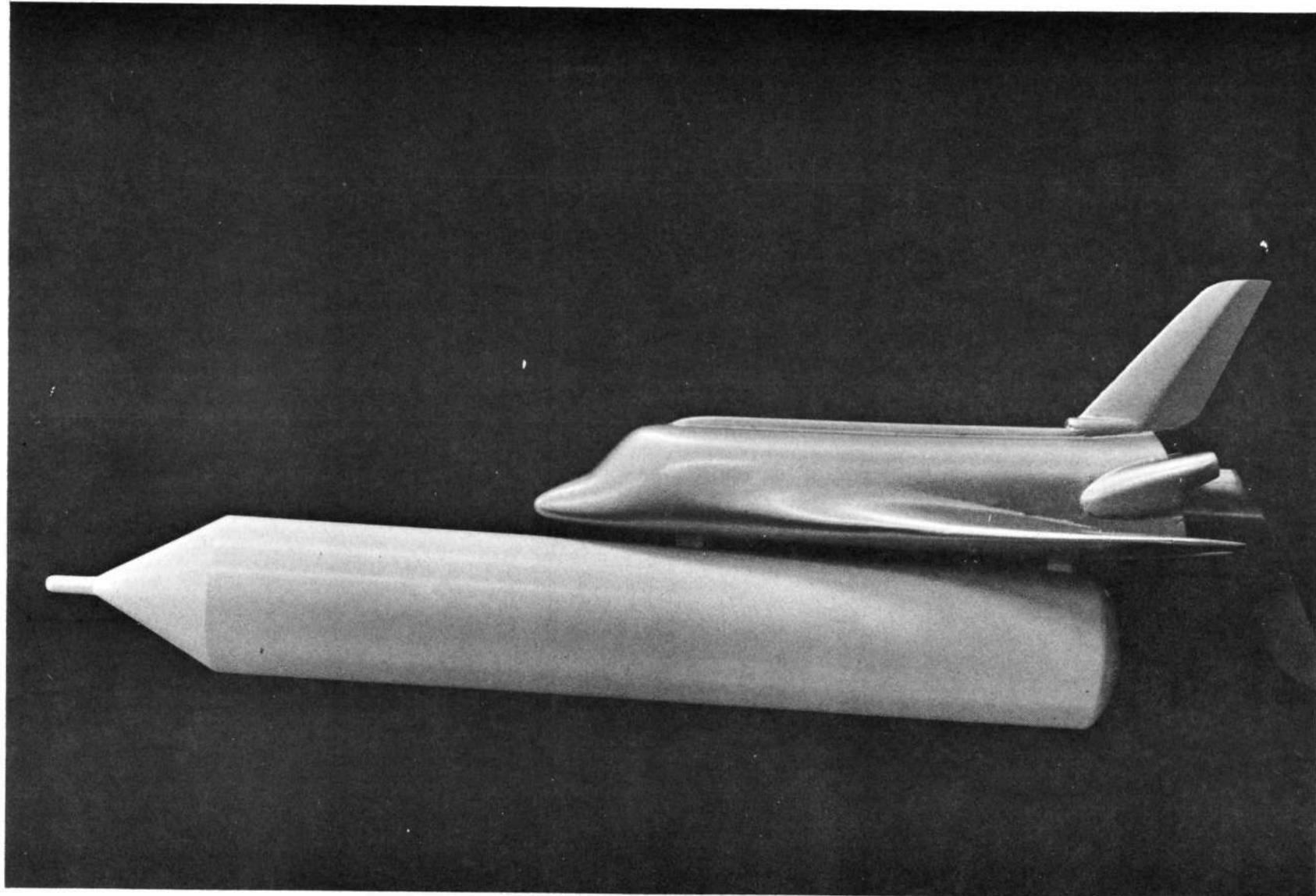
C) Bottom view

Figure 4. - Photograph of .0045 Scale NR (ATP) Orbiter Configuration.



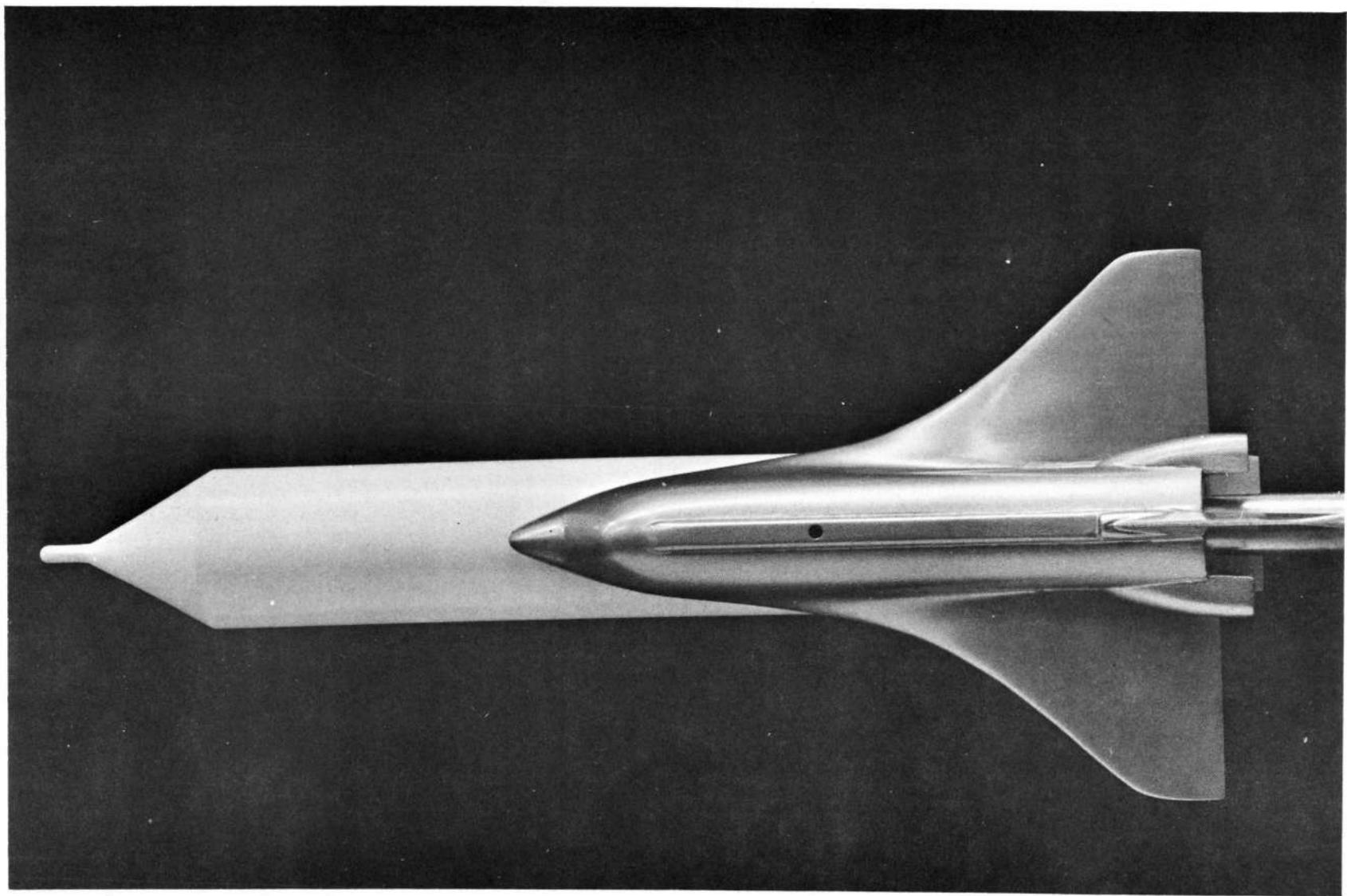
D) Rear oblique view

Figure 4. - Photograph of .0045 Scale NR (ATP) Orbiter Configuration.



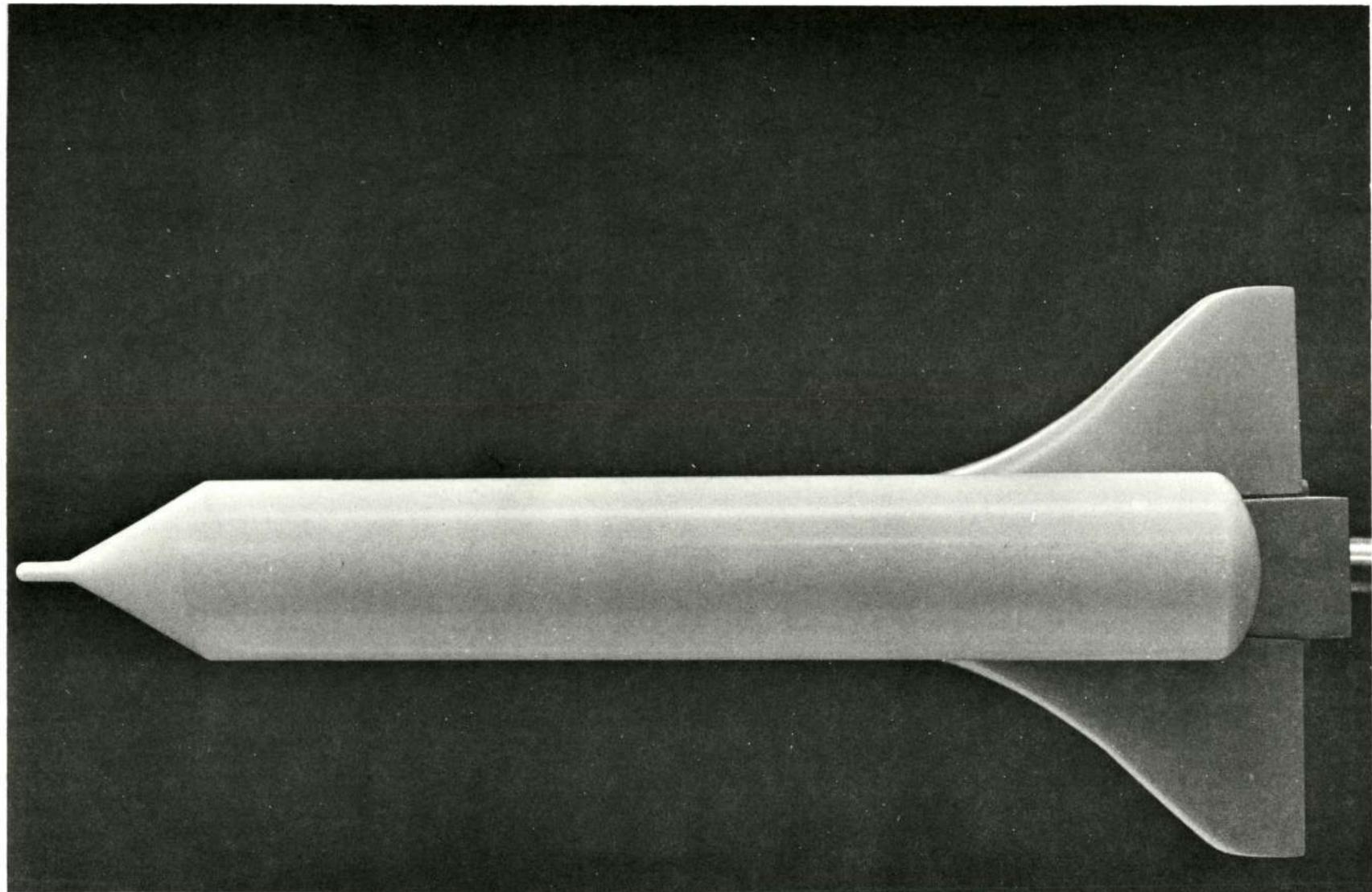
A) Left side view

Figure 5. - Photograph of .0045 Scale NR (ATP) Orbiter
With External Tank Configuration.



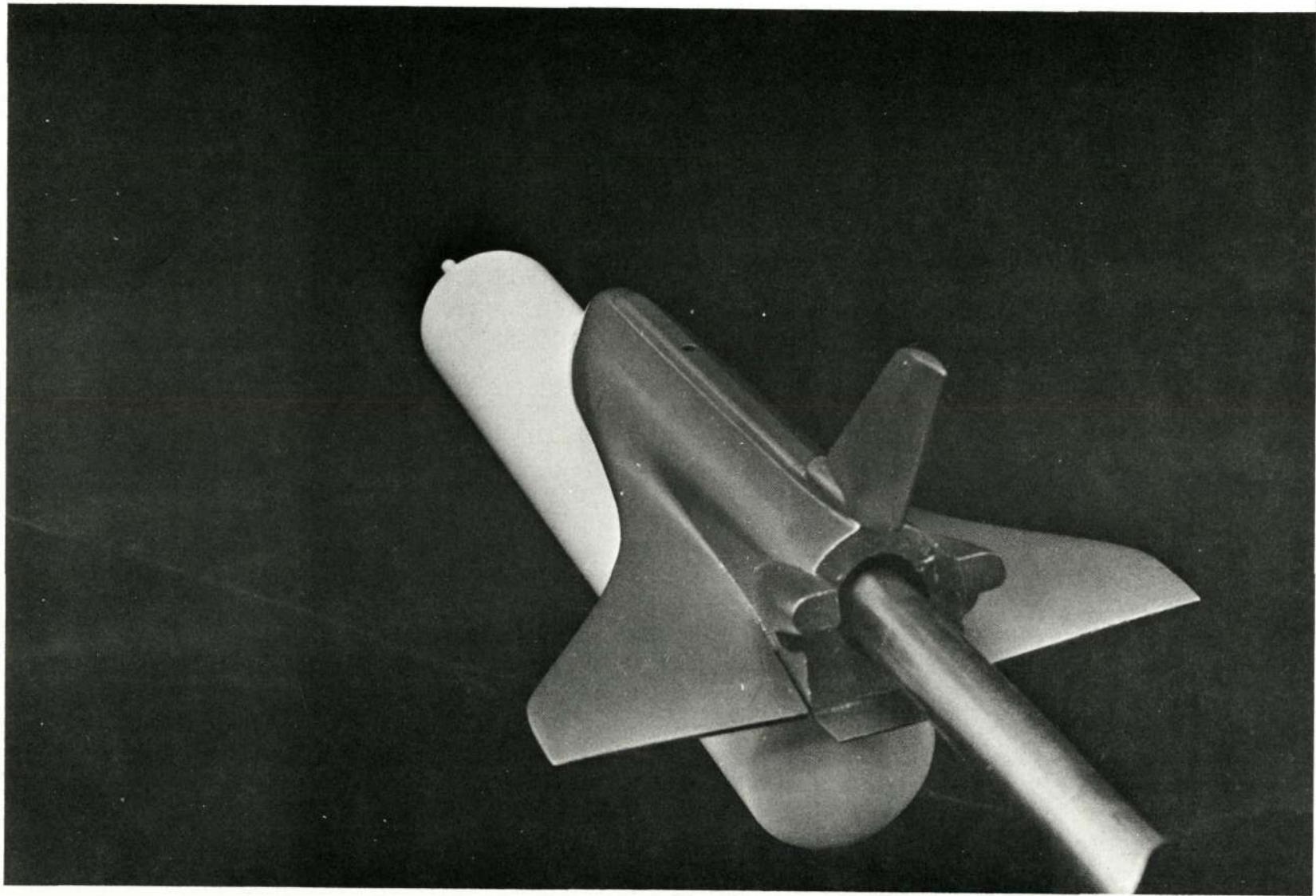
B) Top view

Figure 5. - Photograph of .0045 Scale NR (ATP) Orbiter
With External Tank Configuration.



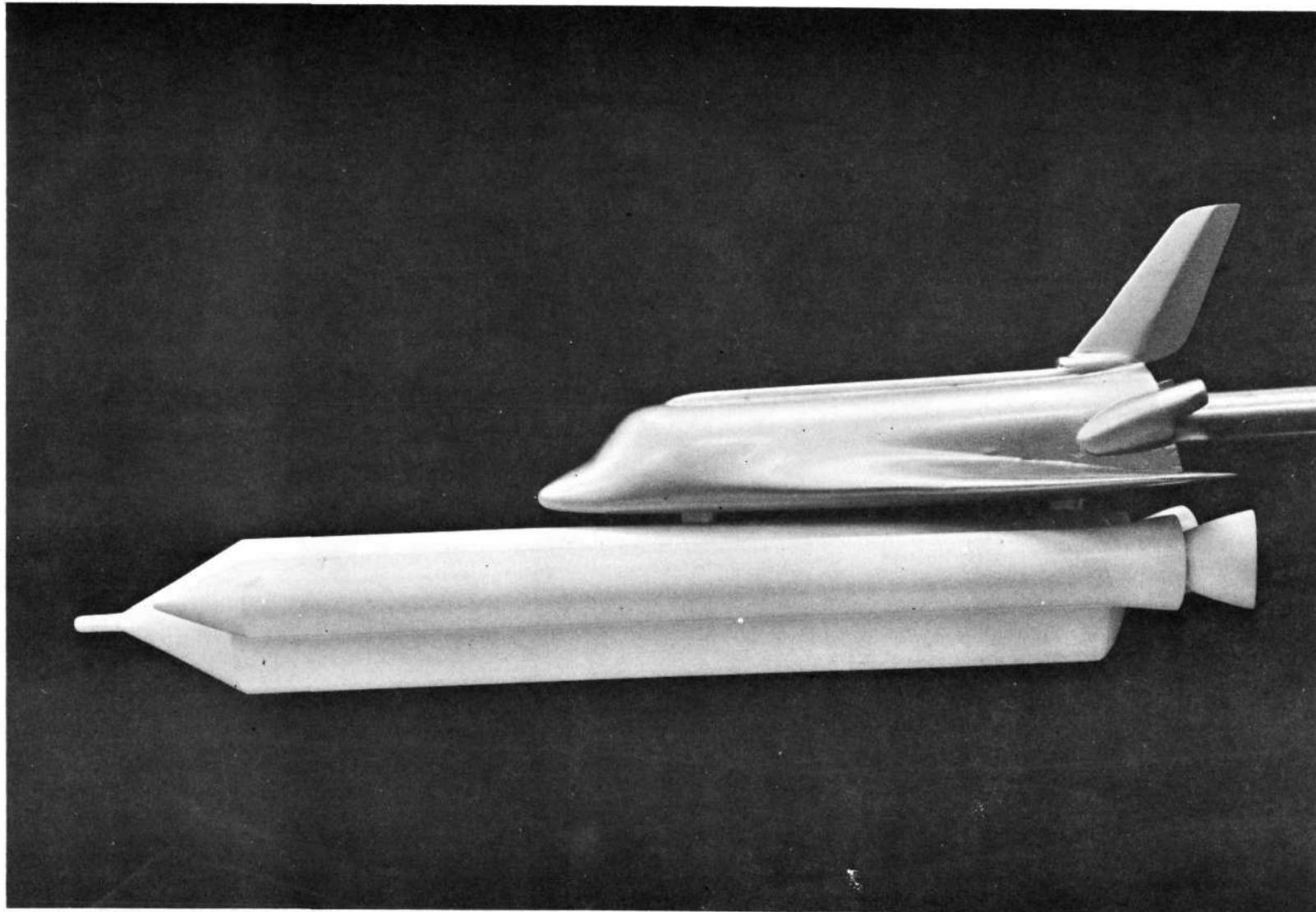
C) Bottom view

Figure 5. - Photograph of .0045 Scale NR (ATP) Orbiter
With External Tank Configuration.



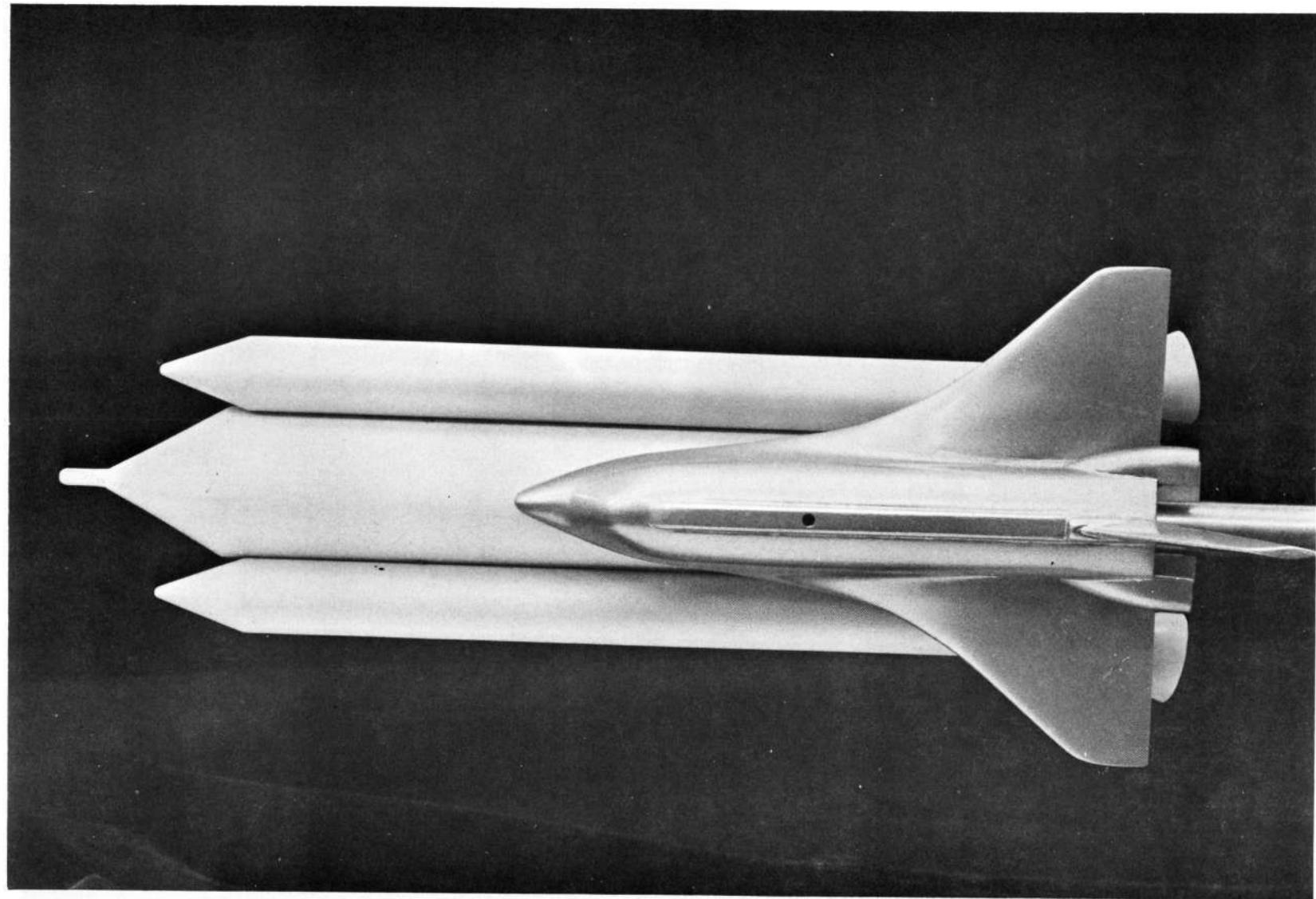
D) Rear oblique view

Figure 5. - Photograph of .0045 Scale NR (ATP) Orbiter
With External Tank Configuration.



A) Left side view

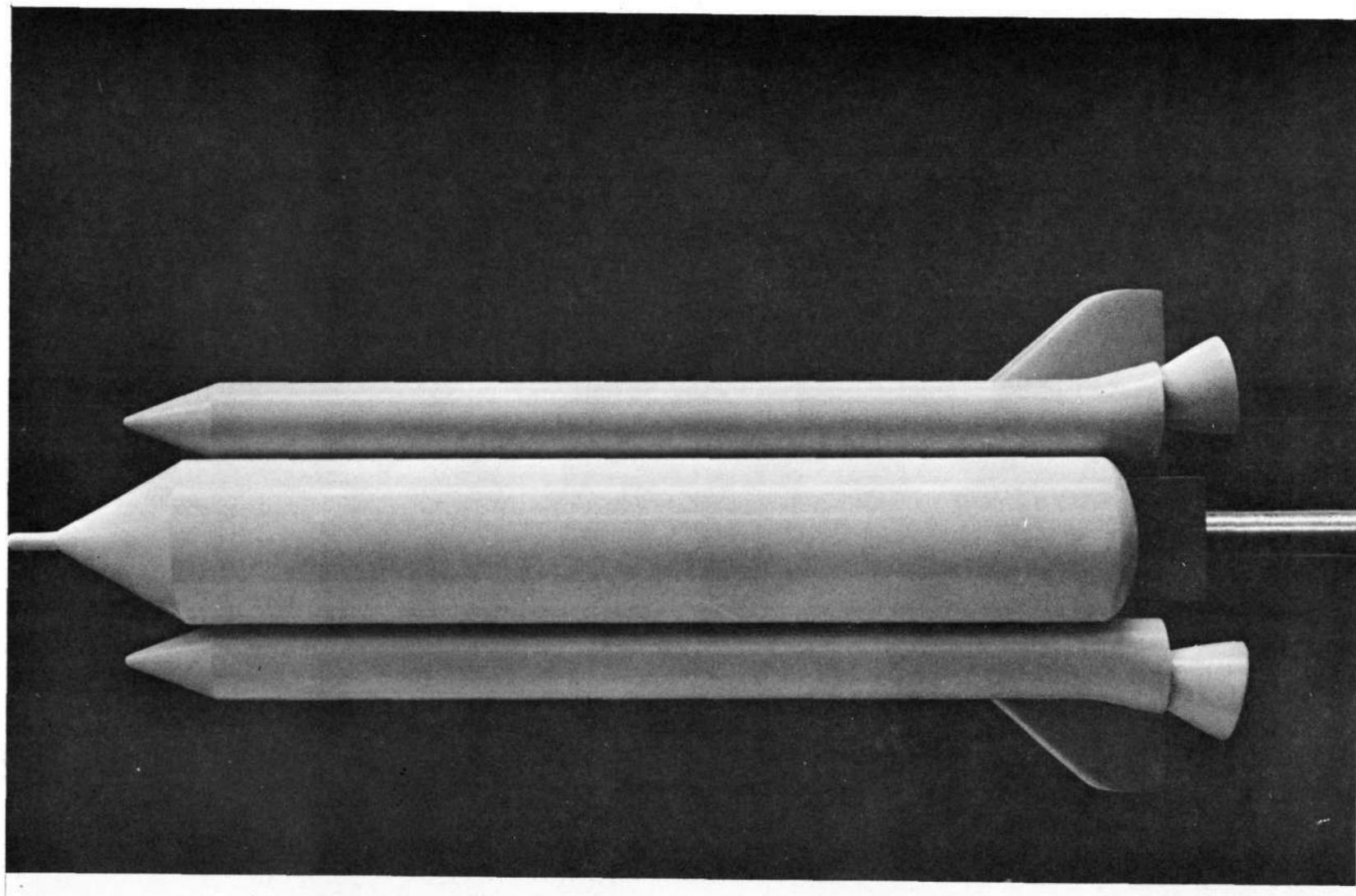
Figure 6. - Photograph of .0045 Scale NR (ATP) Ascent Configuration.



B) Top view

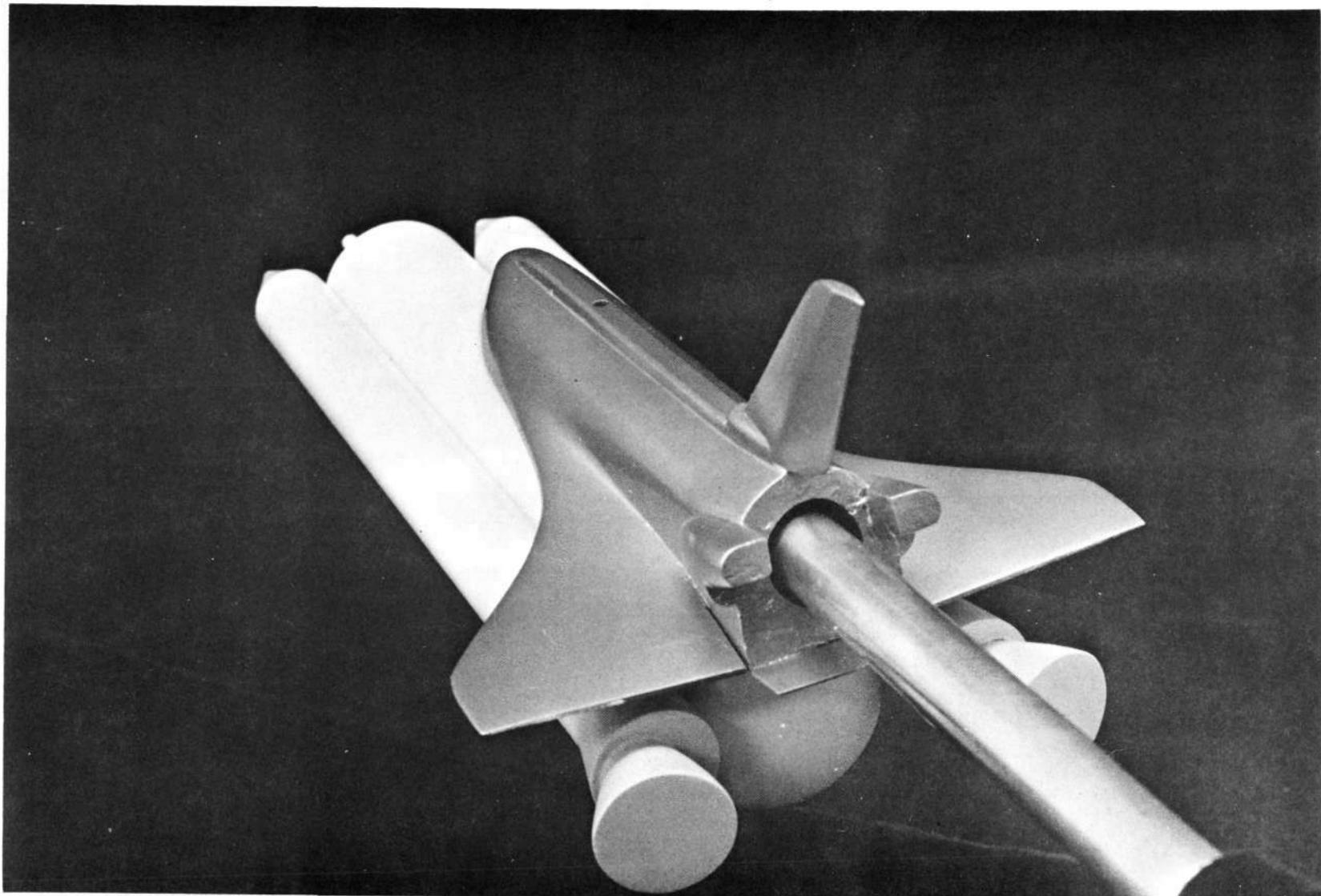
Figure 6. - Photograph of .0045 Scale NR (ATP) Ascent Configuration.

43



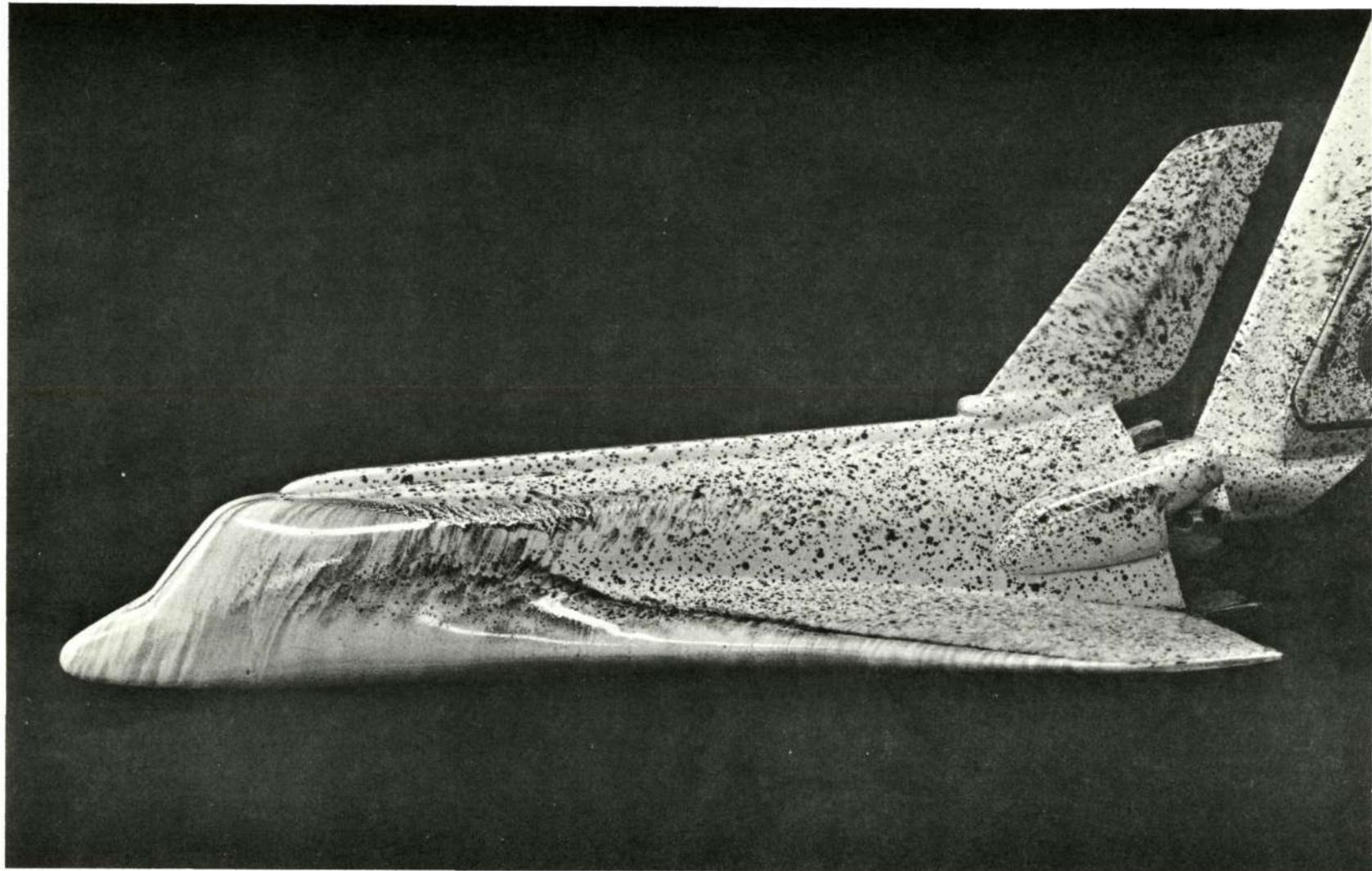
C) Bottom view

Figure 6. - Photograph of .0045 Scale NR (ATP) Ascent Configuration.



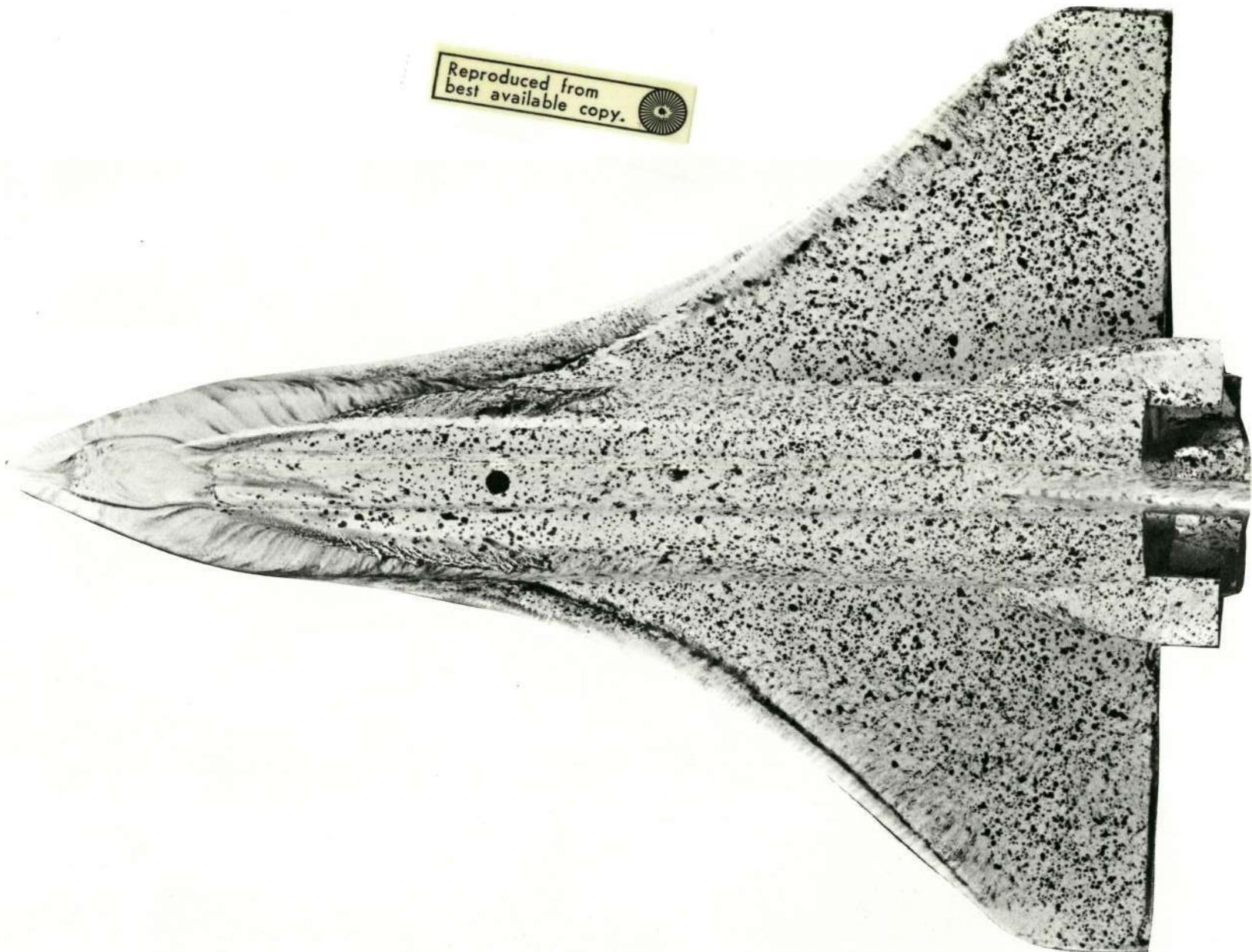
D) Rear oblique view

Figure 6. - Photograph of .0045 Scale NR (ATP) Ascent Configuration.



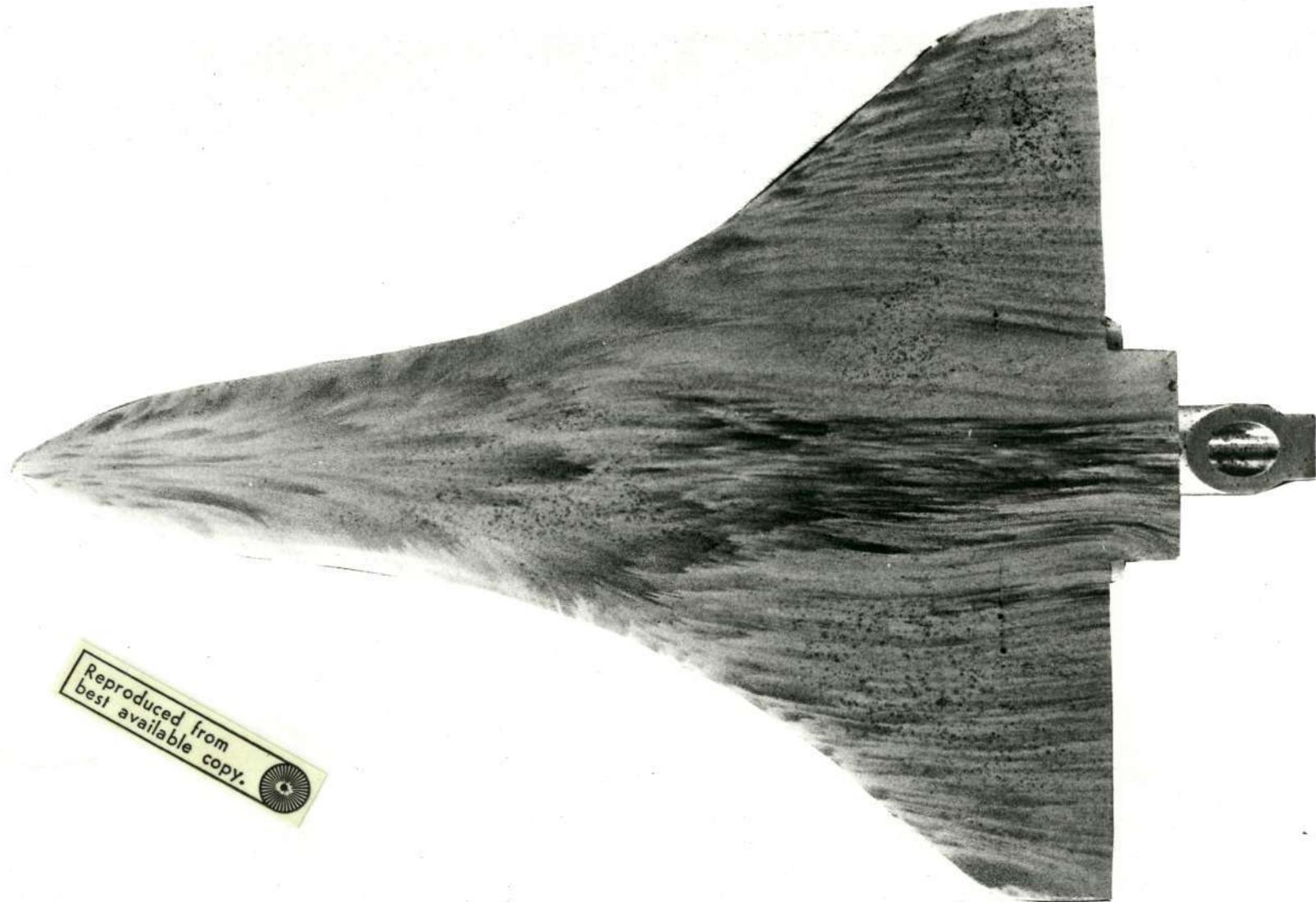
A) Left side view

Figure 7. - Photograph of Oil Flow Pattern After Tunnel Shutdown on the .0045 Scale NR (ATP) Orbiter at $M = 20.3$ and $\alpha = 51^\circ$; $\delta_e = 0^\circ$



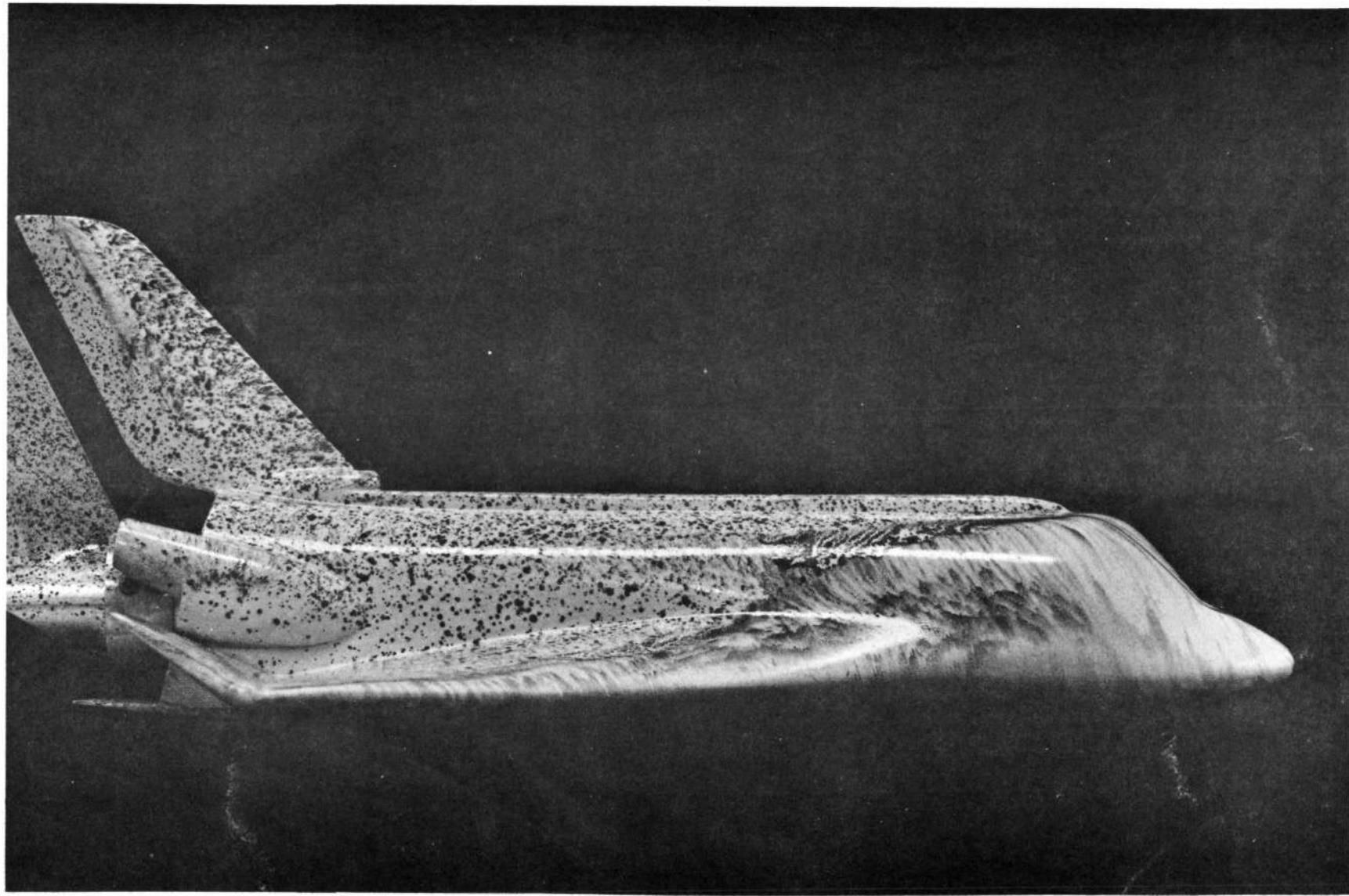
B) Top view

Figure 7. - Photograph of Oil Flow Pattern After Tunnel Shutdown on the .0045 Scale NR (ATP) Orbiter at $M = 20.3$ and $\alpha = 51^\circ$; $\delta_e = 0^\circ$.



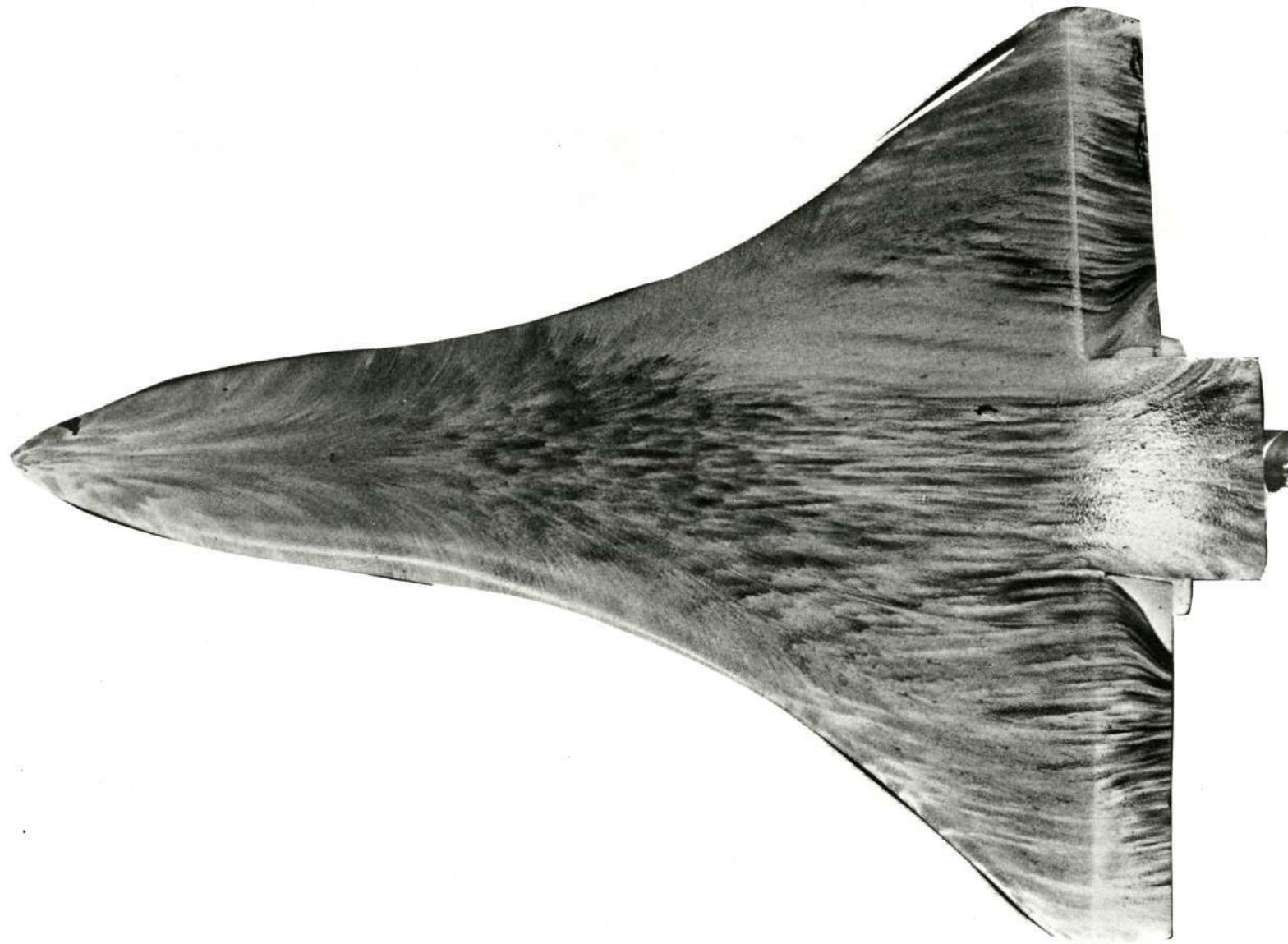
c) Bottom view

Figure 7. - Photograph of Oil Flow Pattern After Tunnel Shutdown on the .0045 Scale NR (ATP) Orbiter at $M = 20.3$ and $\alpha = 51^\circ$; $\delta_e = 0^\circ$.



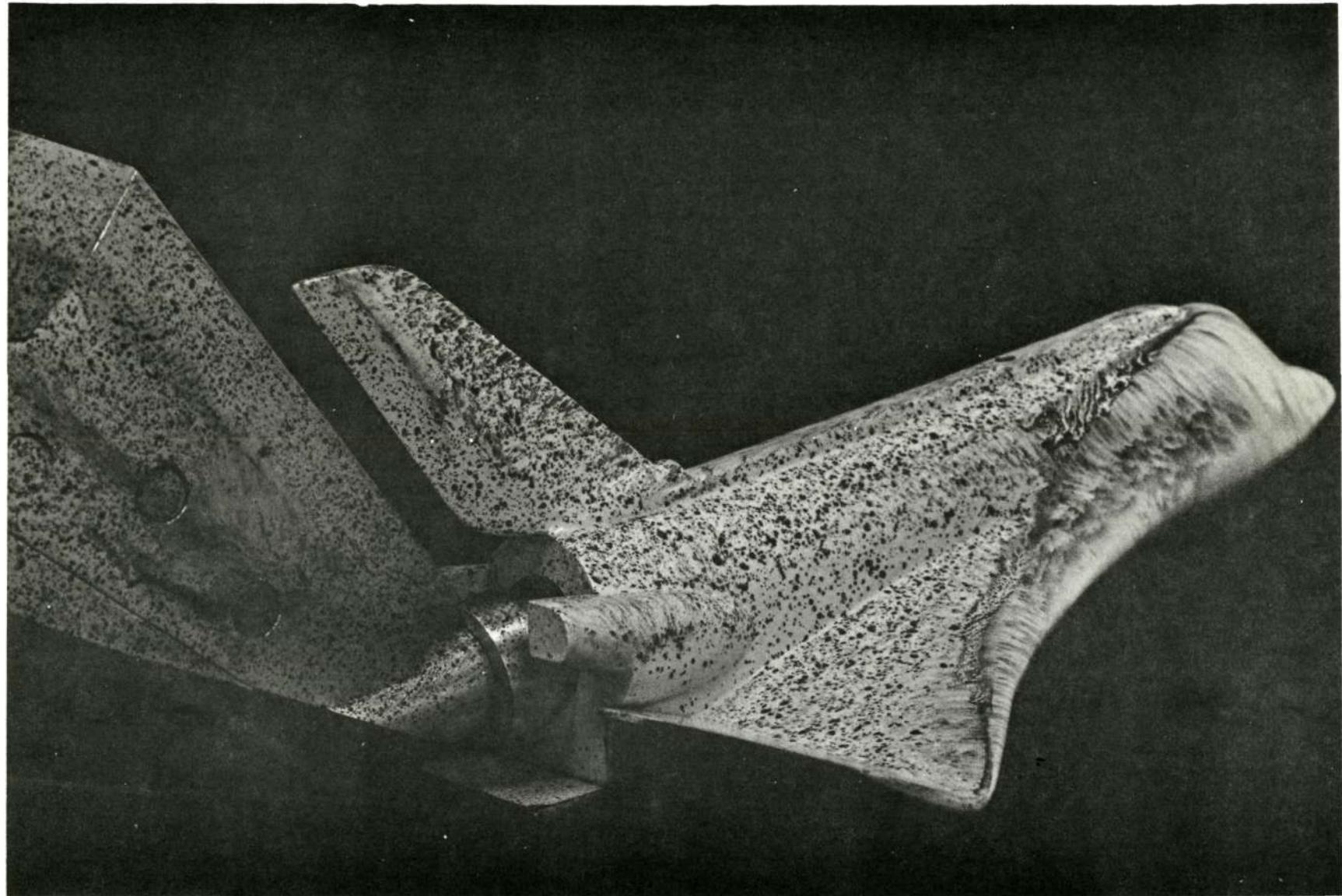
A) Right side view

Figure 8. - Photograph of Oil Flow Pattern After Tunnel Shutdown on the
0.0045 Scale NR (ATP) Orbiter at $M = 20.3$ and $\alpha = 51^\circ$; $\delta_e = -40^\circ$.



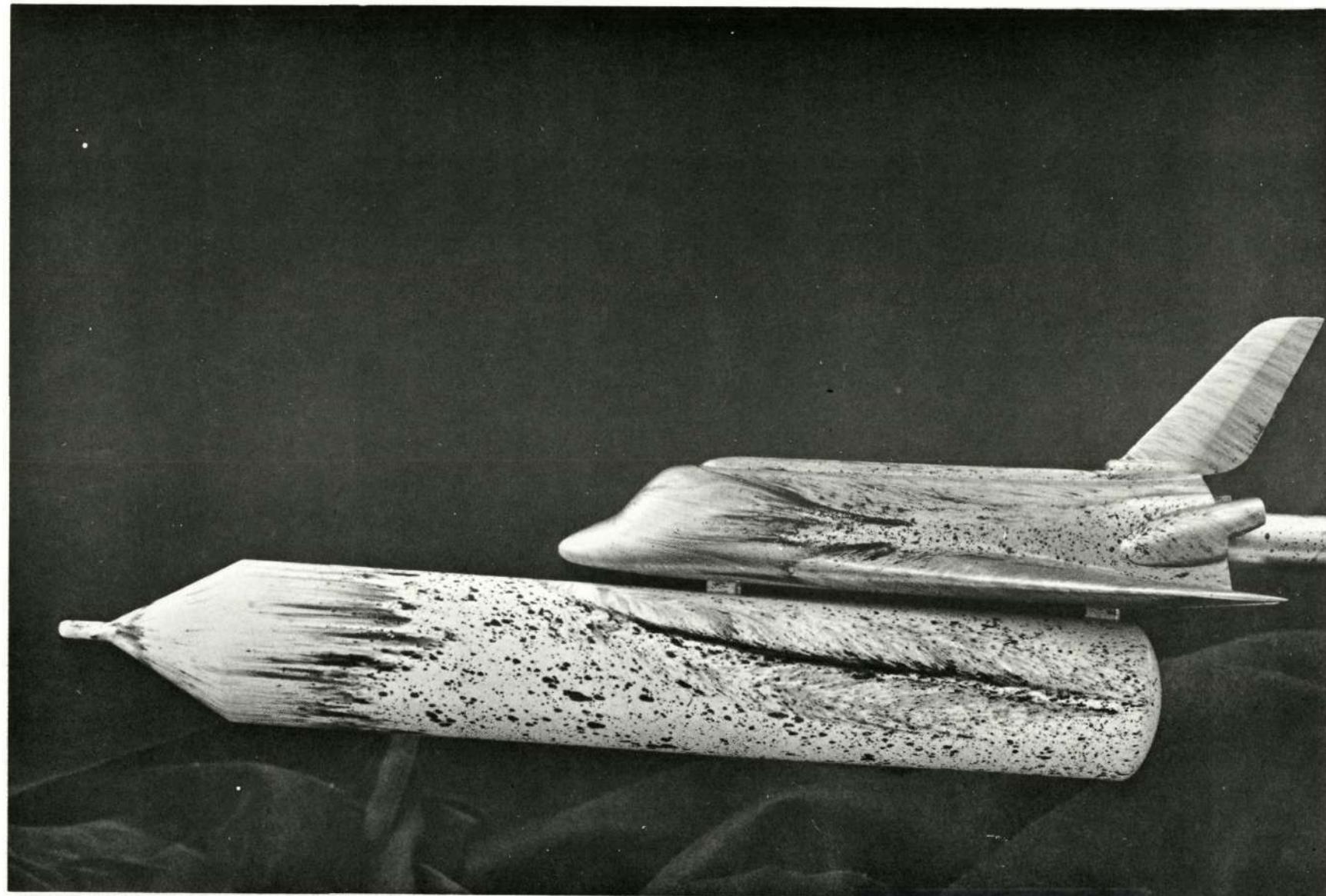
B) Bottom view

Figure 8. - Photograph of Oil Flow Pattern After Tunnel Shutdown on the
.0045 Scale NR (ATP) Orbiter at $M = 20.3$ and $\alpha = 51^\circ$; $\delta_e = -40^\circ$.



C) Right side rear oblique view

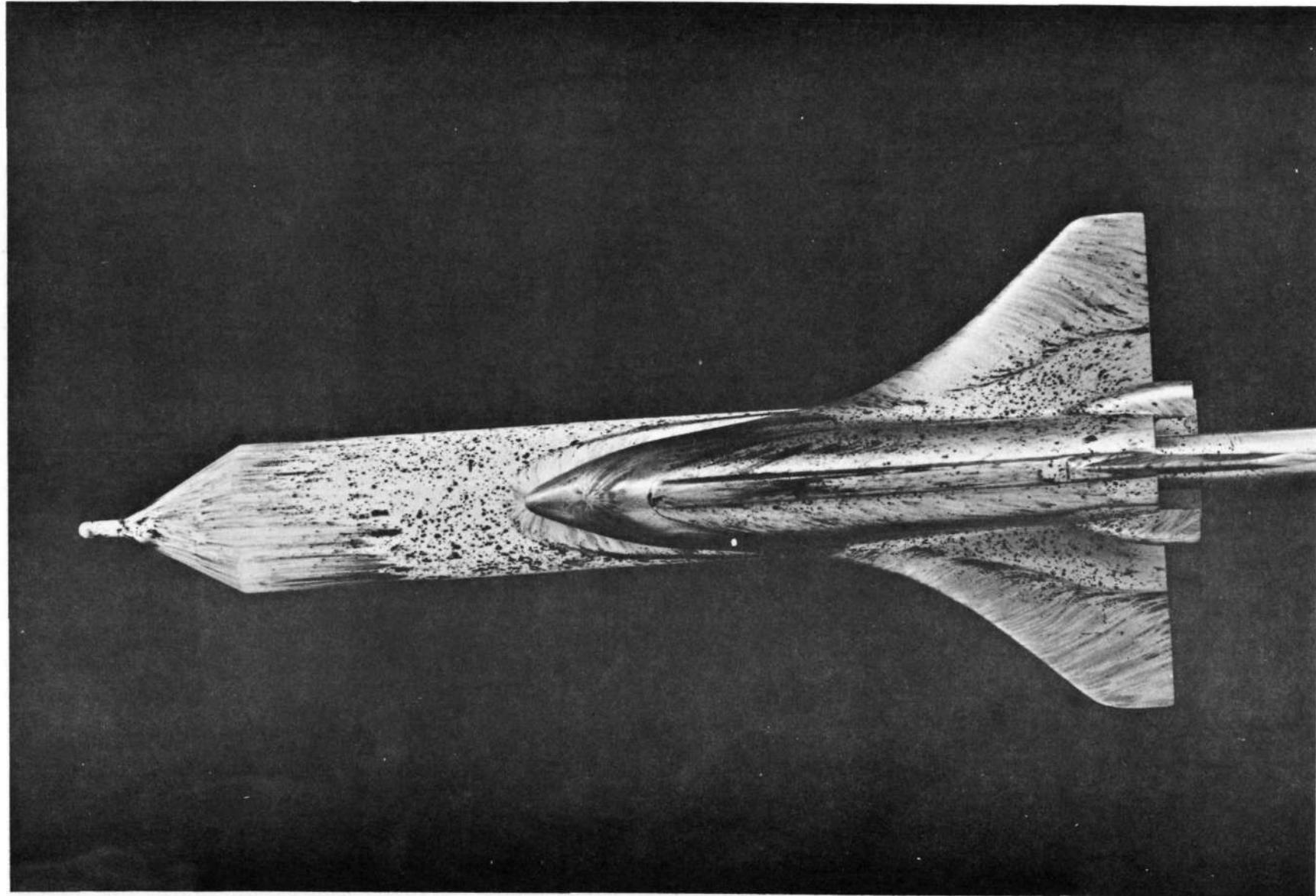
Figure 8. - Photograph of Oil Flow Pattern After Tunnel Shutdown on the .0045 Scale NR (ATP) Orbiter at $M = 20.3$ and $\alpha = 51^\circ$; $\delta_e = -40^\circ$.



A) Side view

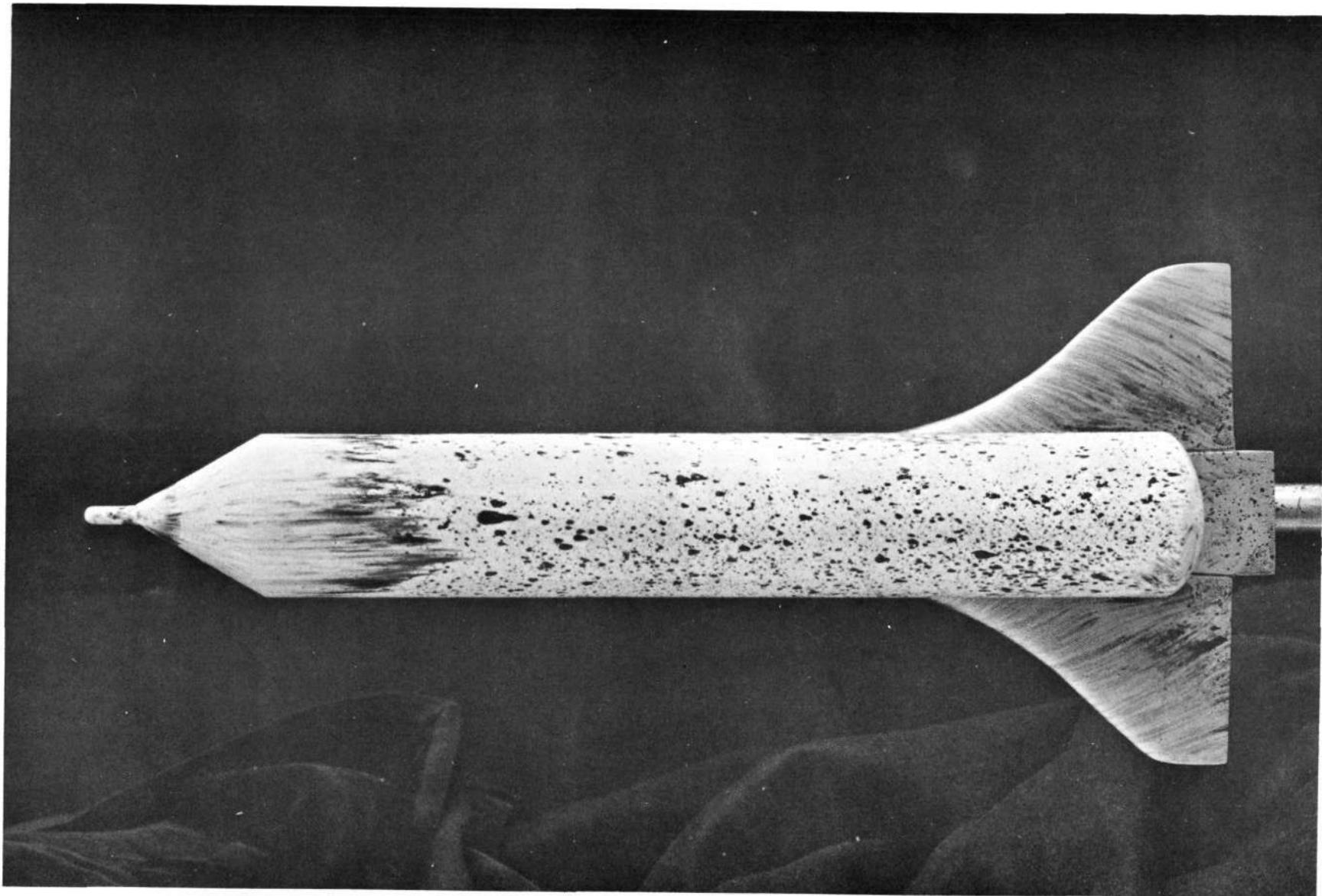
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Figure 9. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = 0^\circ$.



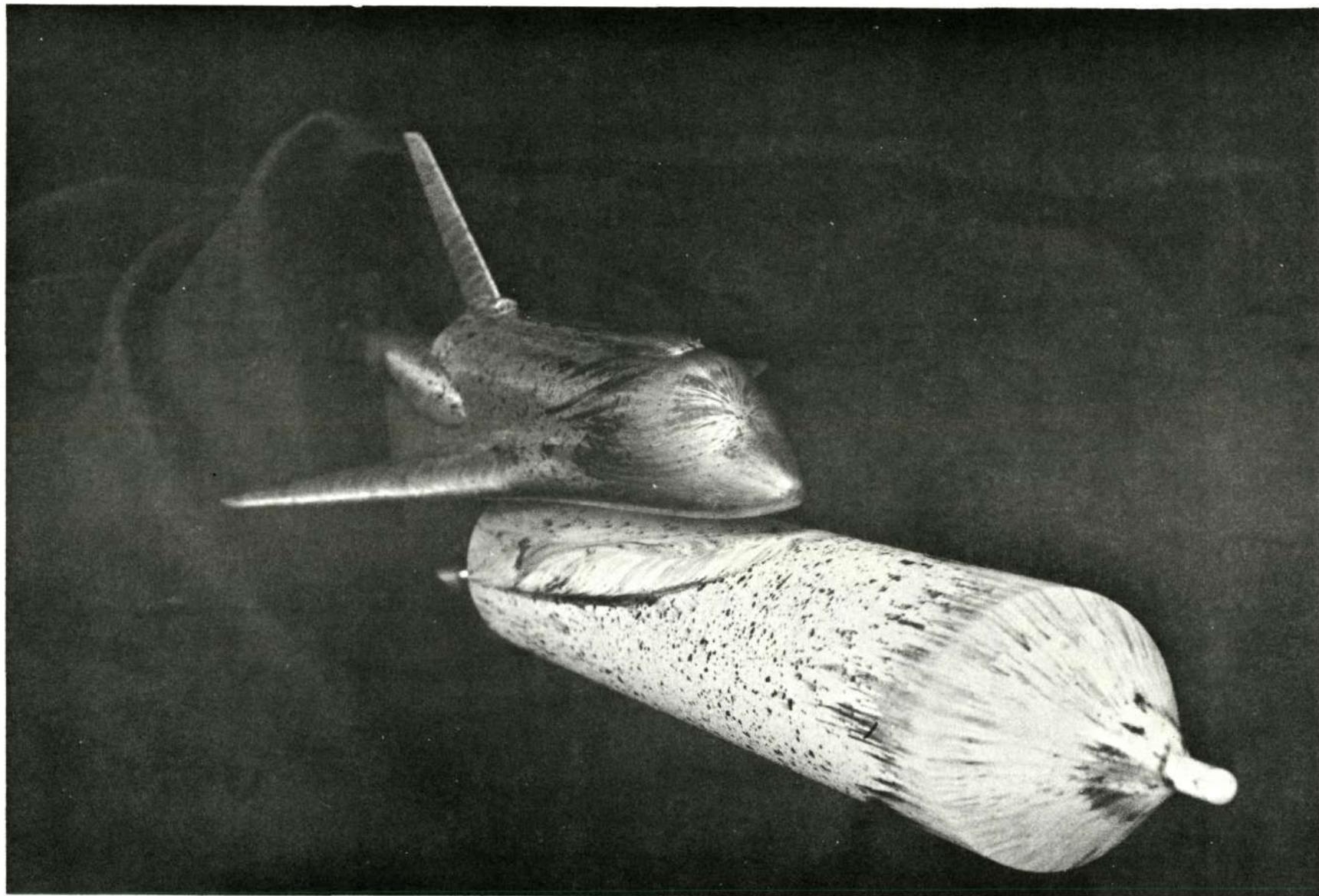
B) Top view

Figure 9. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = 0^\circ$.



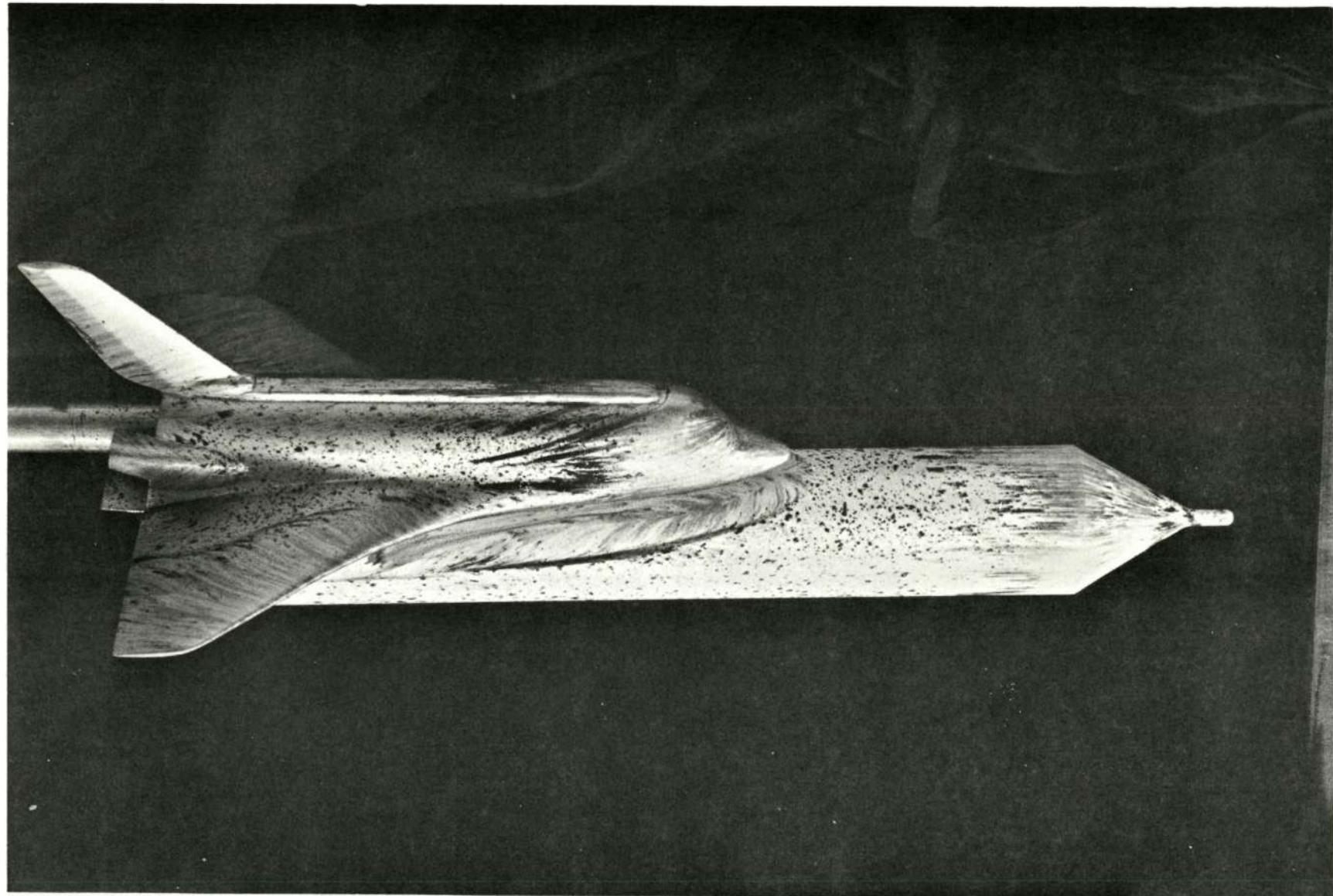
c) Bottom view

Figure 9. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = 0^\circ$.



D) Oblique front side view

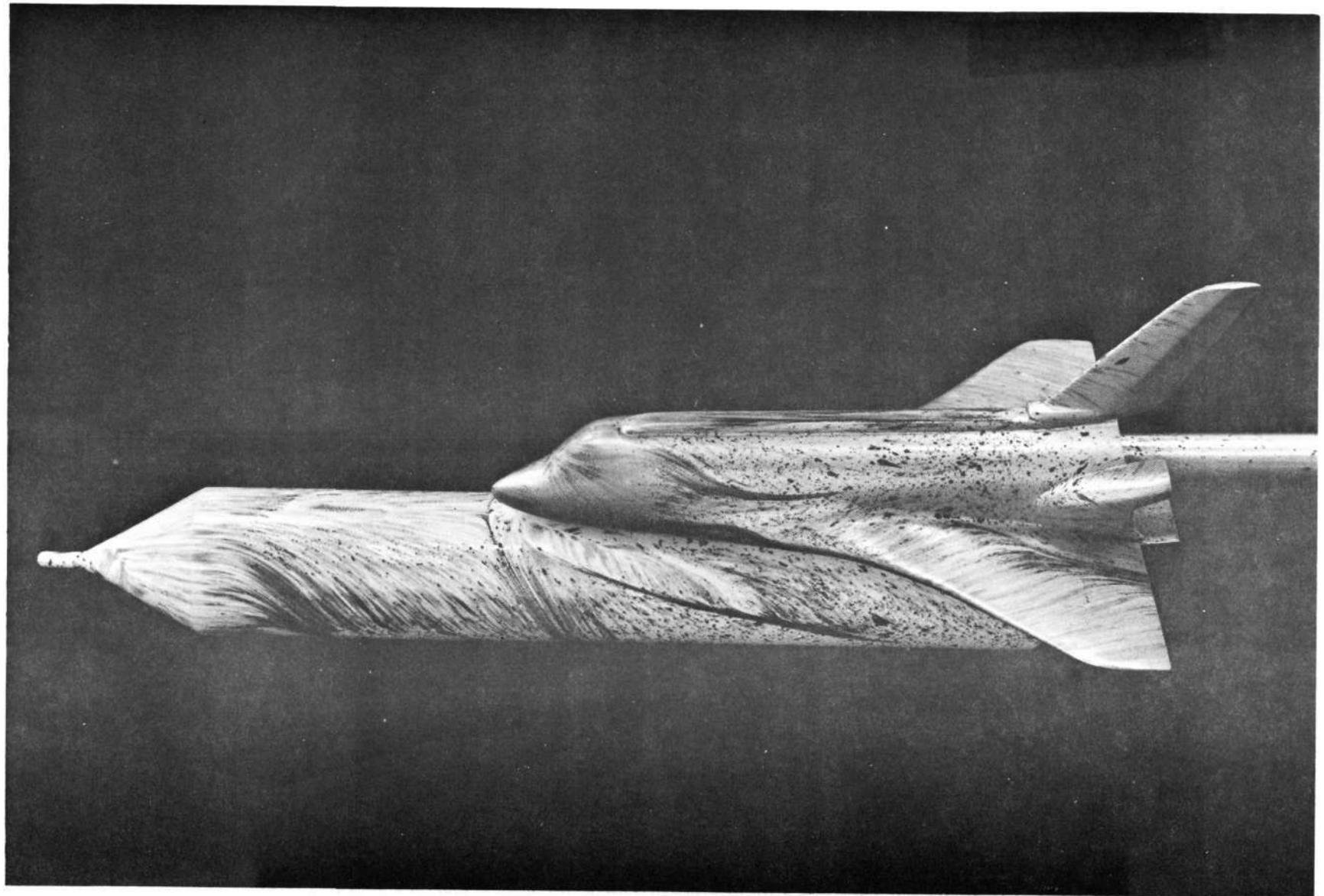
Figure 9. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = 0^\circ$.



E) Oblique top side view

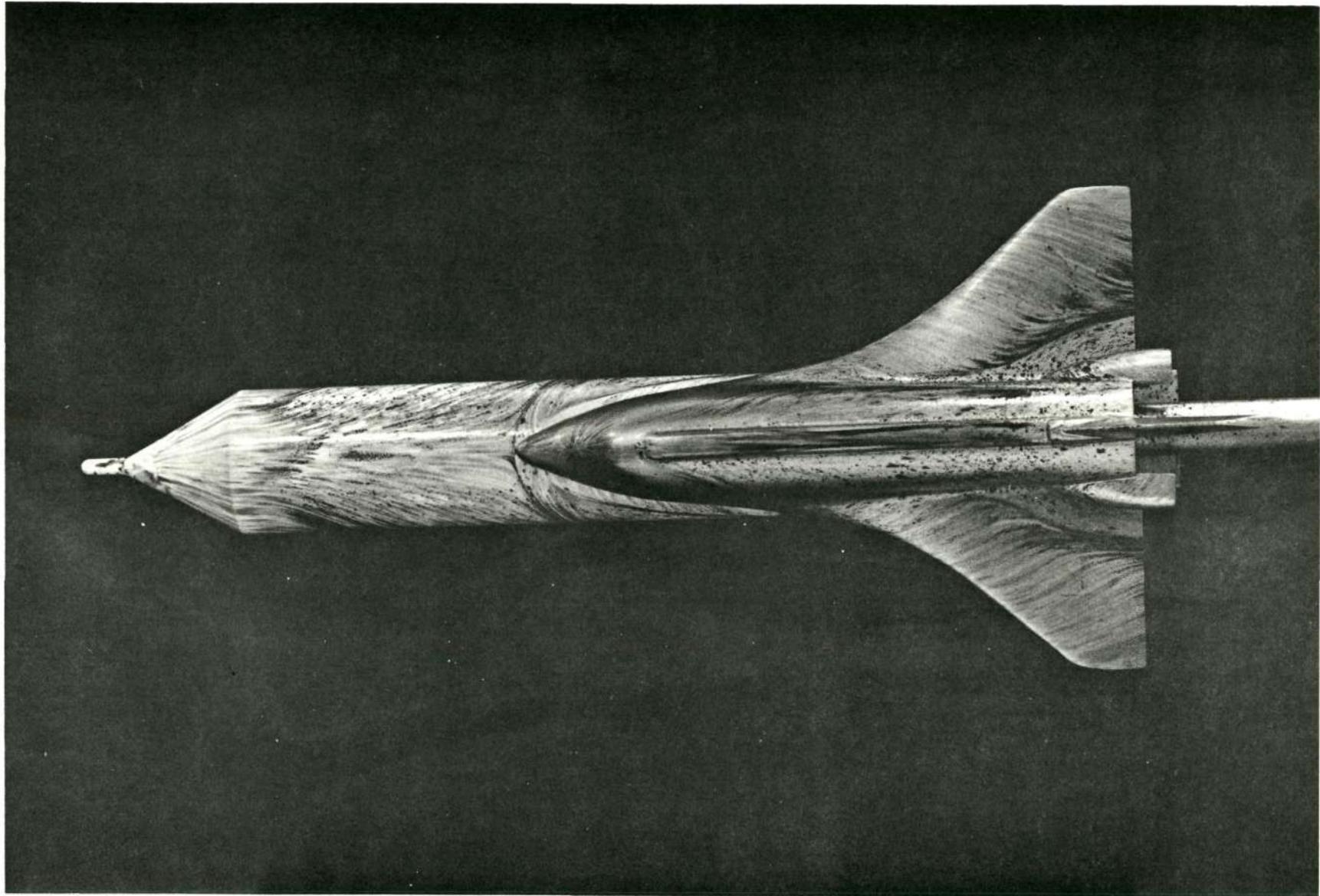
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best available copy.

Figure 9. - Photograph of Oil Flow Pattern After Removal from Tunnel on a
.0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$
and $\alpha = 0^\circ$.



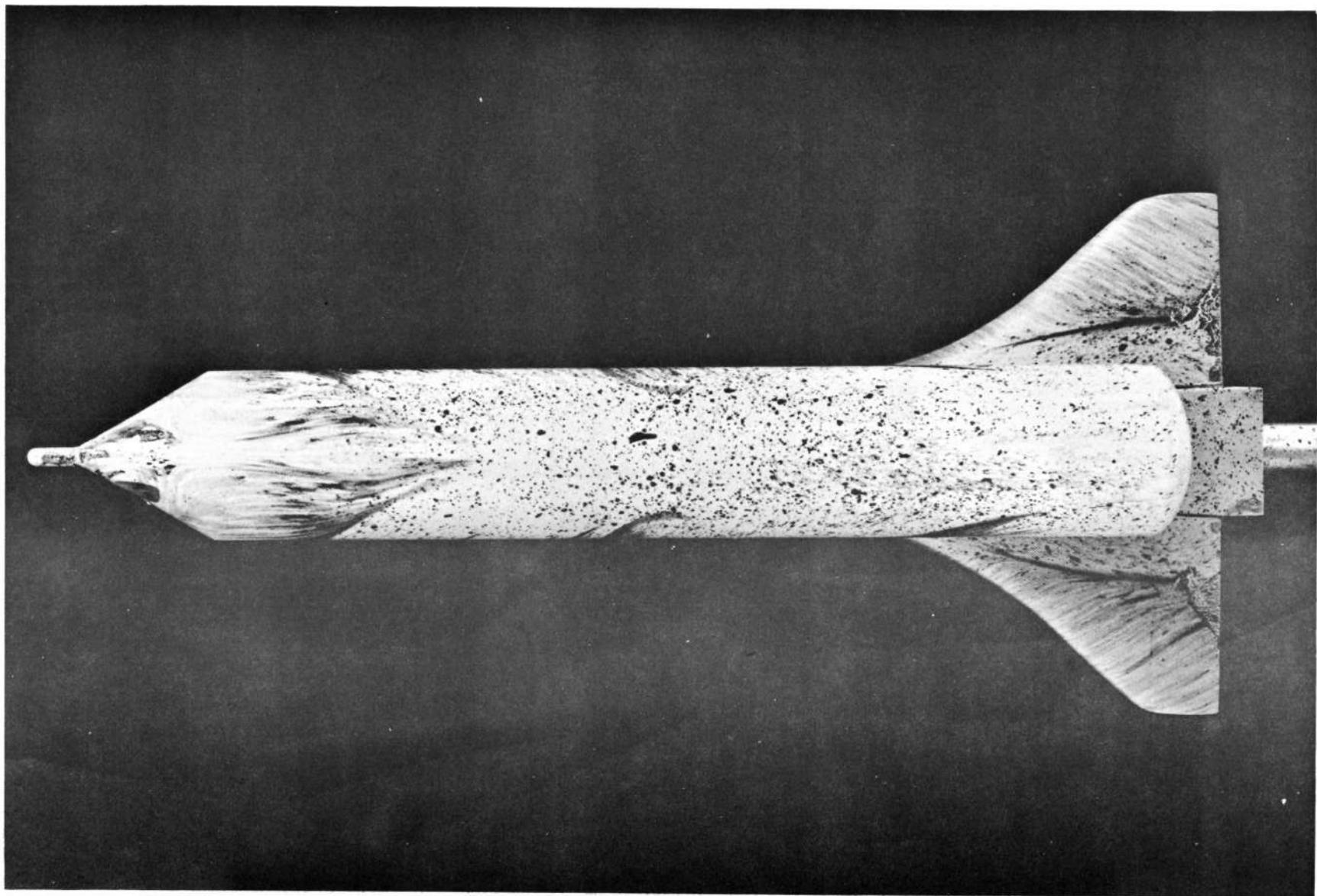
A) Side view (rolled)

Figure 10. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = -5^\circ$.



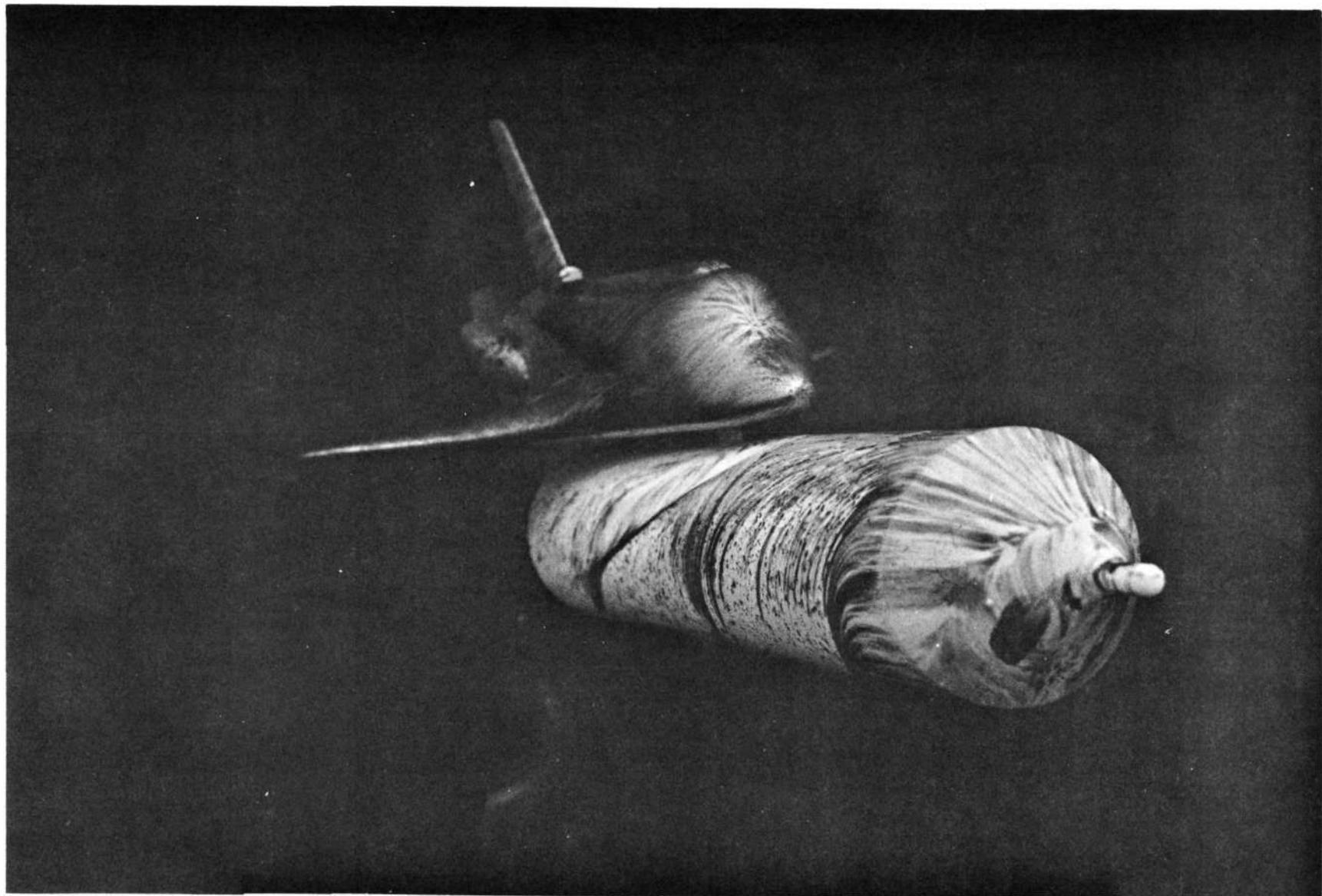
B) Top view

Figure 10. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = -5^\circ$.



c) Bottom view

Figure 10. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = -5^\circ$.



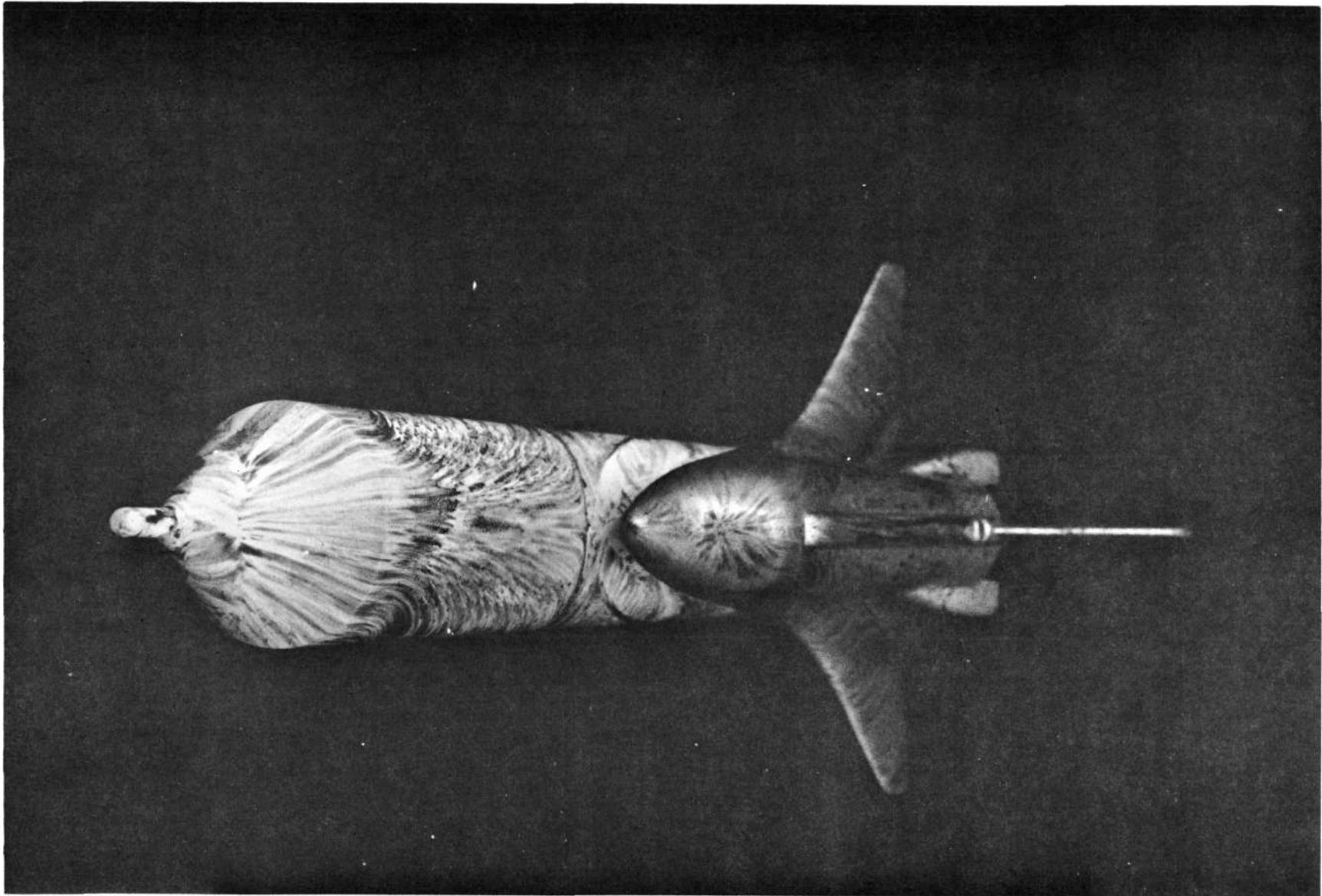
D) Front oblique view

Figure 10. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = -5^\circ$.



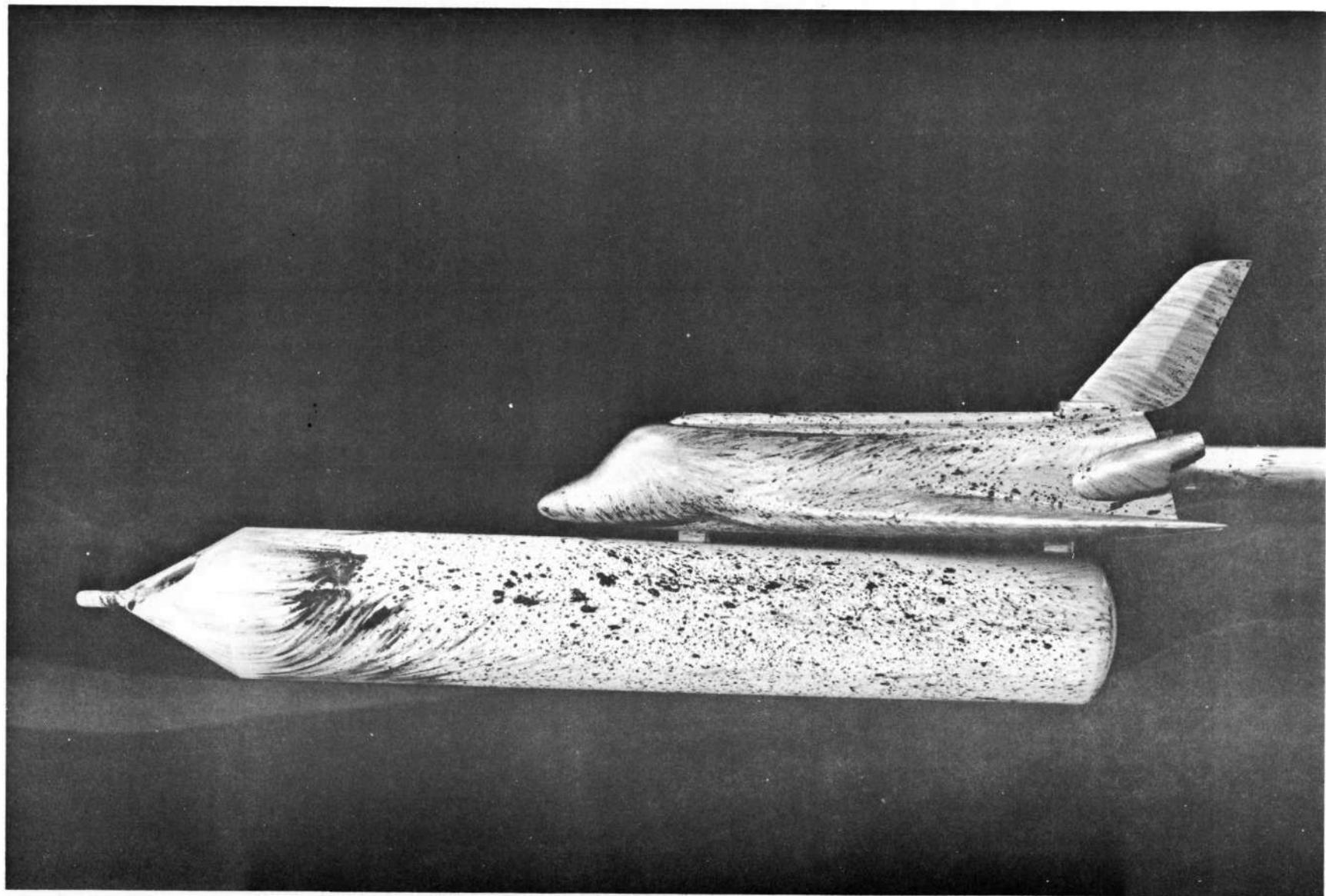
E) Top-side oblique view

Figure 10. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = -5^\circ$.



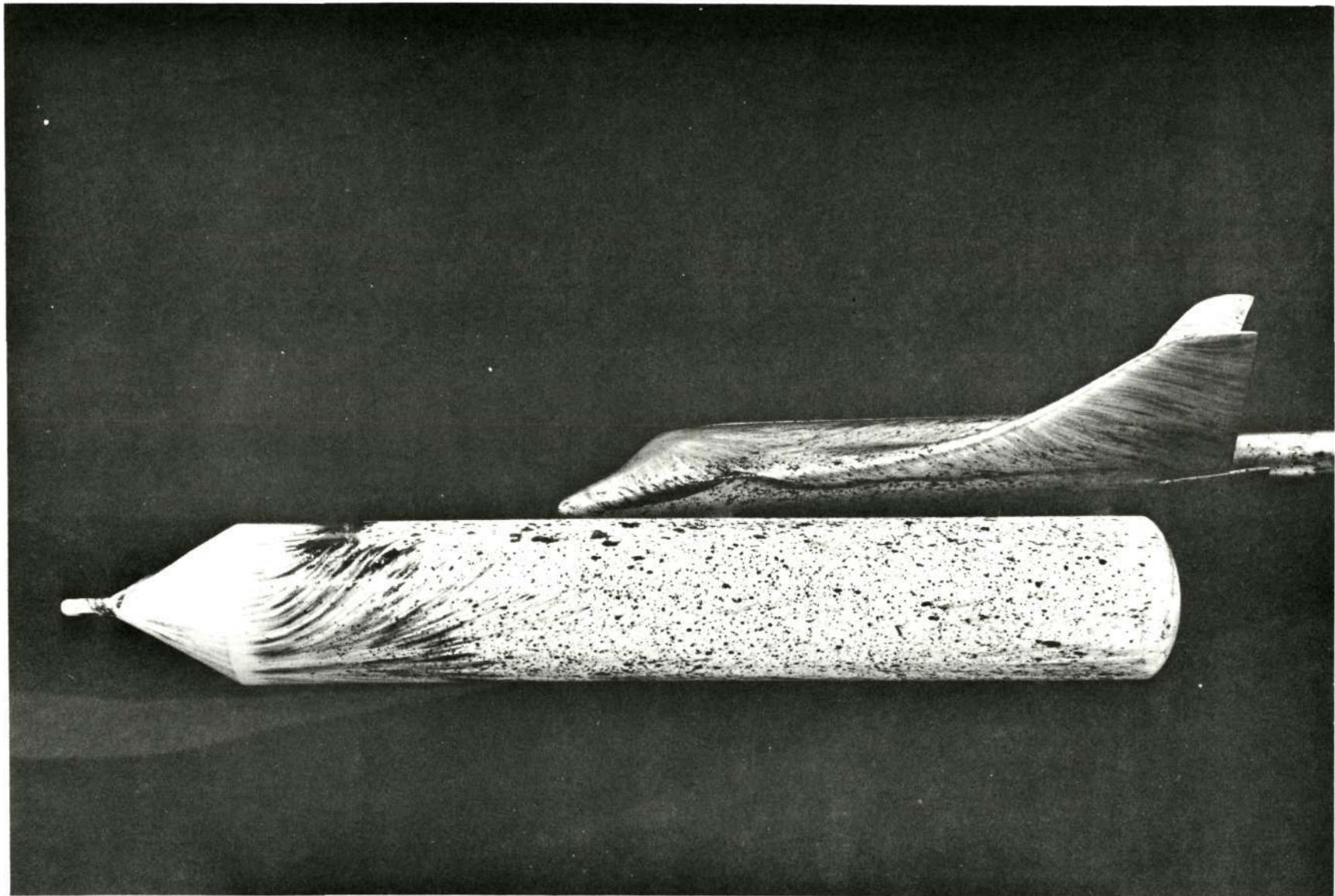
F) Top oblique view

Figure 10. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = -5^\circ$.



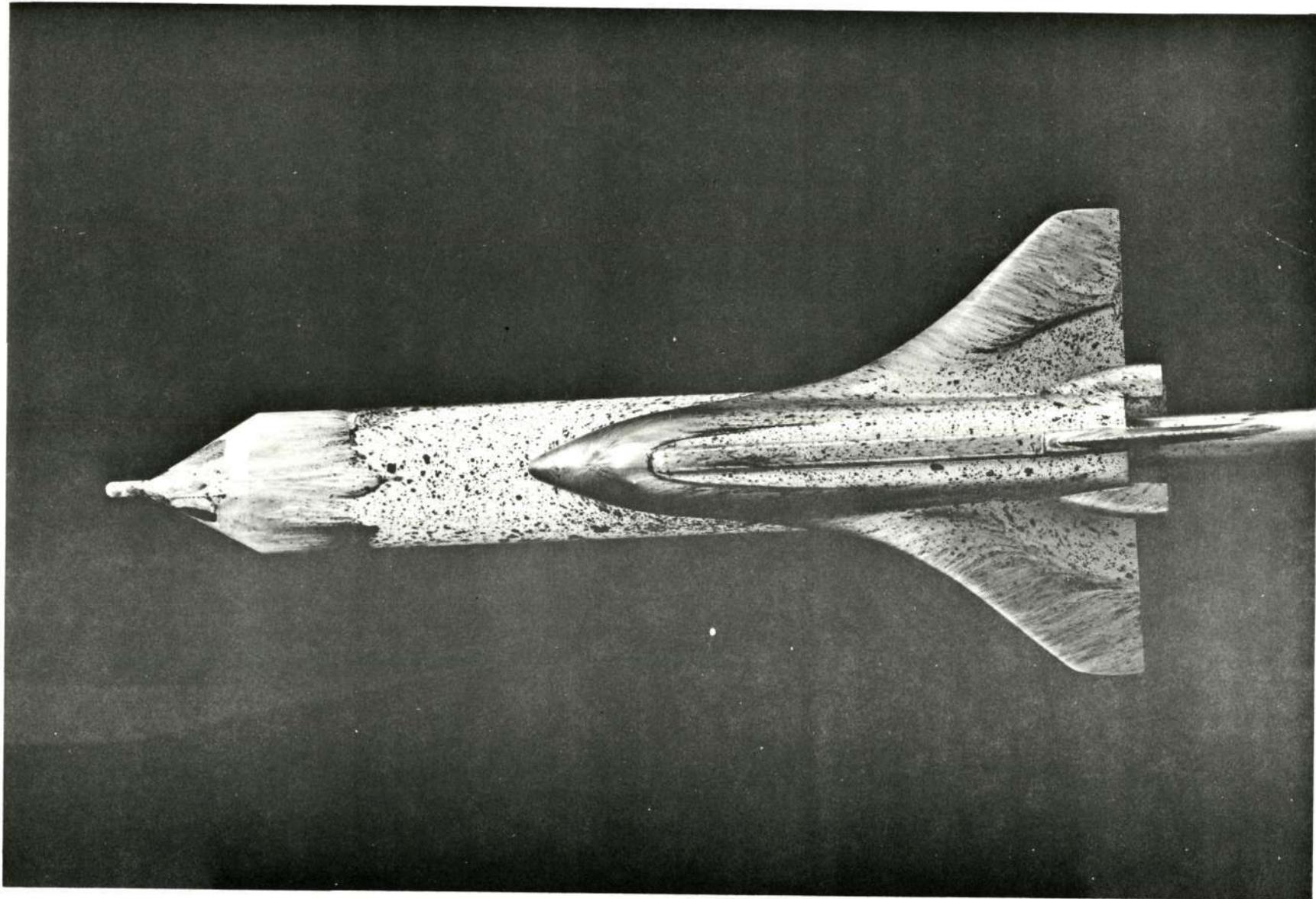
A) Side View

Figure 11. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = +5^\circ$.



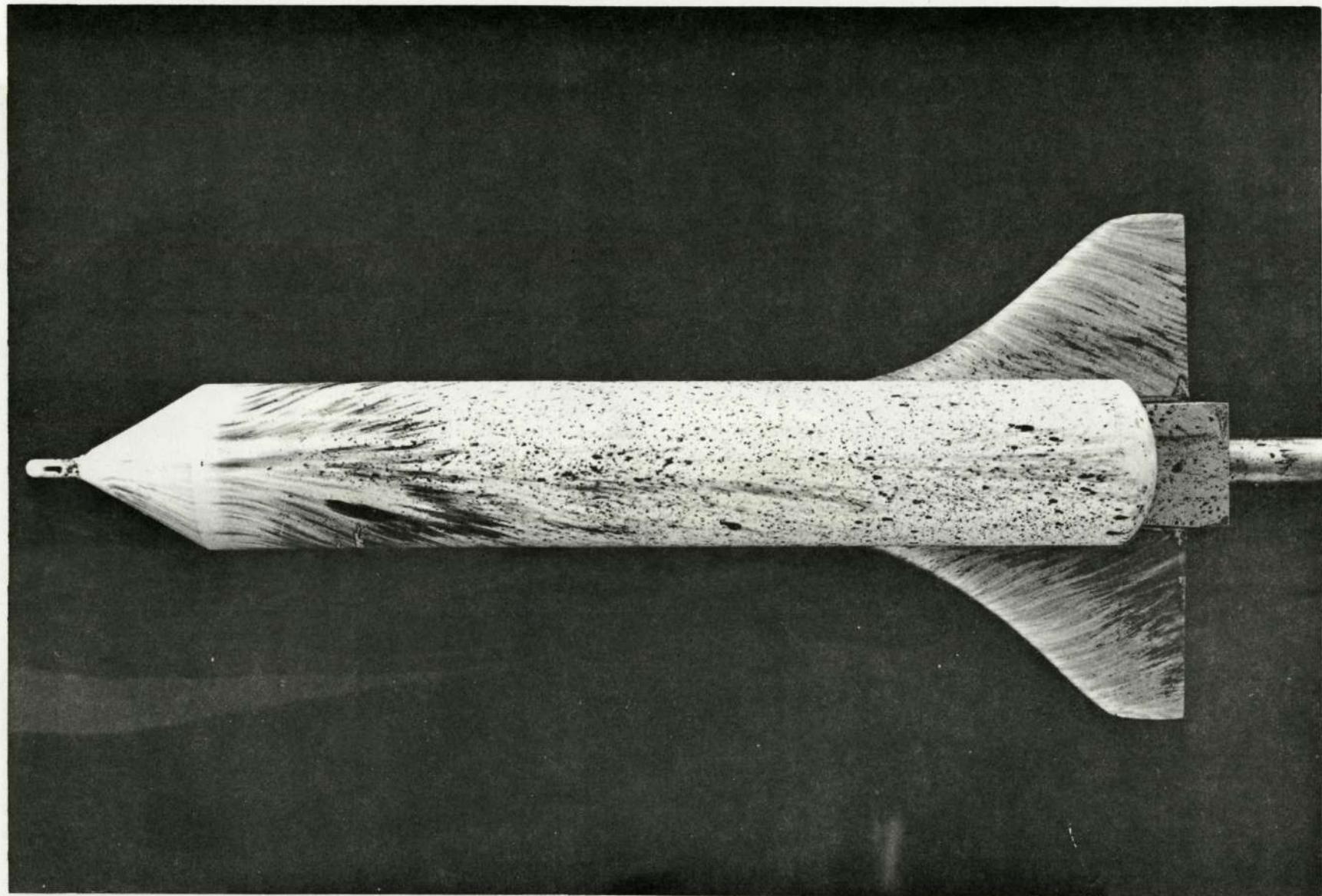
B) Side view (rolled)

Figure 11. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = +5^\circ$.



C) Top view

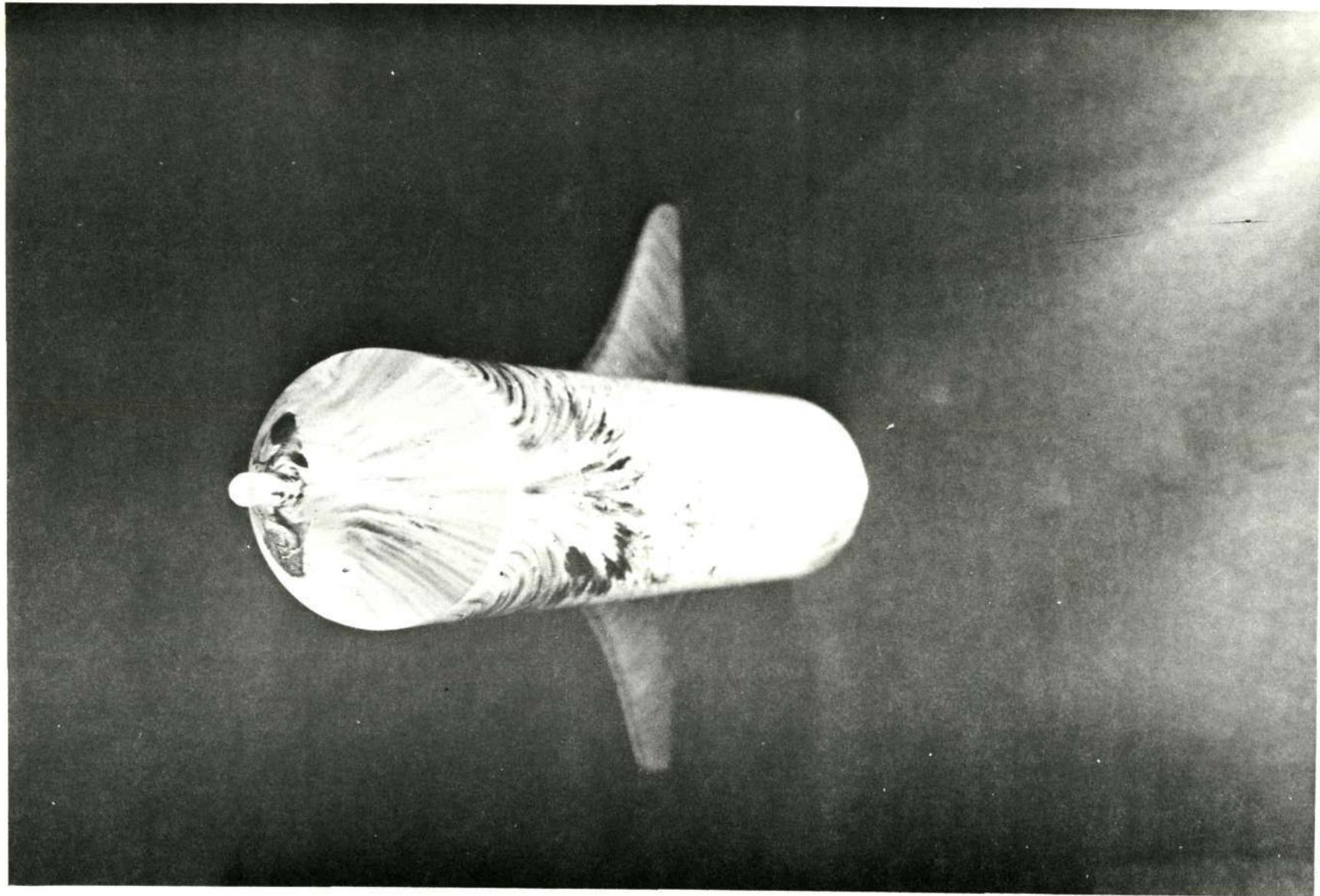
Figure 11. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = +5^\circ$.



D) Bottom view

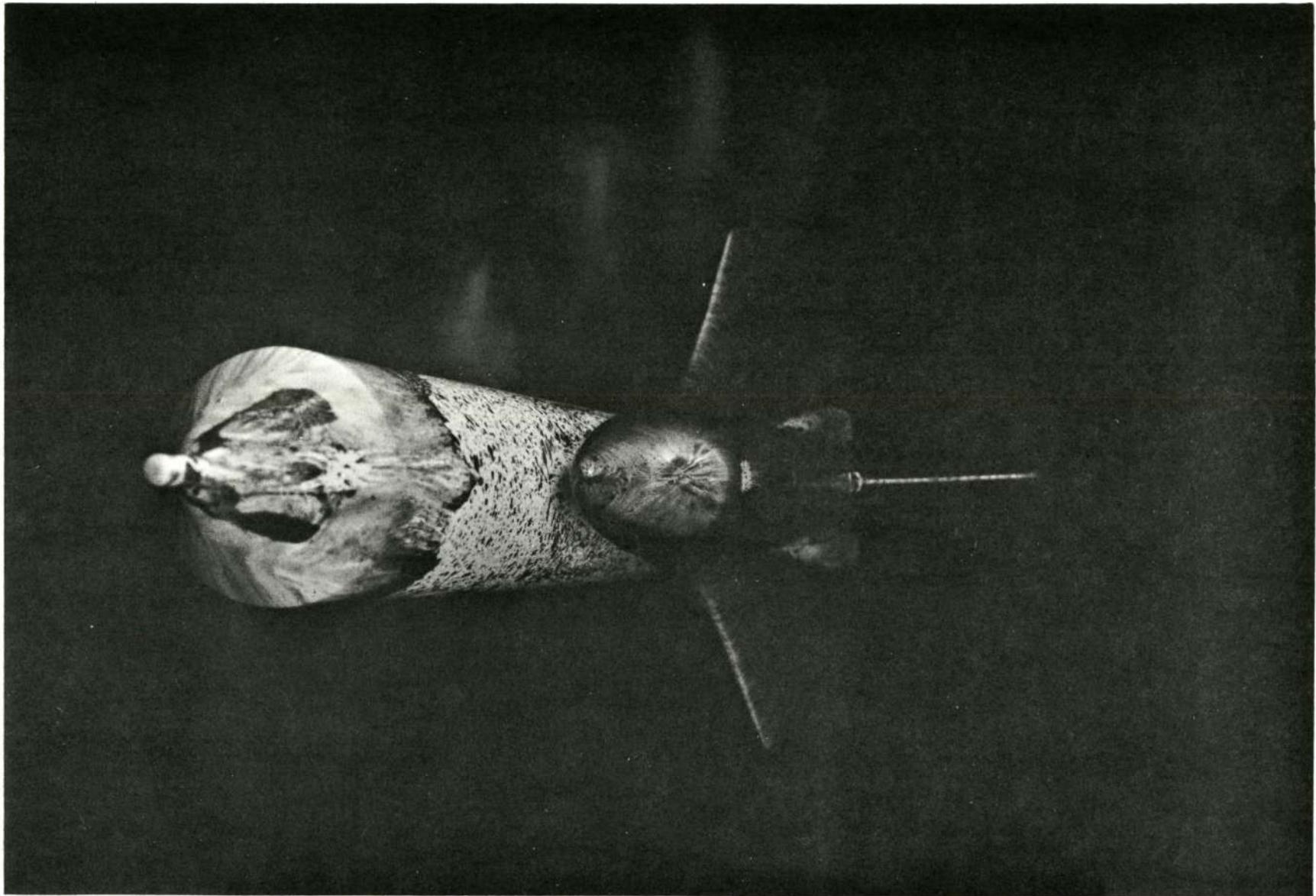
Figure 11. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = +5^\circ$.

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best available copy.



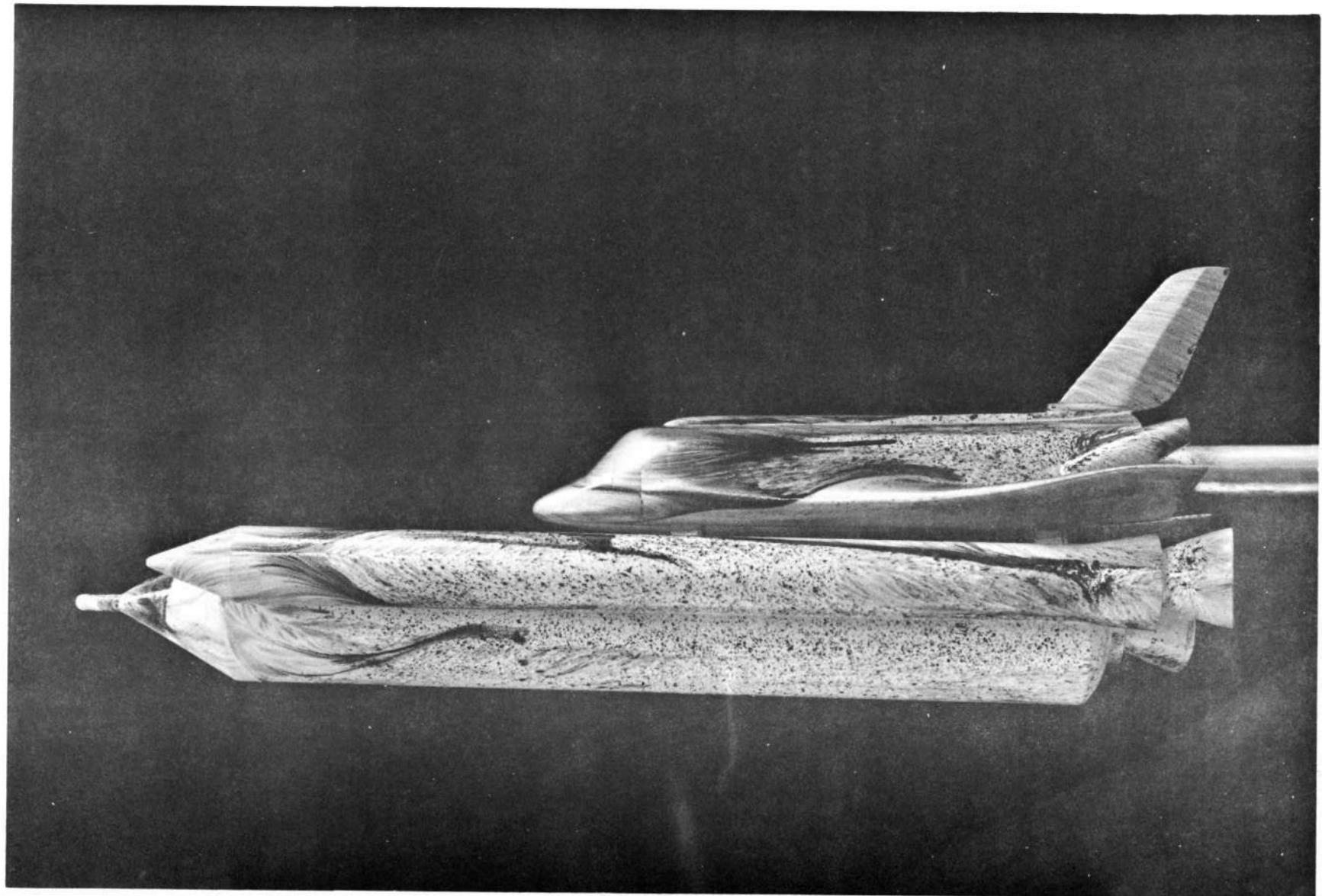
E) Front-lower surface view

Figure 11. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = +5^\circ$.



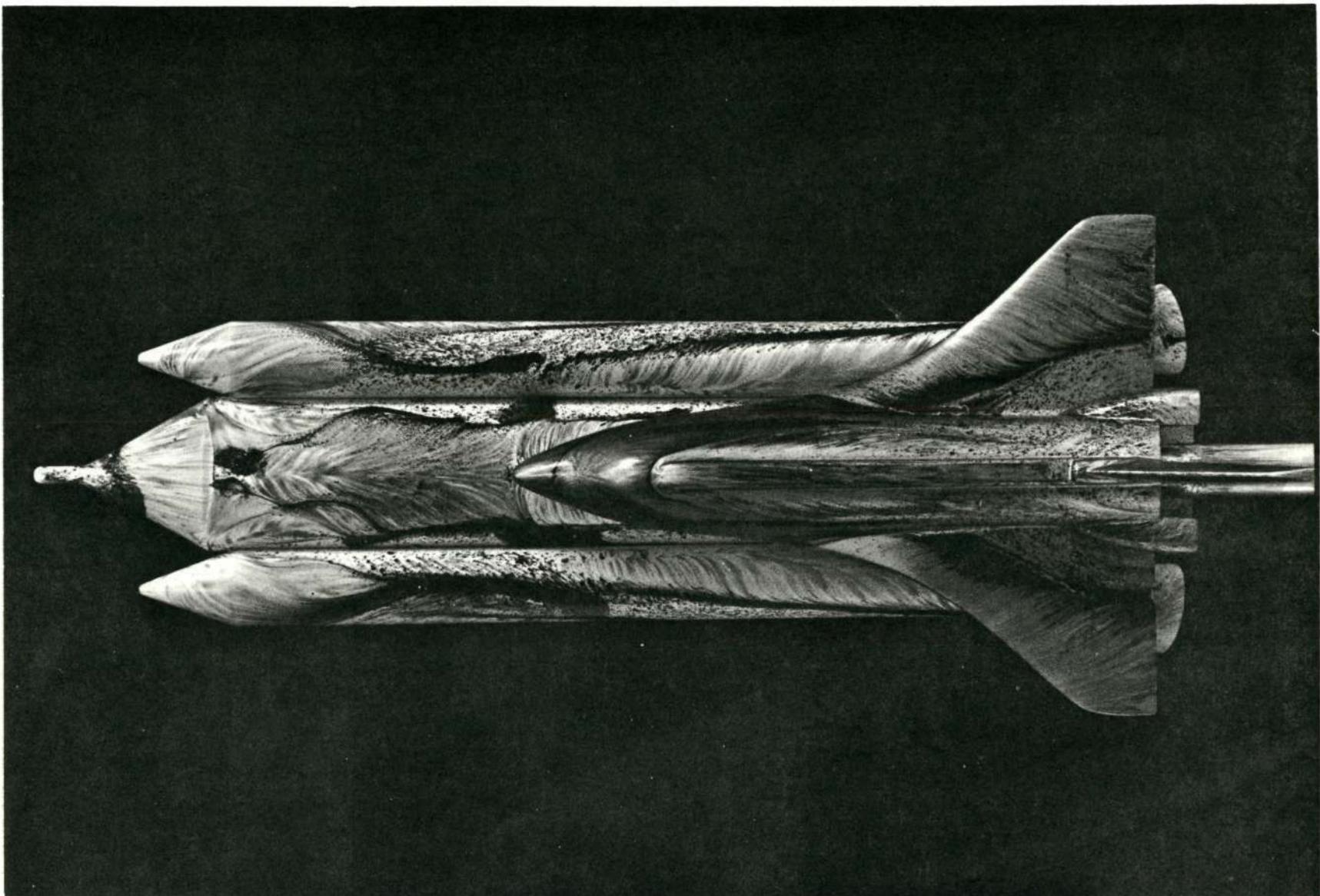
F) Top oblique view

Figure 11. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = +5^\circ$.



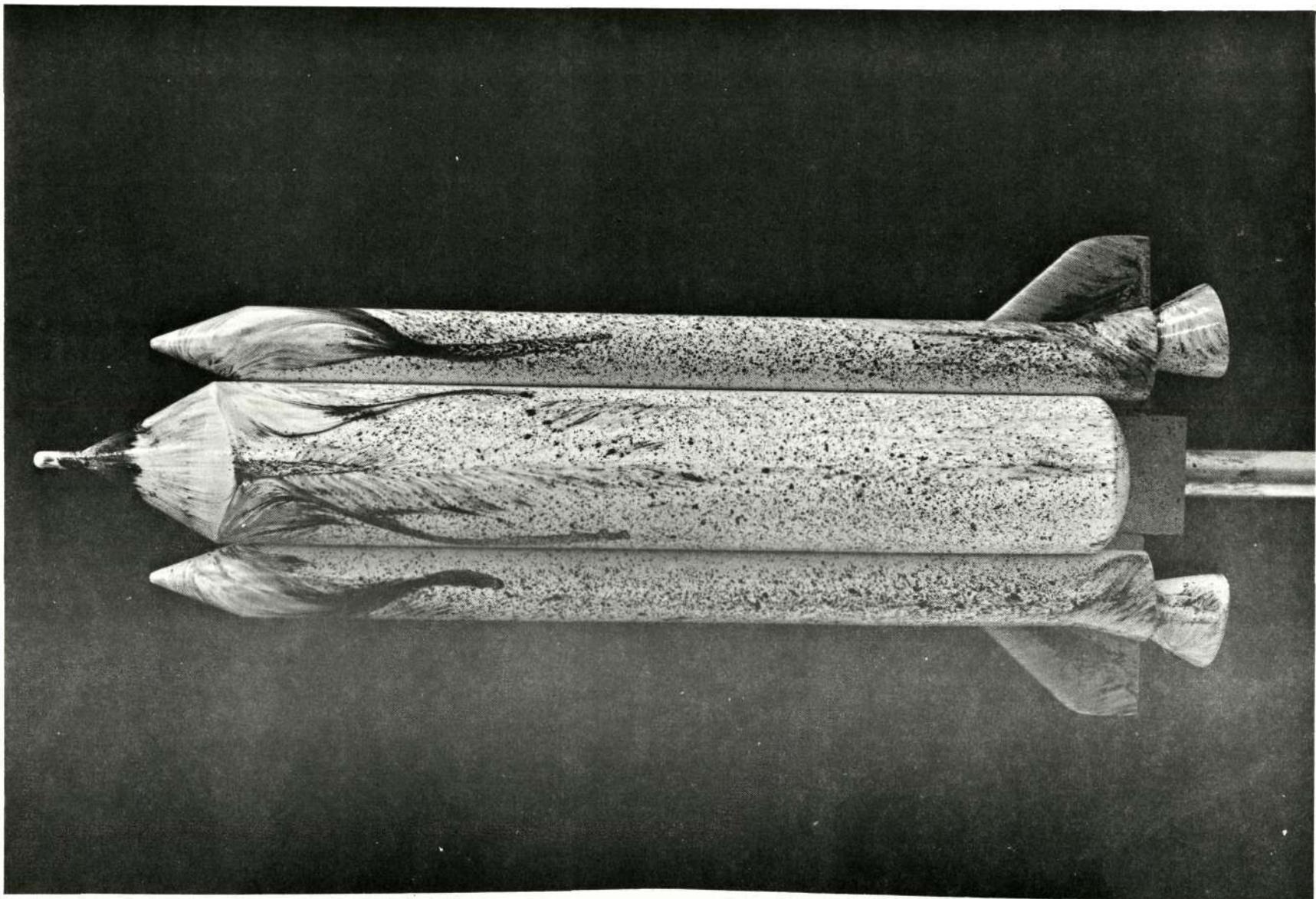
A) Left side view

Figure 12. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = 0^\circ$.



B) Top view

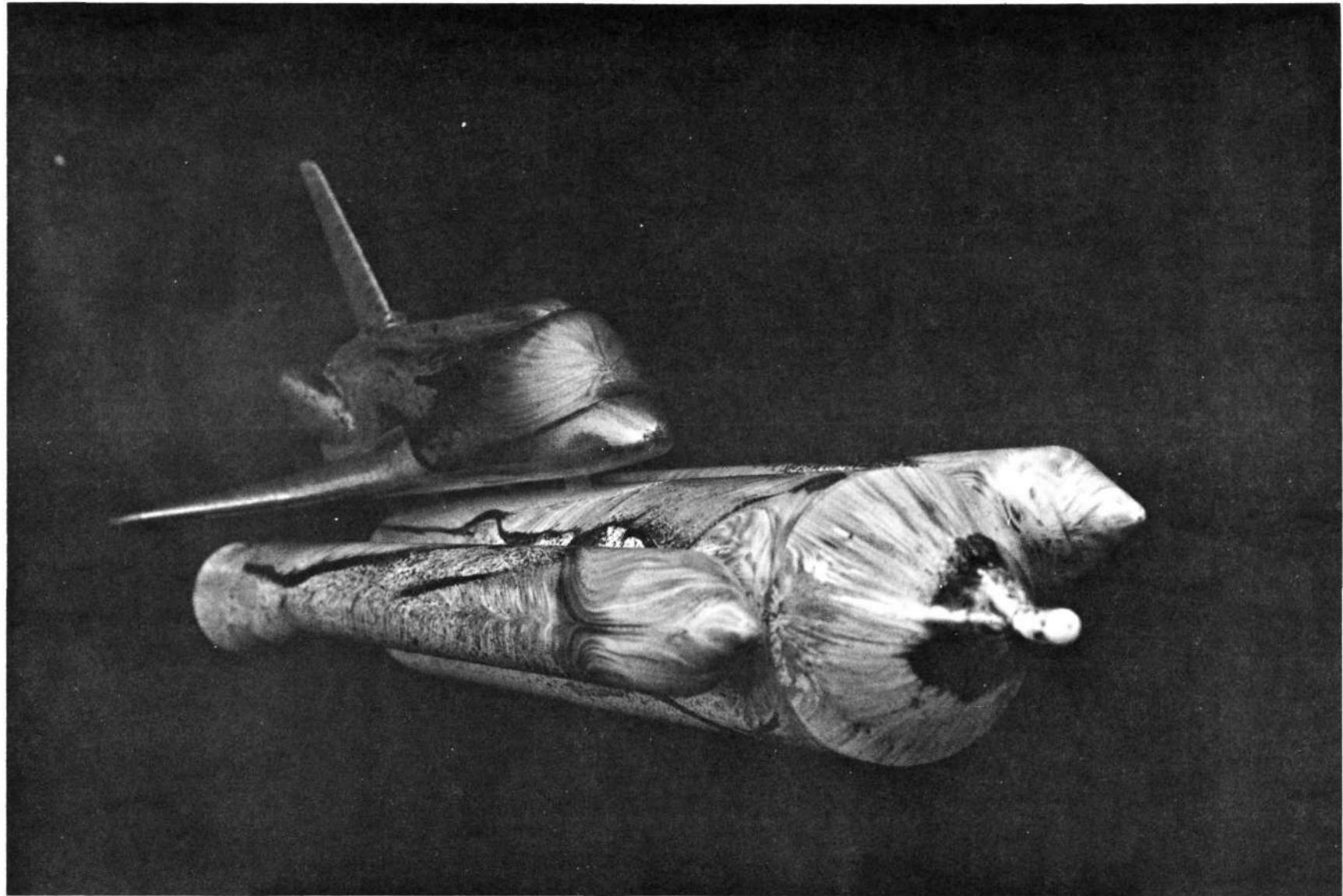
Figure 12. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = 0^\circ$.



c) Bottom view

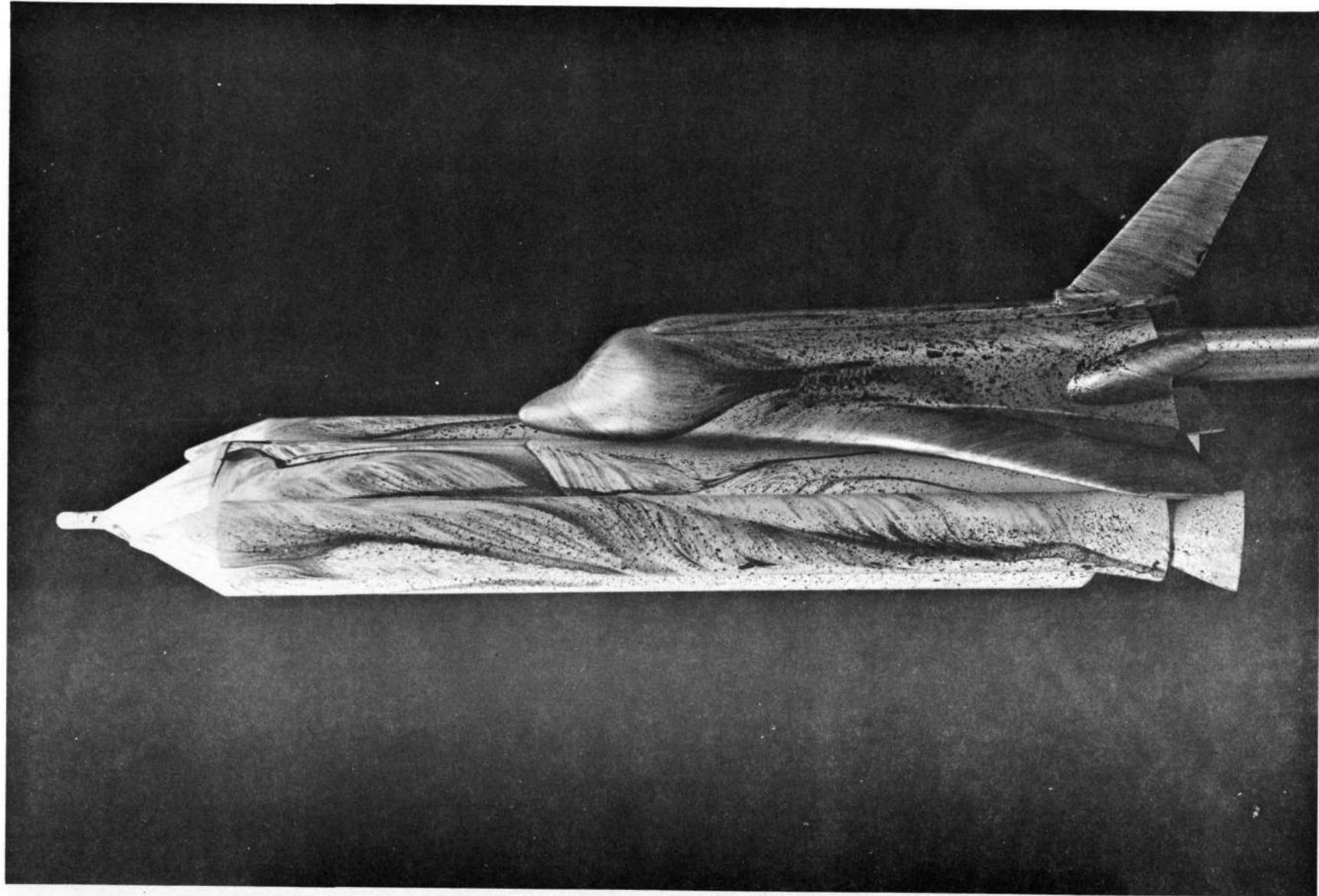
Figure 12. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = 0^\circ$.

Reproduced from
best available
copy.



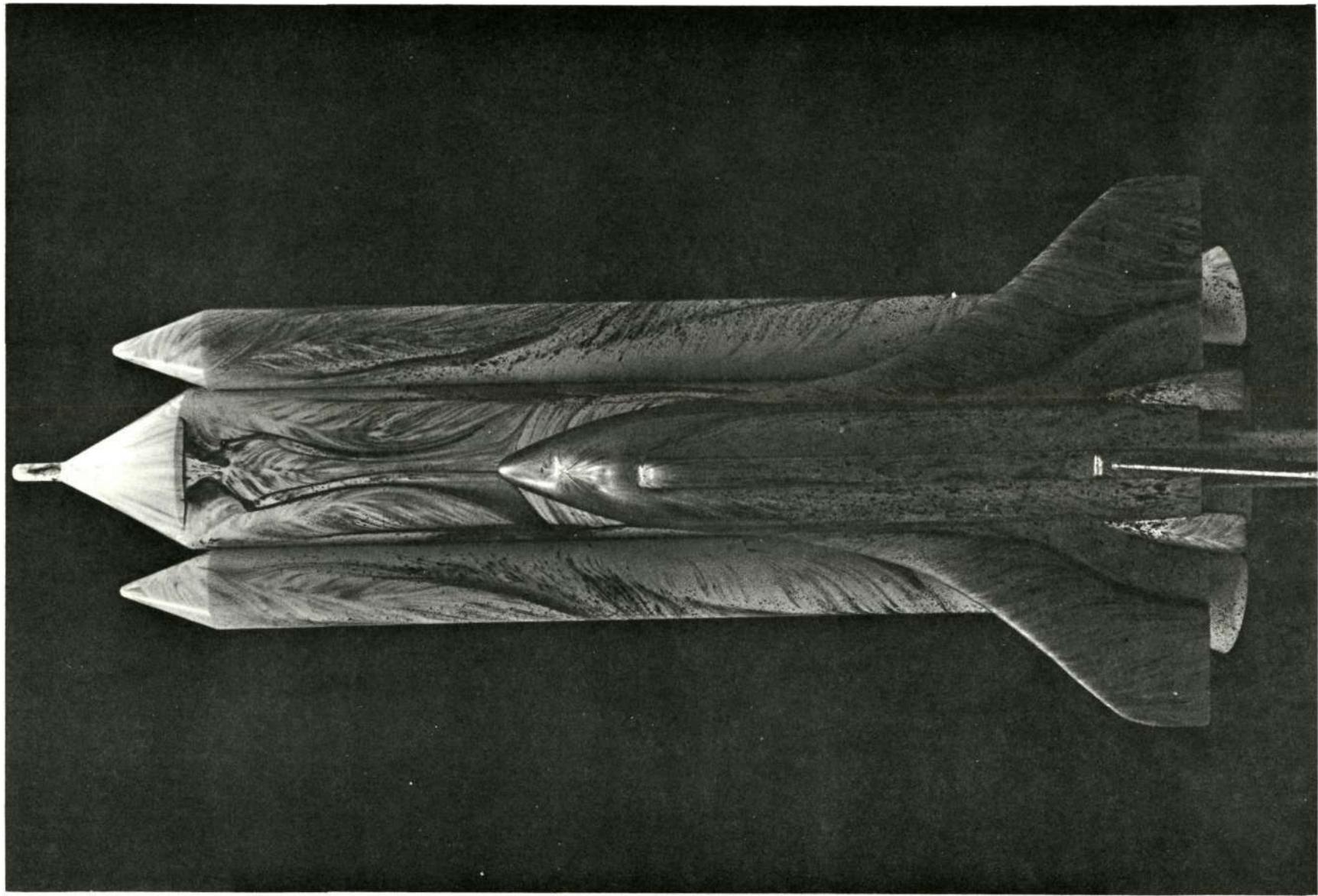
D) Front oblique view

Figure 12. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = 0^\circ$.



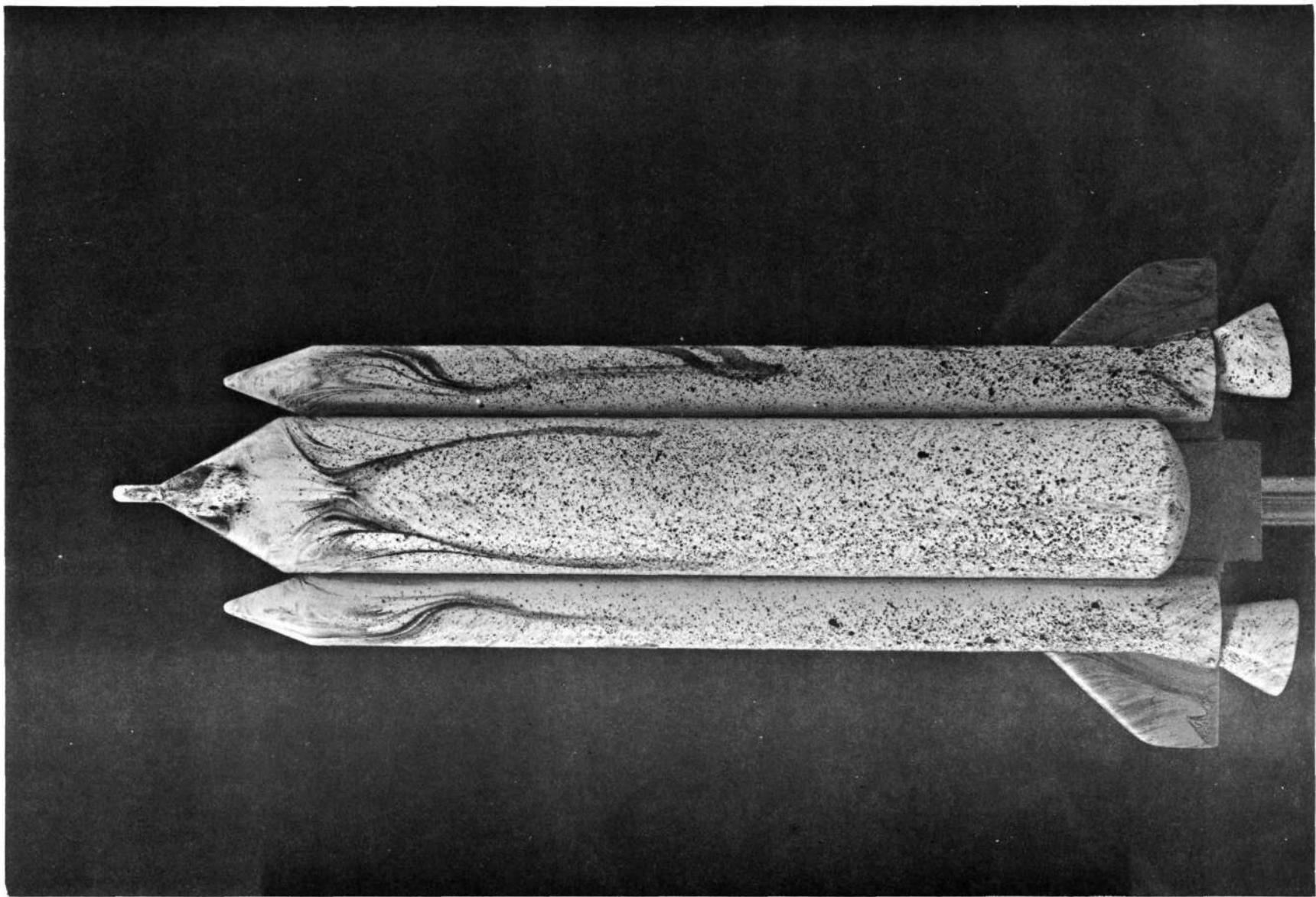
A) Left side view (rolled)

Figure 13. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = -5^\circ$.



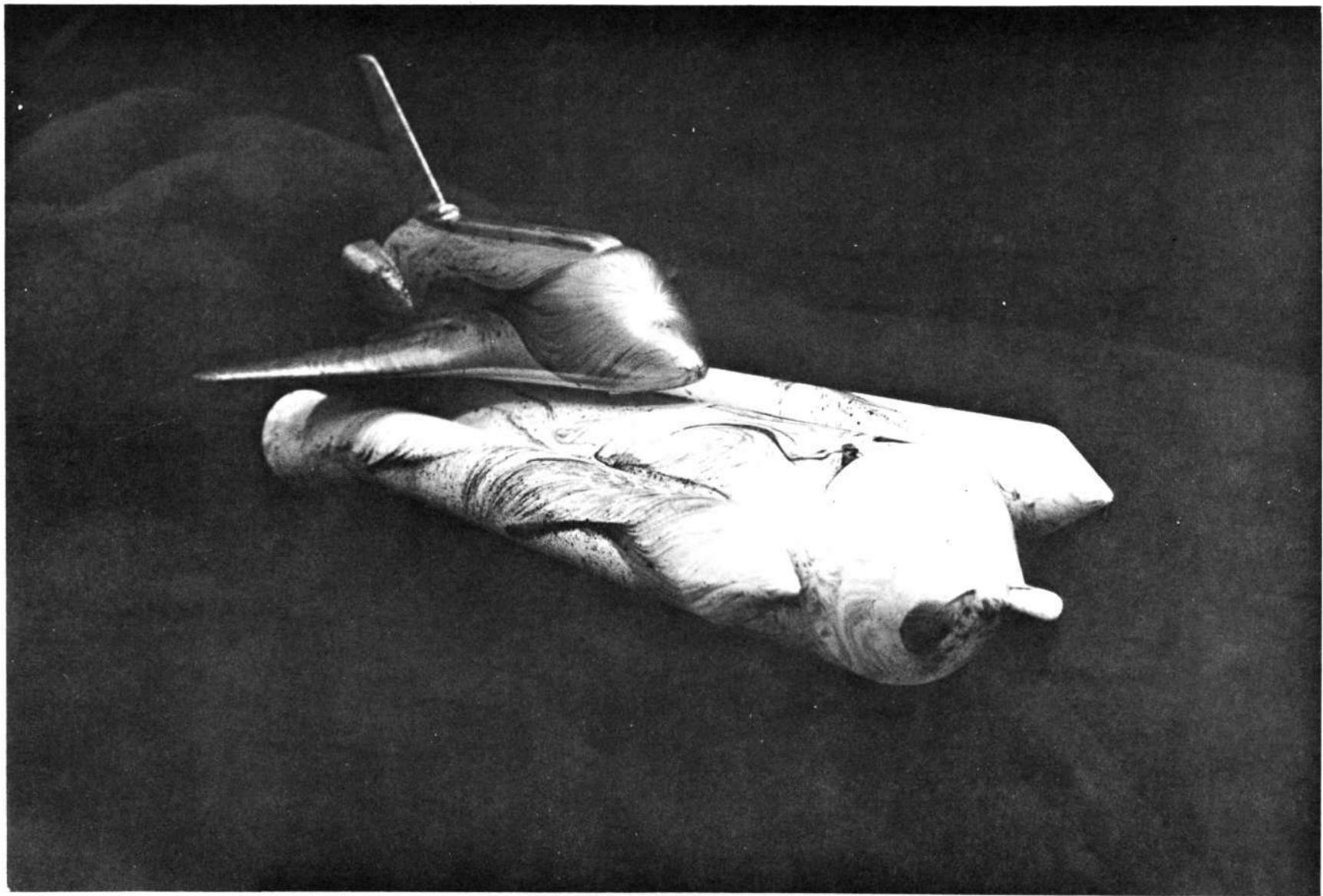
B) Top view

Figure 13. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = -5^\circ$.



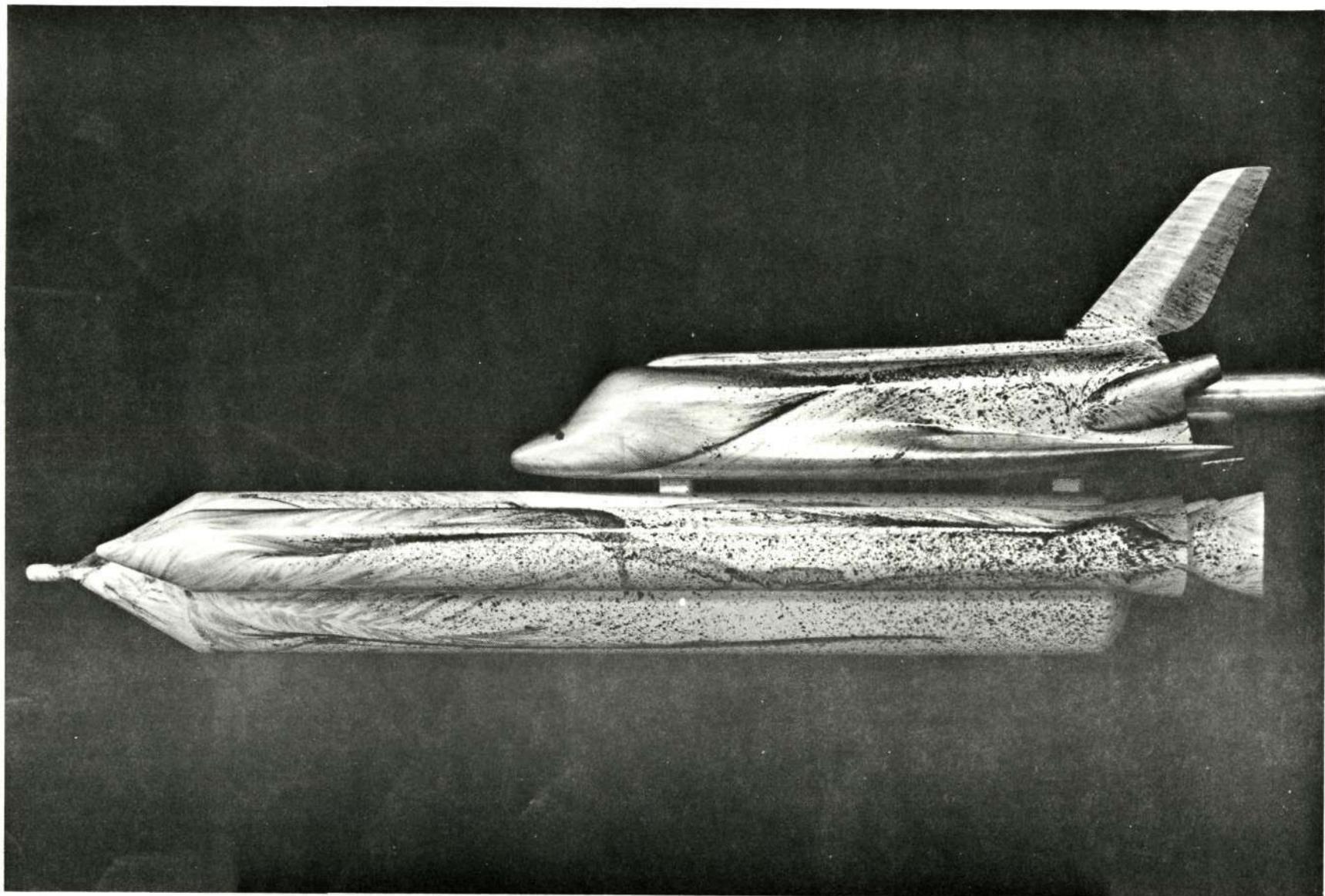
C) Bottom view

Figure 13. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = -5^\circ$.



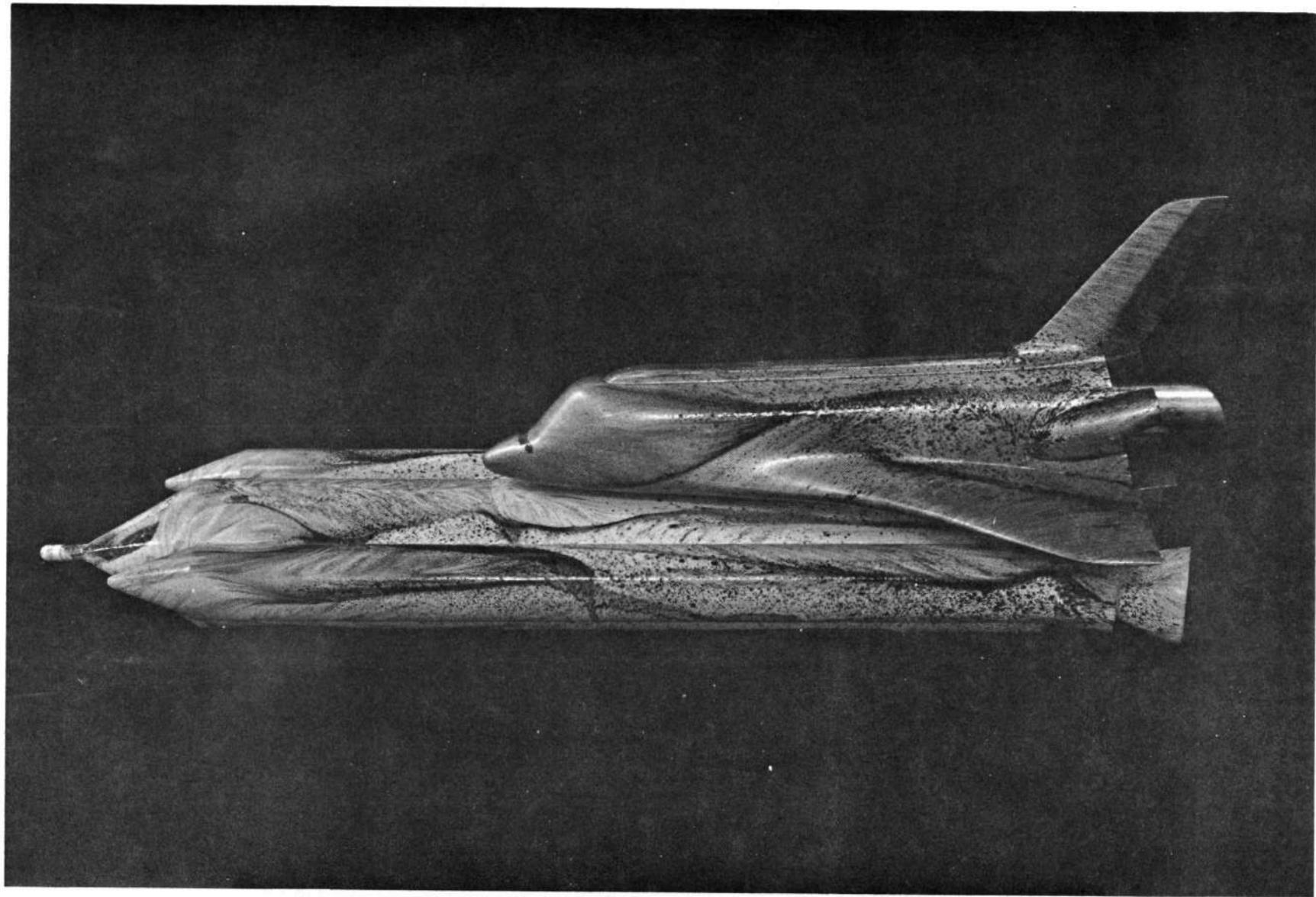
D) Front oblique view

Figure 13. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = -5^\circ$.



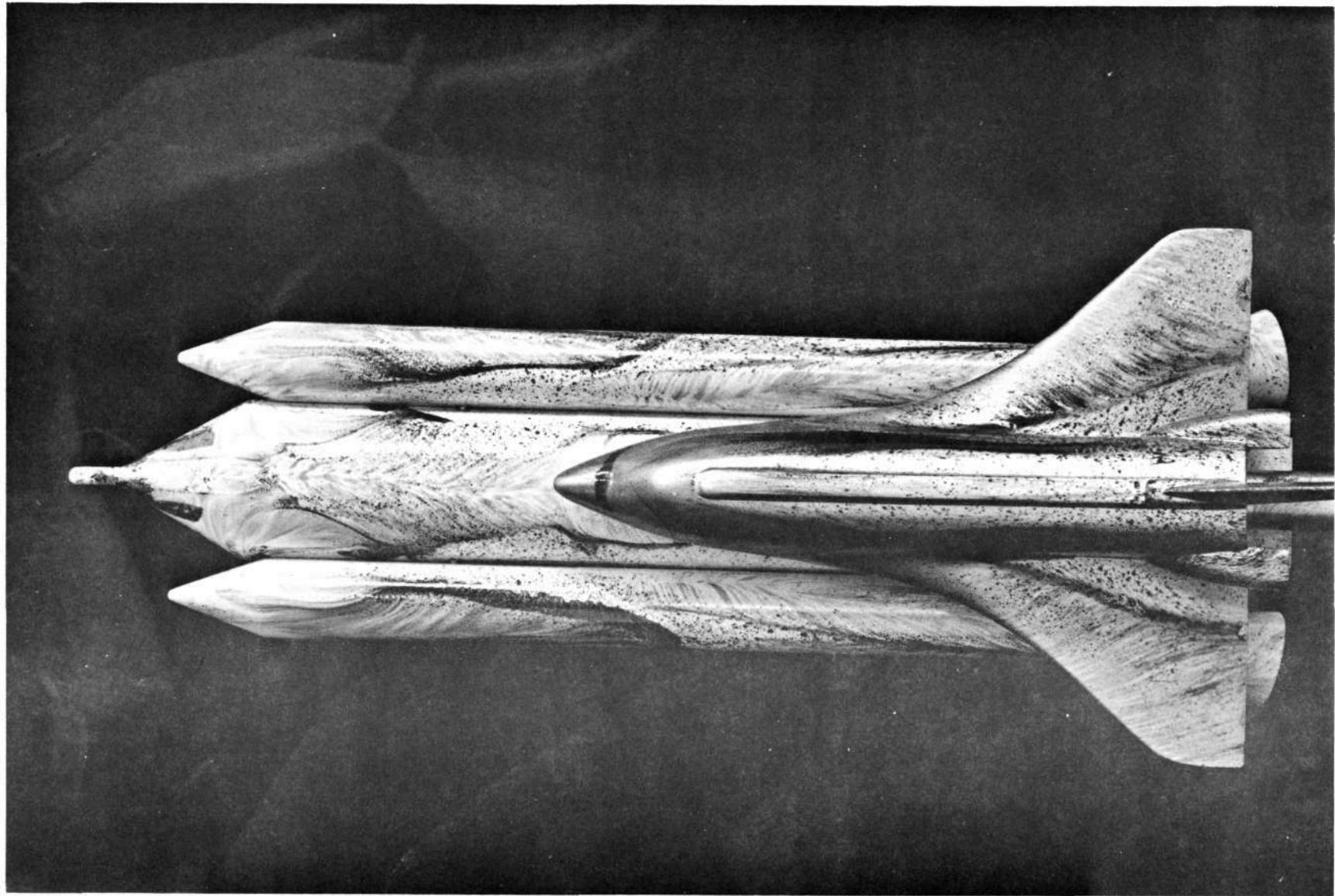
A): Left side view

Figure 14. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = +5^\circ$.



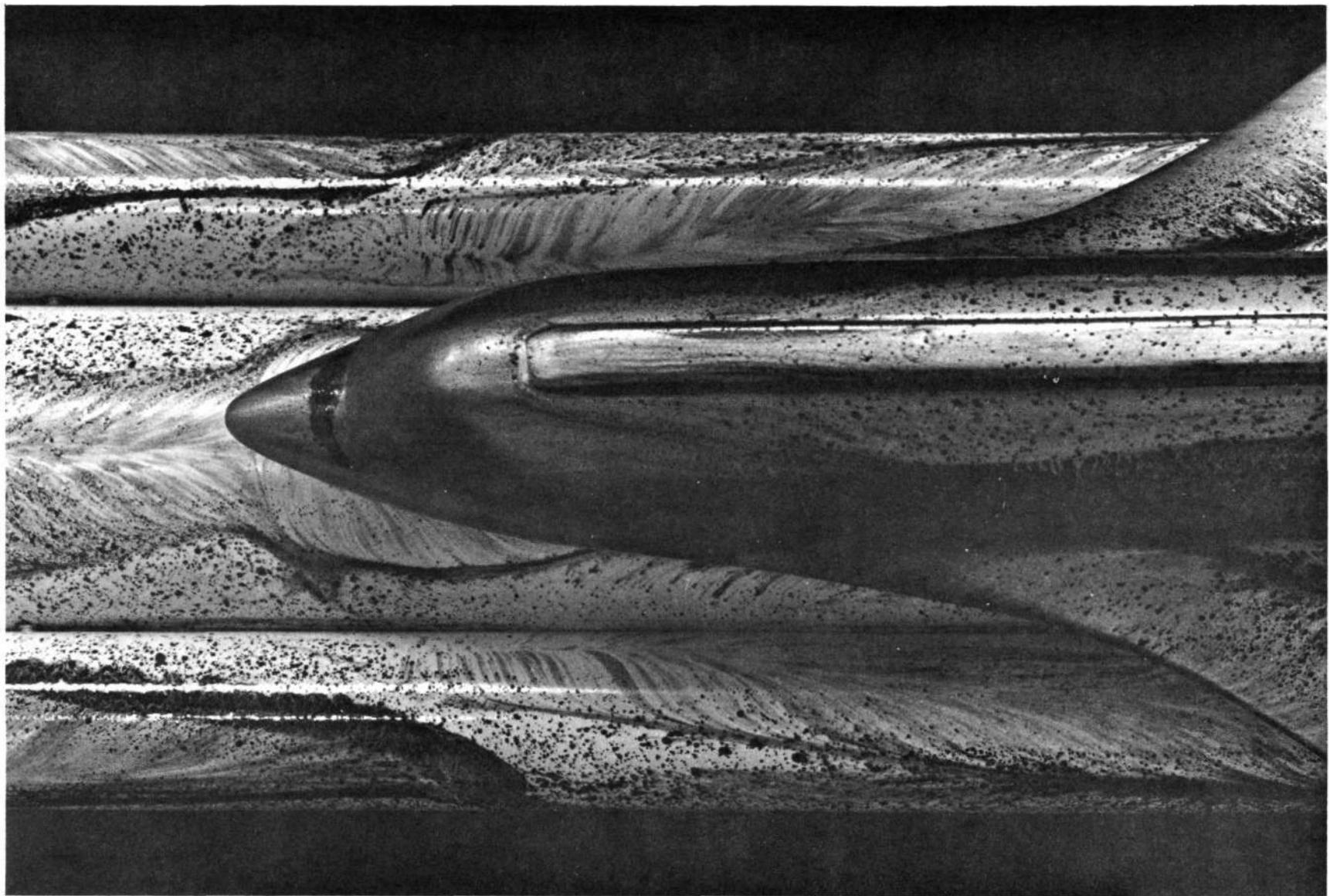
B) Left side view (rolled)

Figure 14. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = +5^\circ$.



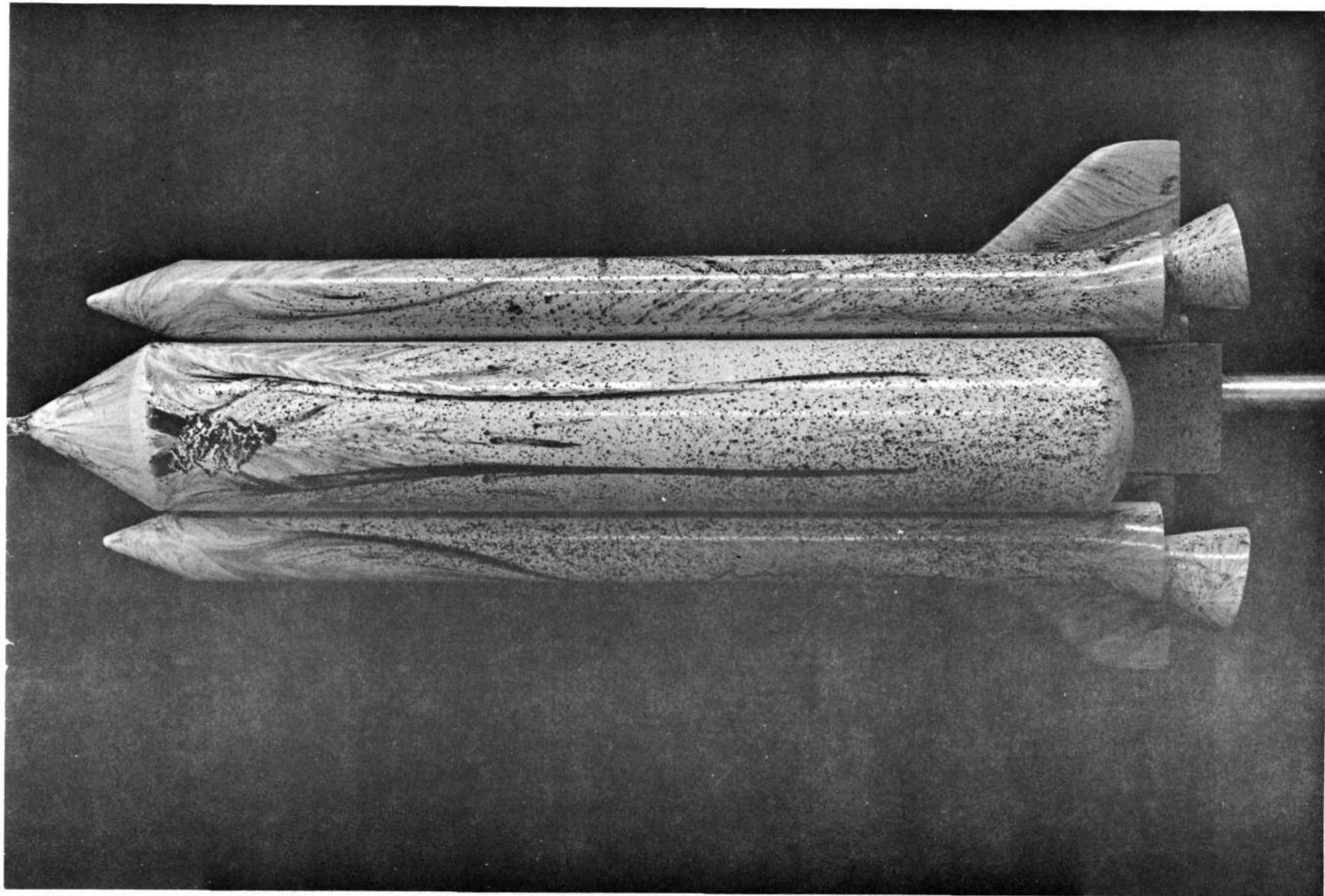
c) Top view

Figure 14. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = +5^\circ$.



D) Top view close-up

Figure 14. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = +5^\circ$.



E) Bottom view

Figure 14. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = +5^\circ$.



F) Front oblique view

Figure 14. - Photograph of Oil Flow Pattern After Removal from Tunnel on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = +5^\circ$.

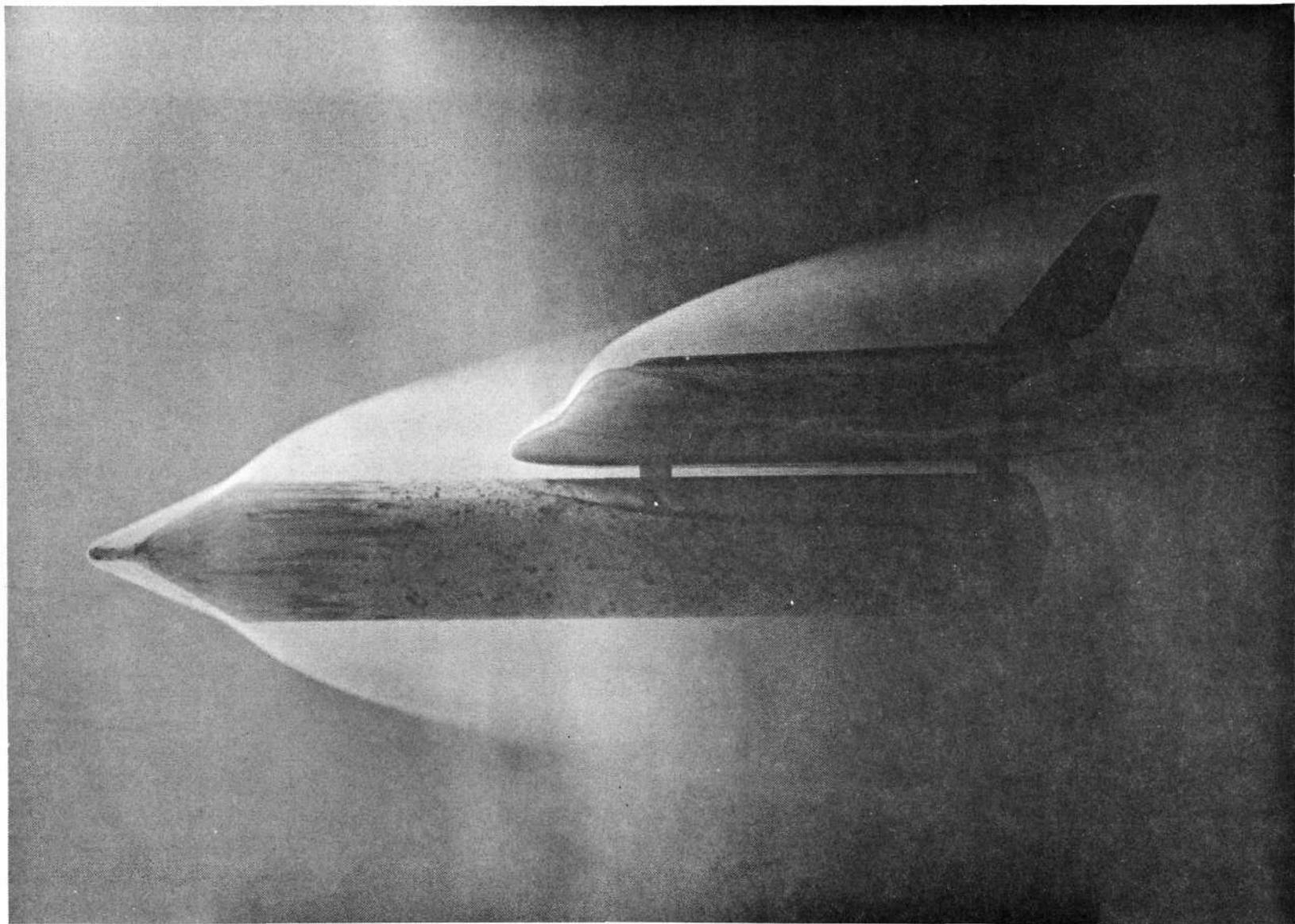


Figure 15. - Photograph of Electron Beam Illuminated Oil Flow Pattern on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = 0^\circ$.

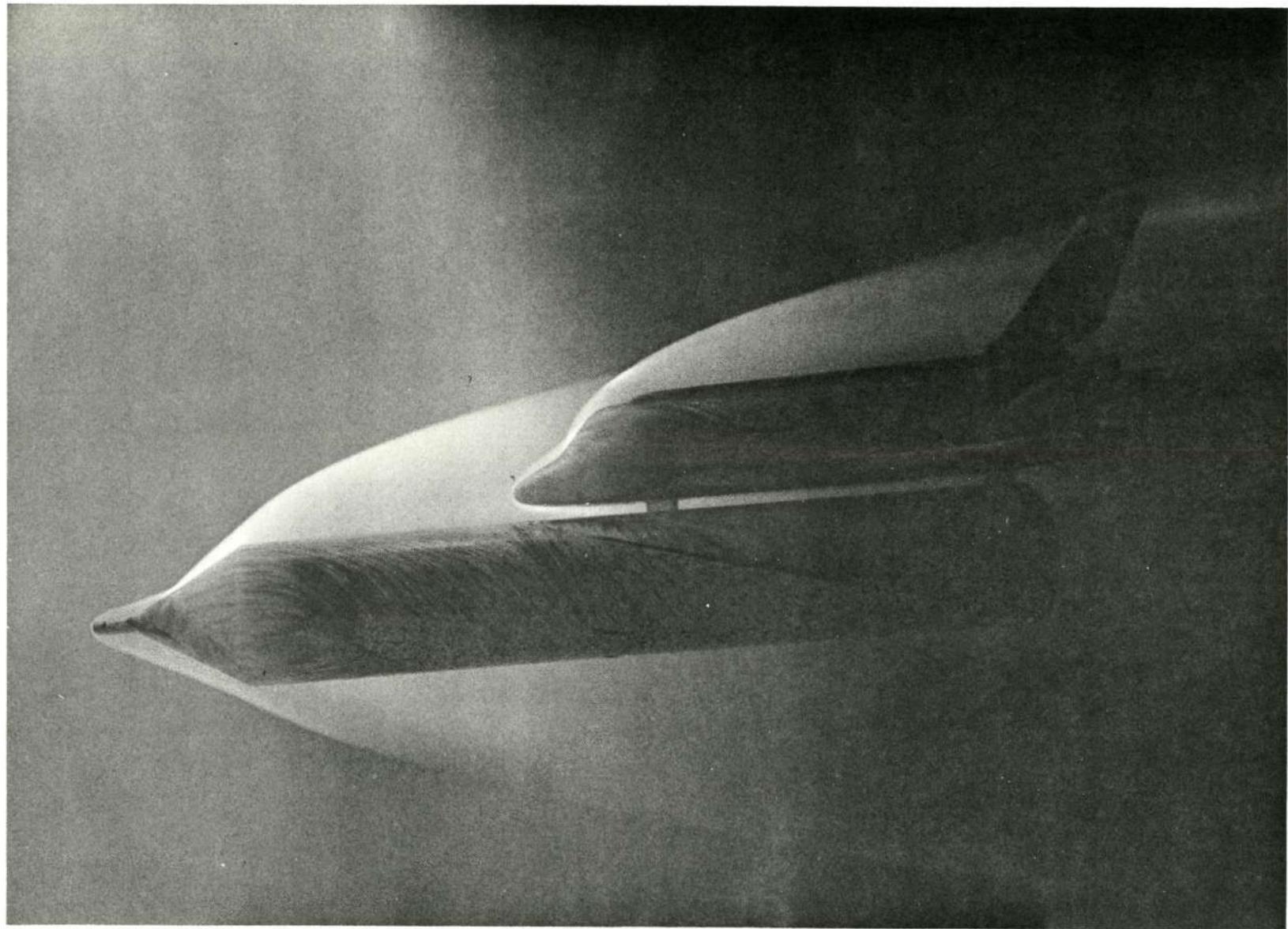


Figure 16. - Photograph of Electron Beam Illuminated Oil Flow Pattern on a .0045 Scale NR (ATP) Orbiter with External Tank at $M = 20.3$ and $\alpha = -5^\circ$.

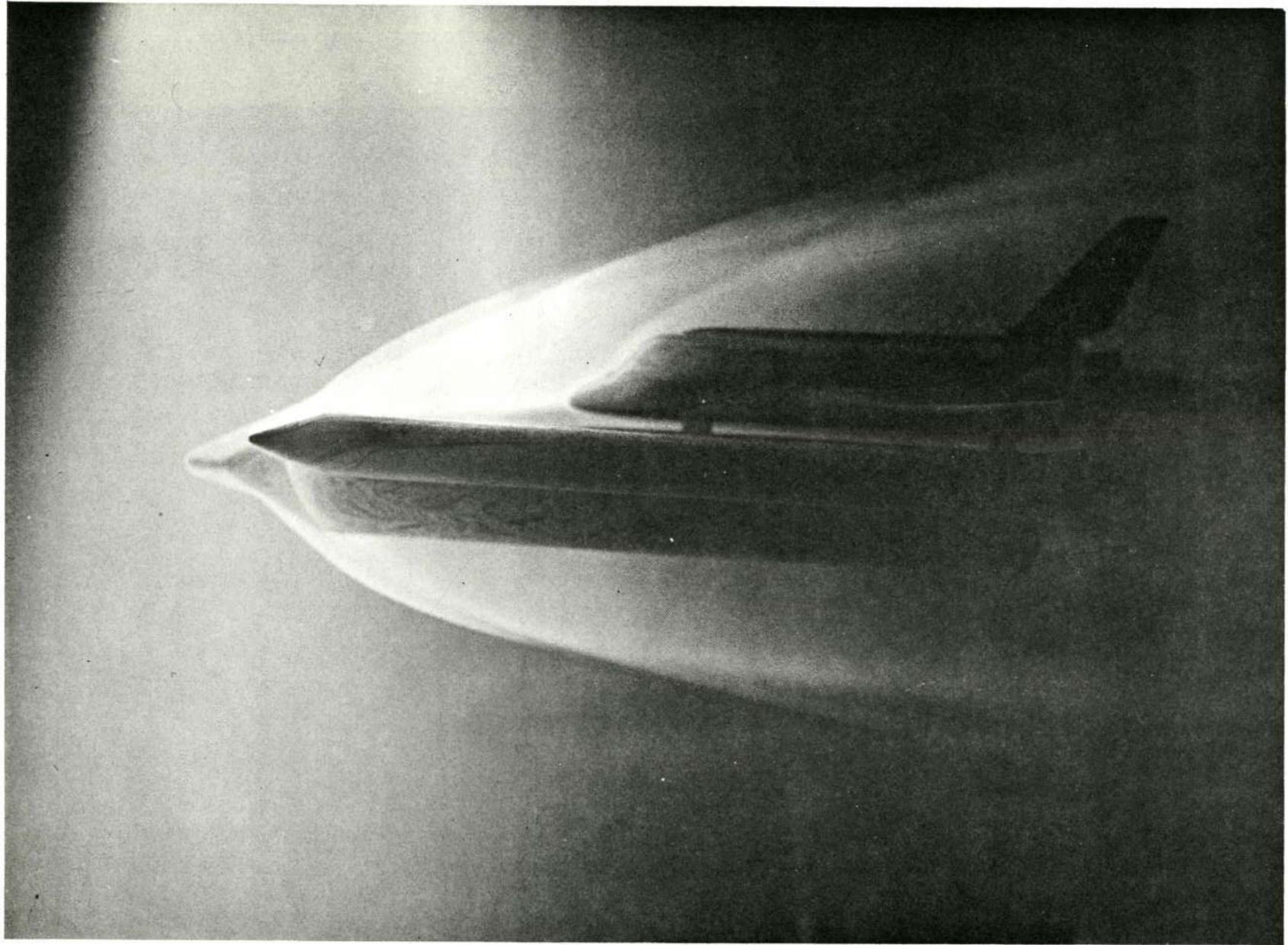


Figure 17. - Photograph of Electron Beam Illuminated Oil Flow Pattern on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = +5^\circ$.

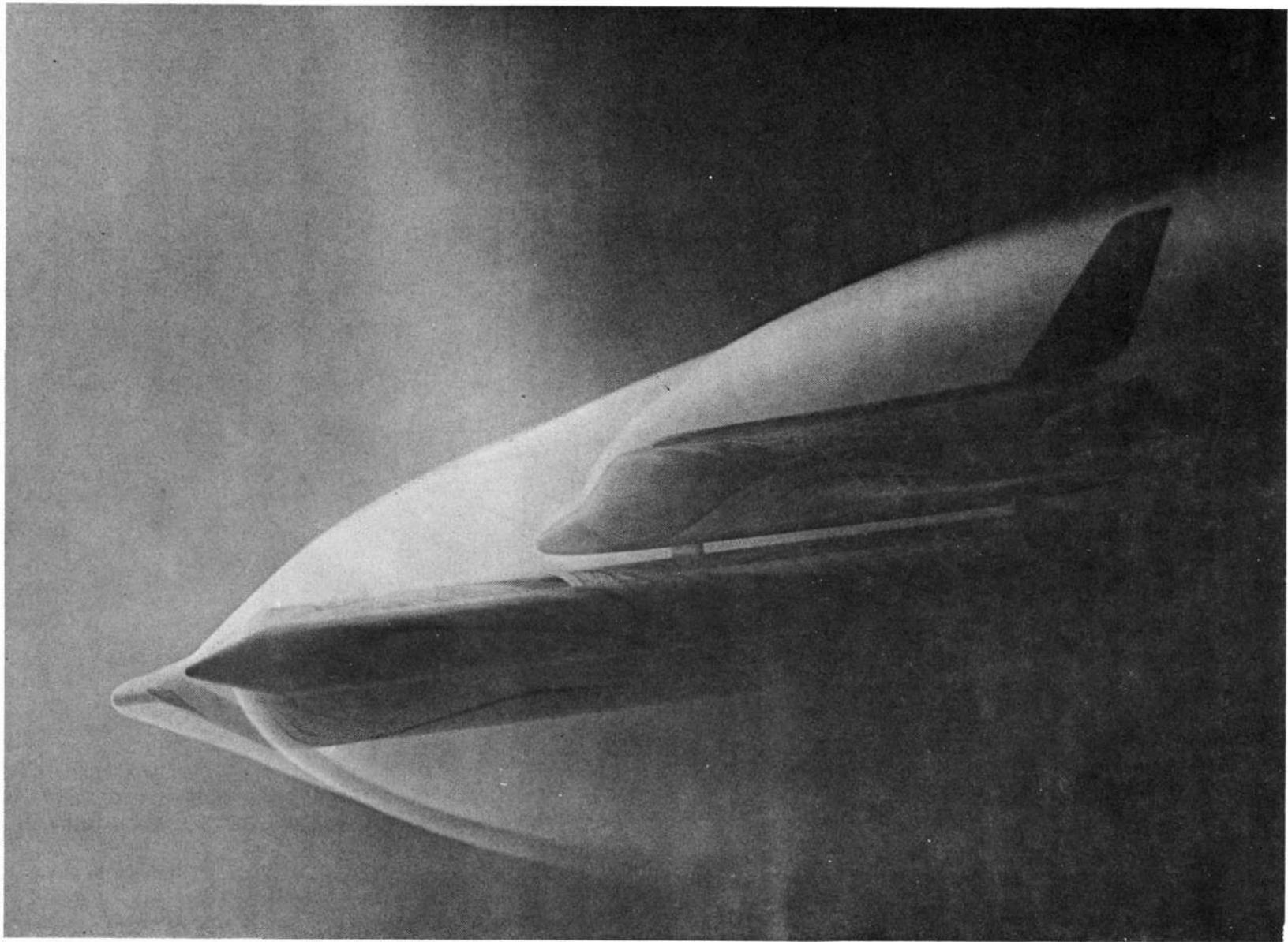


Figure 18. - Photograph of Electron Beam Illuminated Oil Flow Pattern on a .0045 Scale NR (ATP) Ascent Configuration at $M = 20.3$, $\alpha = -5^\circ$.

NOTES:

1. POSITIVE DIRECTIONS OF FORCE COEFFICIENTS
MOMENT COEFFICIENTS, AND ANGLES ARE
INDICATED BY ARROWS.
2. FOR CLARITY, ORIGINS OF WIND AND STABILITY
AXES HAVE BEEN DISPLACED FROM THE CENTER
OF GRAVITY.

98

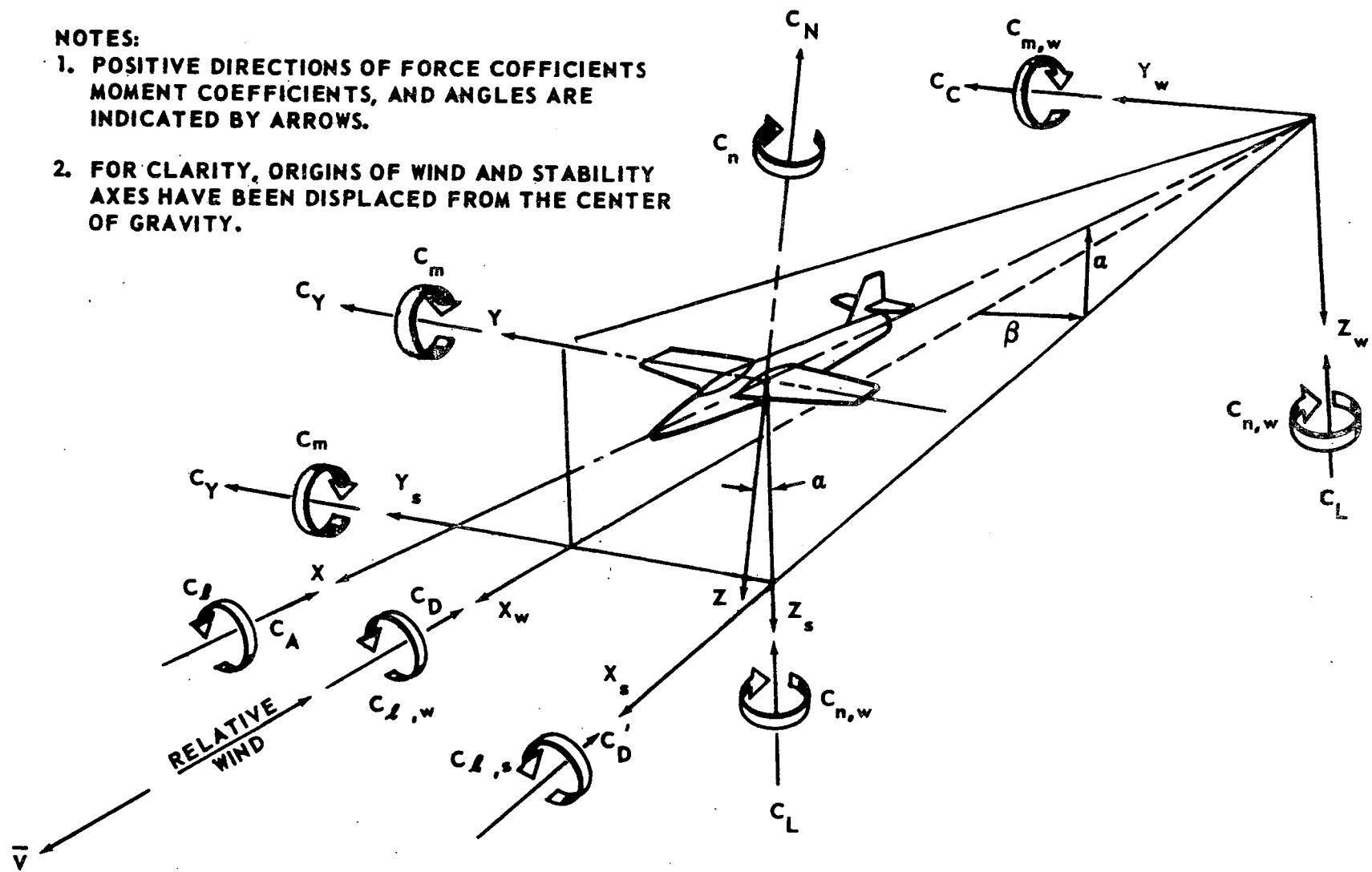
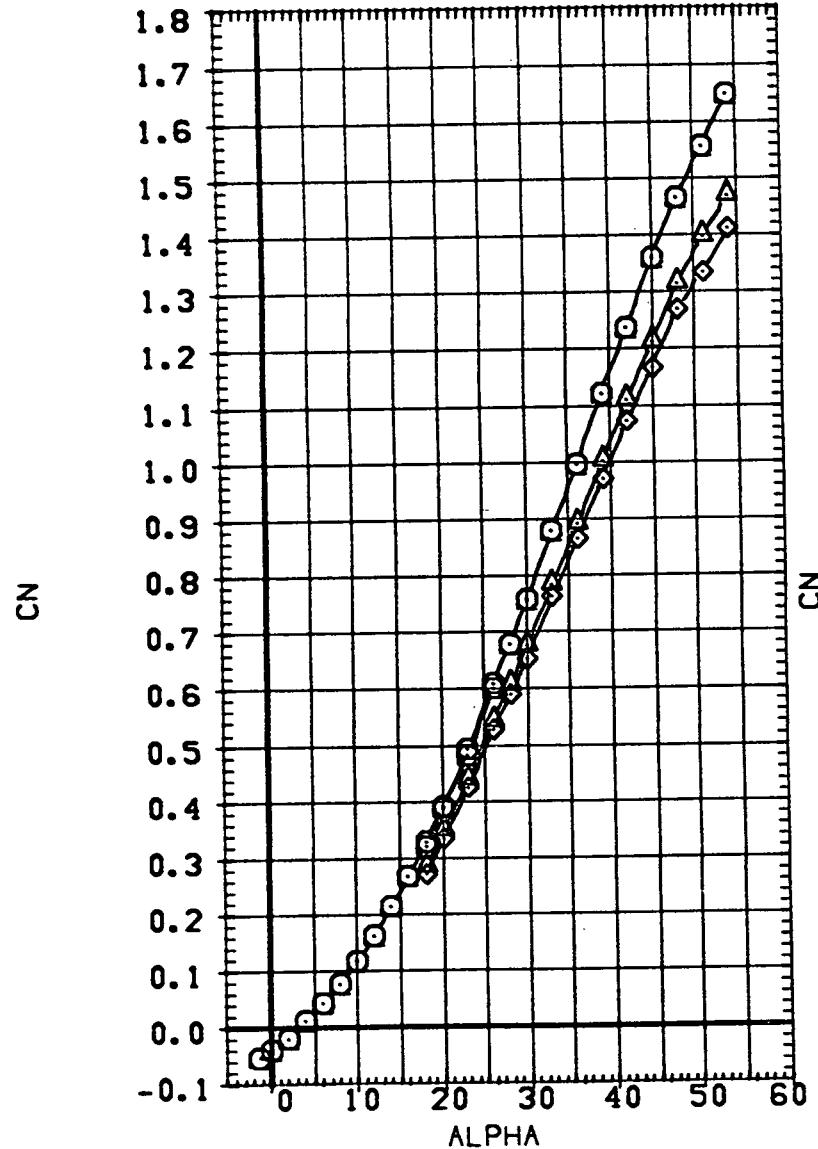


Figure 19. - Axis systems.

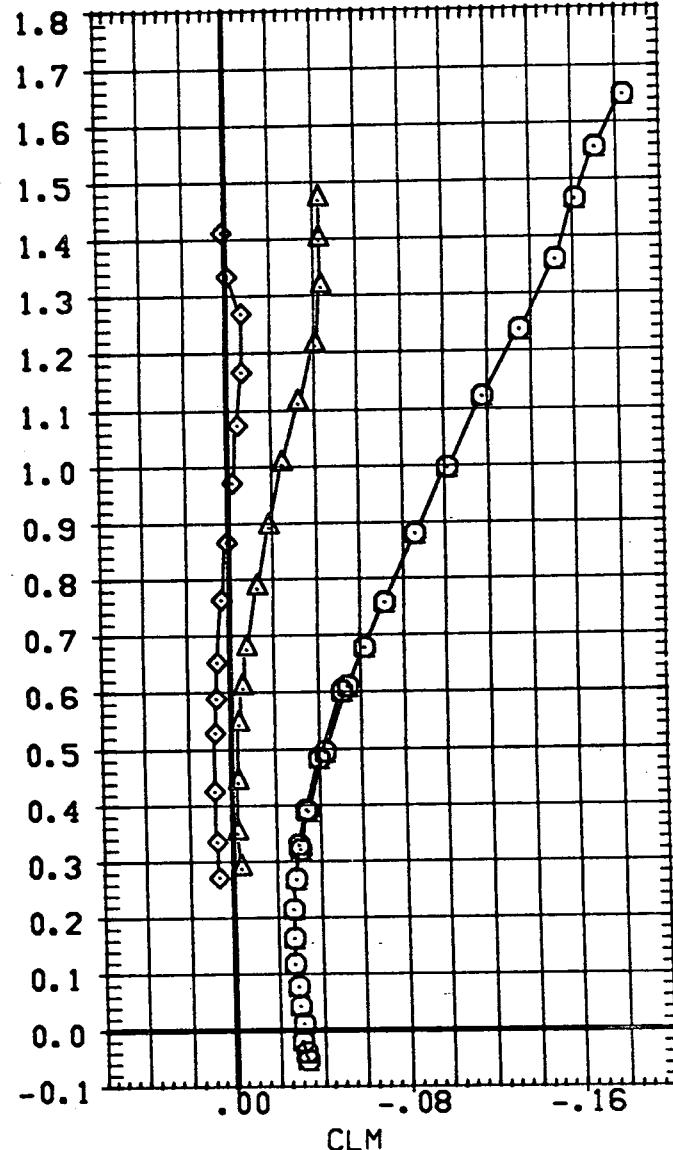
DATA FIGURES

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 (SOS015) △ HE.T. 409 NAR ATP ORB(B1C1D1F1H1) (W1E1) (V1R1R1)
 (SOS016) □ HE.T. 409 NAR ATP ORB(B1C1D1F1H1) (W1E1) (V1K1R1)
 (SOS017) ◇ HE.T. 409 NAR ATP ORB(B1C1D1F1H1) (W1E1) (V1K1R1)

ELEVTR AILRDN RUDDER BDFLAP REFERENCE INFORMATION
 0.000 0.000 0.000 0.000 SREF 9.3900 SQ.IN.
 0.000 0.000 0.000 0.000 LREF 2.3400 INCHES
 -20.000 0.000 0.000 0.000 BREF 4.5300 INCHES
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 ZMRP 0.0000 INCHES
 SCALE 0.0045 SCALE

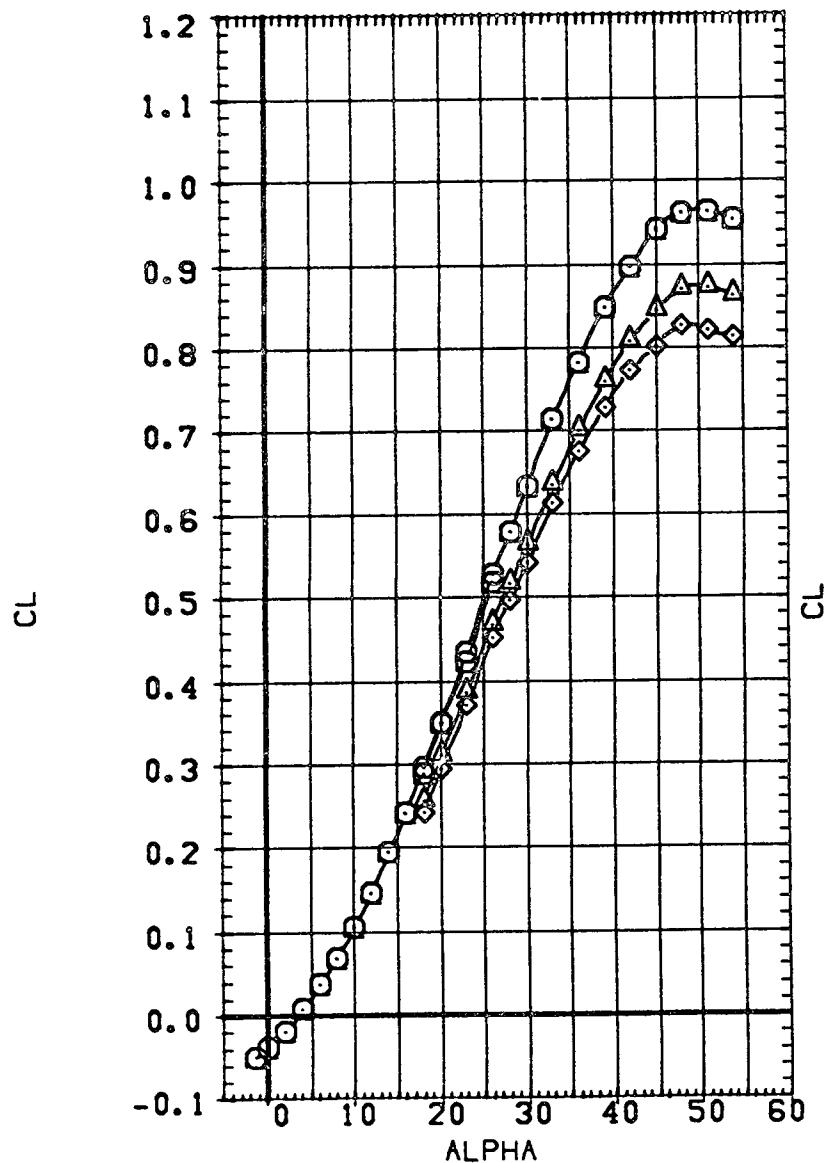


EFFECT OF ELEVATOR DEFLECTION ON LONGITUDINAL CHARACT. OF BASELINE ORBITER
 (A)MACH = 20.30

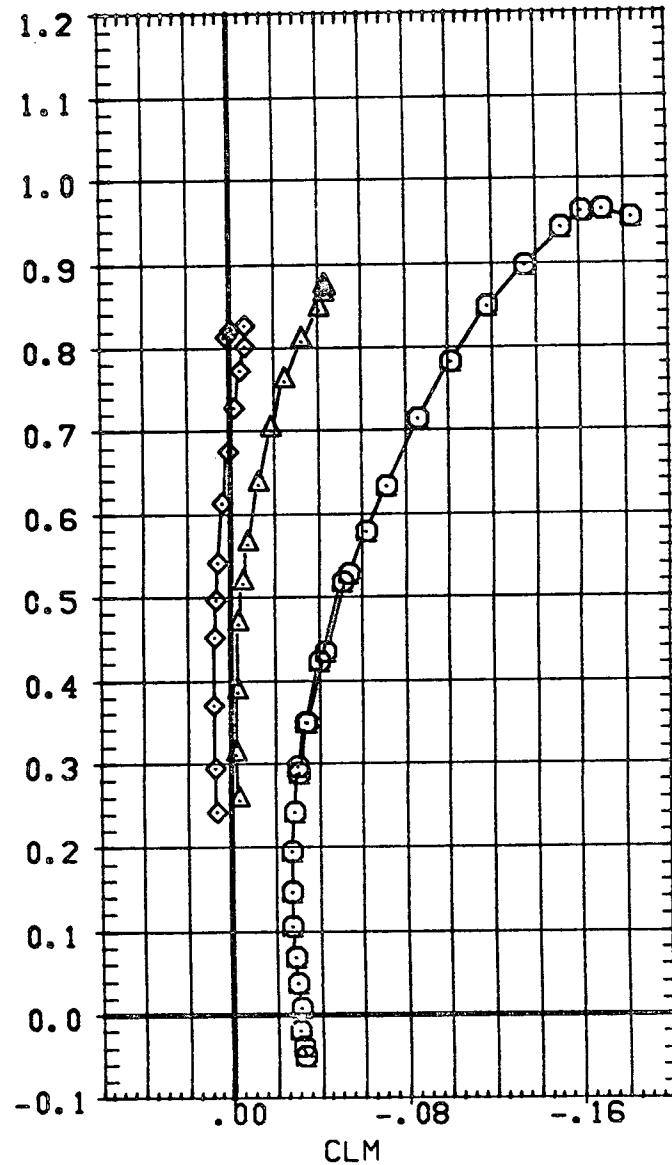


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(S0S019)	HE.T. 409 NAR ATP ORB(B1C1D1F1M1) (W1E1) (V1K1R1)
(S0S018)	HE.T. 409 NAR ATP ORB(B1C1D1F1M1) (W1E1) (V1K1R1)
(S0S017)	HE.T. 409 NAR ATP ORB(B1C1D1F1M1) (W1E1) (V1K1R1)

ELEVTR	AIRRON	RUBBER	BOFLAP	REFERENCE INFORMATION
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-20.000	0.000	0.000	0.000	BREF 4.5300 INCHES
-40.000	0.000	0.000	0.000	XMRP 3.8650 INCHES
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				ZMRP 0.0000 INCHES
				SCALE 0.0045 SCALE

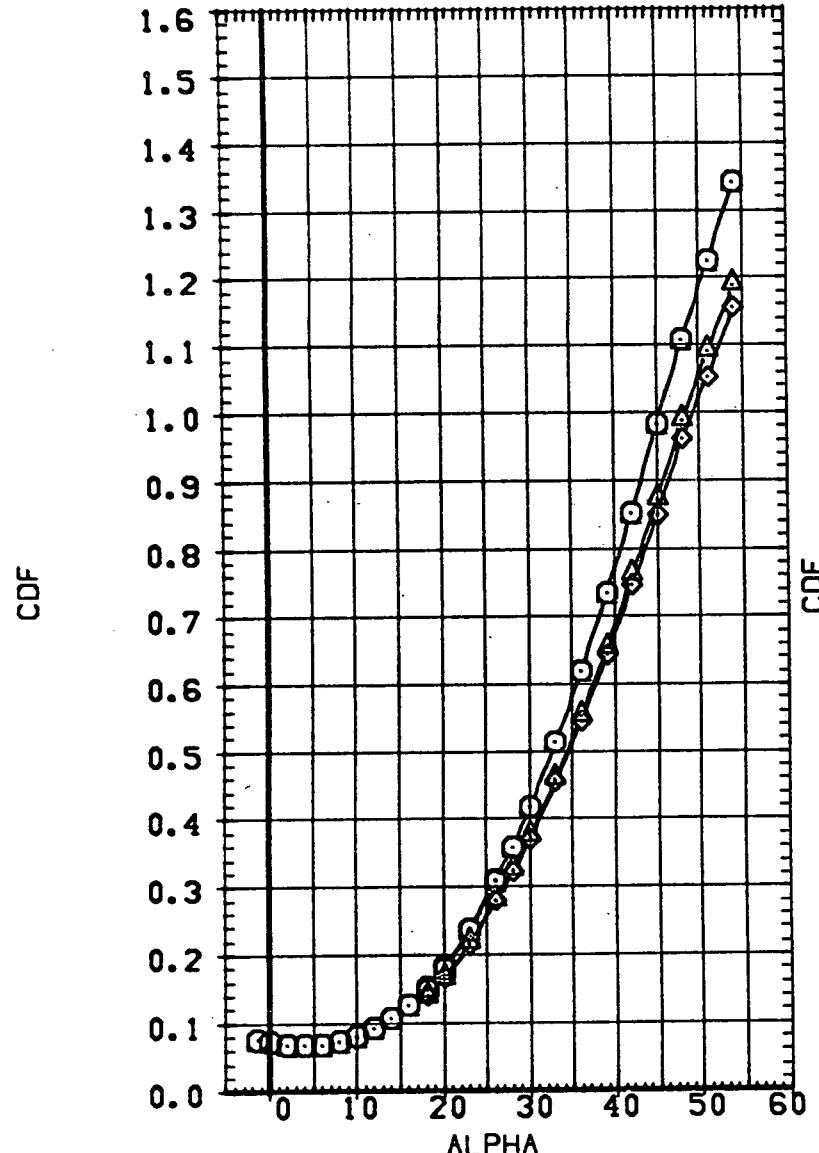


EFFECT OF ELEVATOR DEFLECTION ON LONGITUDINAL CHARACT. OF BASELINE ORBITER
 (A)MACH = 20.30

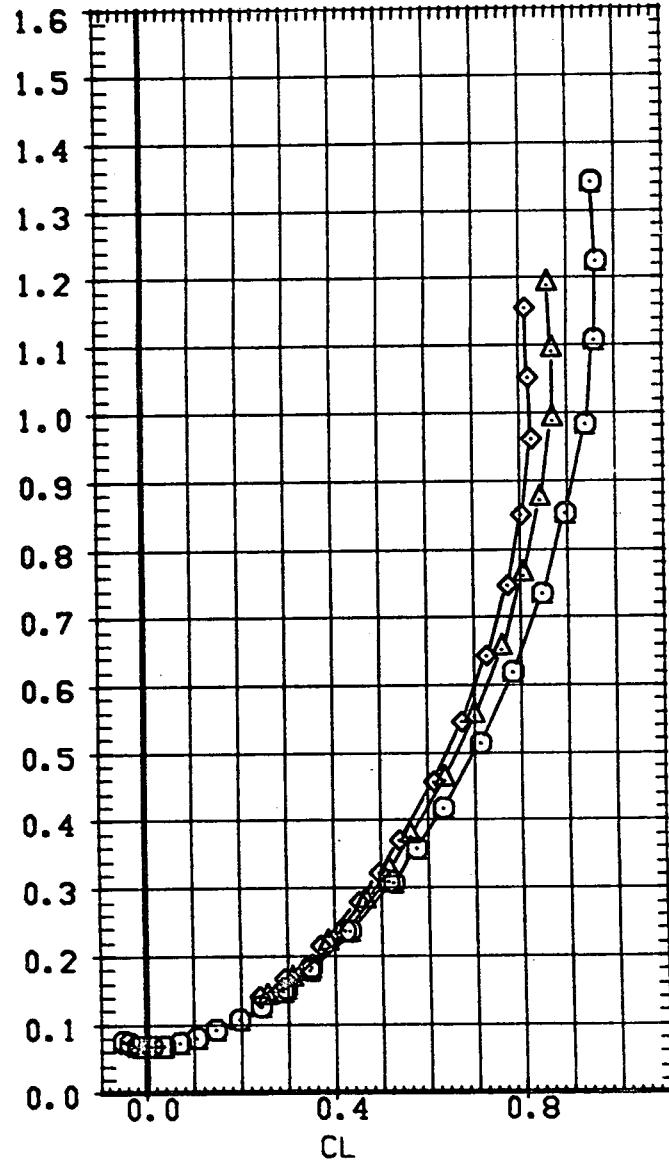


DATA SET SYMBOL CONFIGURATION DESCRIPTION
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 (S03019) □ HE.T. 409 NAR ATP ORB(B1C1D1F1H1) (W1E1) (V1K1R1)
 (S03018) △ HE.T. 409 NAR ATP ORB(B1C1D1F1H1) (W1E1) (V1K1R1)
 (S03017) ◇ HE.T. 409 NAR ATP ORB(B1C1D1F1H1) (W1E1) (V1K1R1)

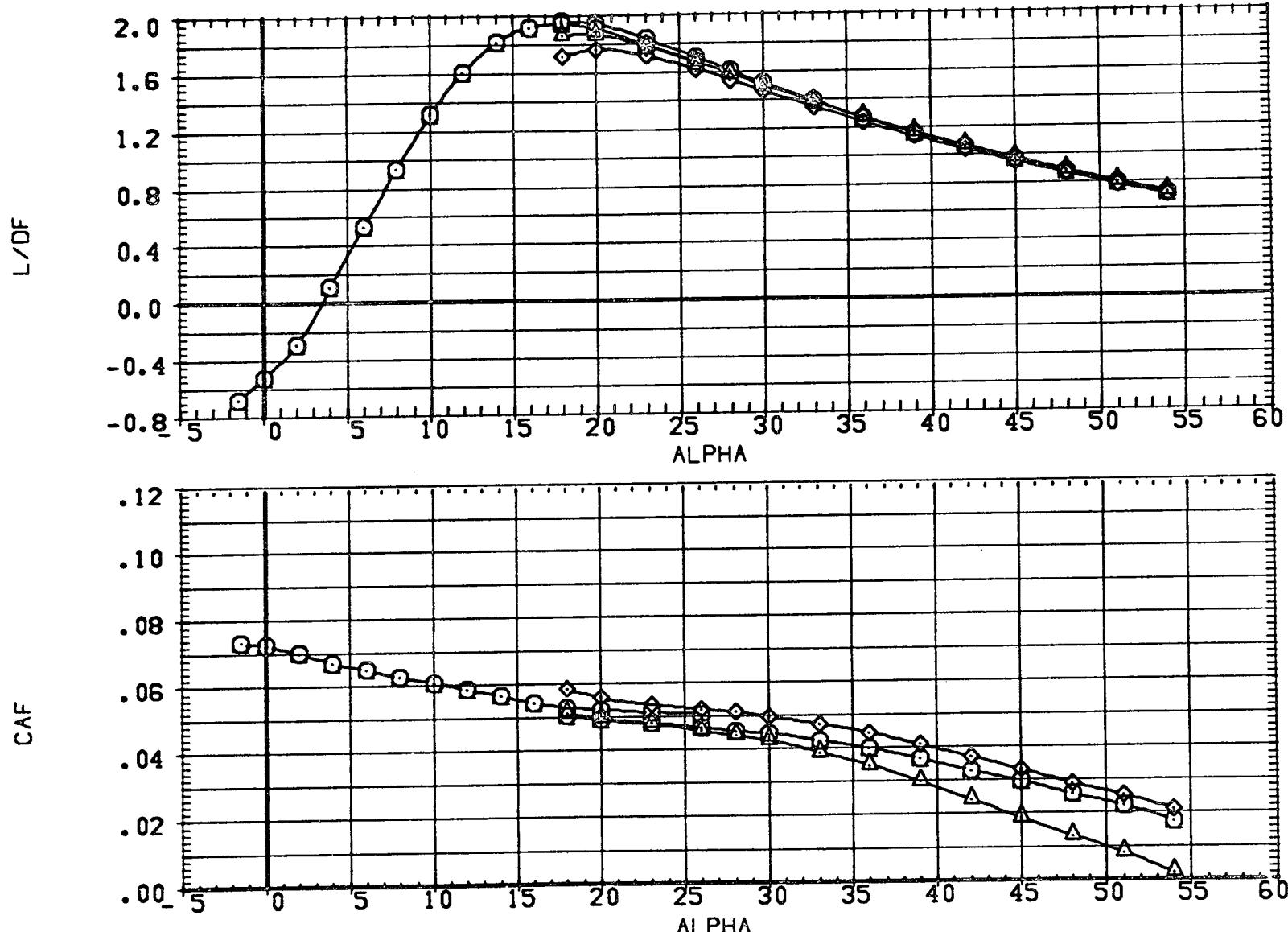
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 -20.000 0.000 0.000 0.000 BREF 4.5300 INCHES
 -40.000 0.000 0.000 0.000 XMRP 3.8850 INCHES
 YMRP 0.0000 INCHES
 ZMRP 0.0000 INCHES
 SCALE 0.0045 SCALE



EFFECT OF ELEVATOR DEFLECTION ON LONGITUDINAL CHARACT. OF BASELINE ORBITER
 (A)MACH = 20.30

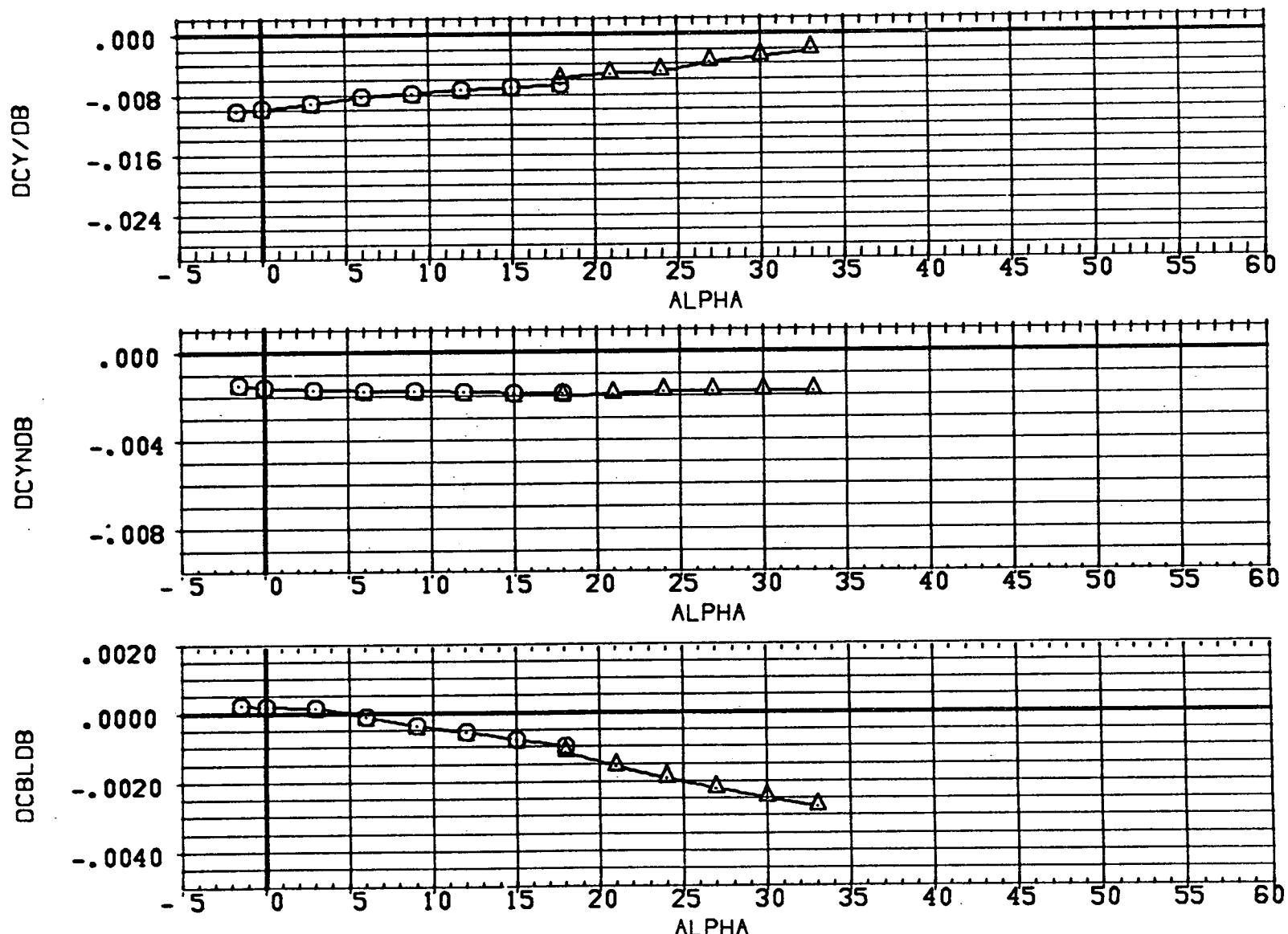


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(S03016)	HE.T. 409 NAR ATP ORB(B1C1D1F1M1) (W1E1) (V1K1R1)	-20.000	0.000	0.000	BREF	4.3300 INCHES
(S03017)	HE.T. 409 NAR ATP ORB(B1C1D1F1M1) (W1E1) (V1K1R1)	-40.000	0.000	0.000	XHRP	3.8850 INCHES
					YMRP	0.0000 INCHES
					ZMRP	0.0000 INCHES
					SCALE	0.0045 SCALE



EFFECT OF ELEVATOR DEFLECTION ON LONGITUDINAL CHARACT. OF BASELINE ORBITER
 (A)MACH = 20.30

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(AO3C26)	HE.T. 409 NAR ATP ORB(B1C1D1F1M1) (W1E1) (V1R1R1)	-4.500	0.000	0.000	0.000	SREF 9.3900 30. IN.
(AO3C27)	HE.T. 409 NAR ATP ORB(B1C1D1F1M1) (W1E1) (V1R1R1)	-2.250	0.000	0.000	0.000	LREF 2.3400 INCHES
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					XMRP 3.8850 INCHES	
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					ZMRP 0.0000 INCHES	
					SCALE 0.0045 SCALE	



LATERAL-DIRECTIONAL CHARACTERISTICS OF BASELINE ORBITER

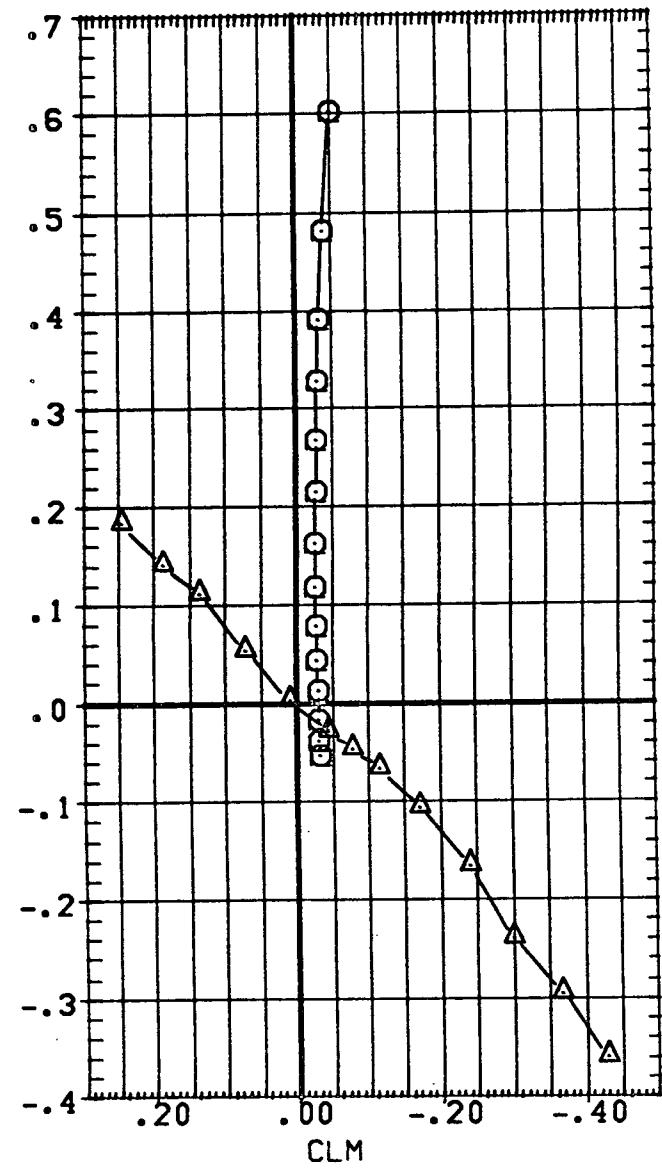
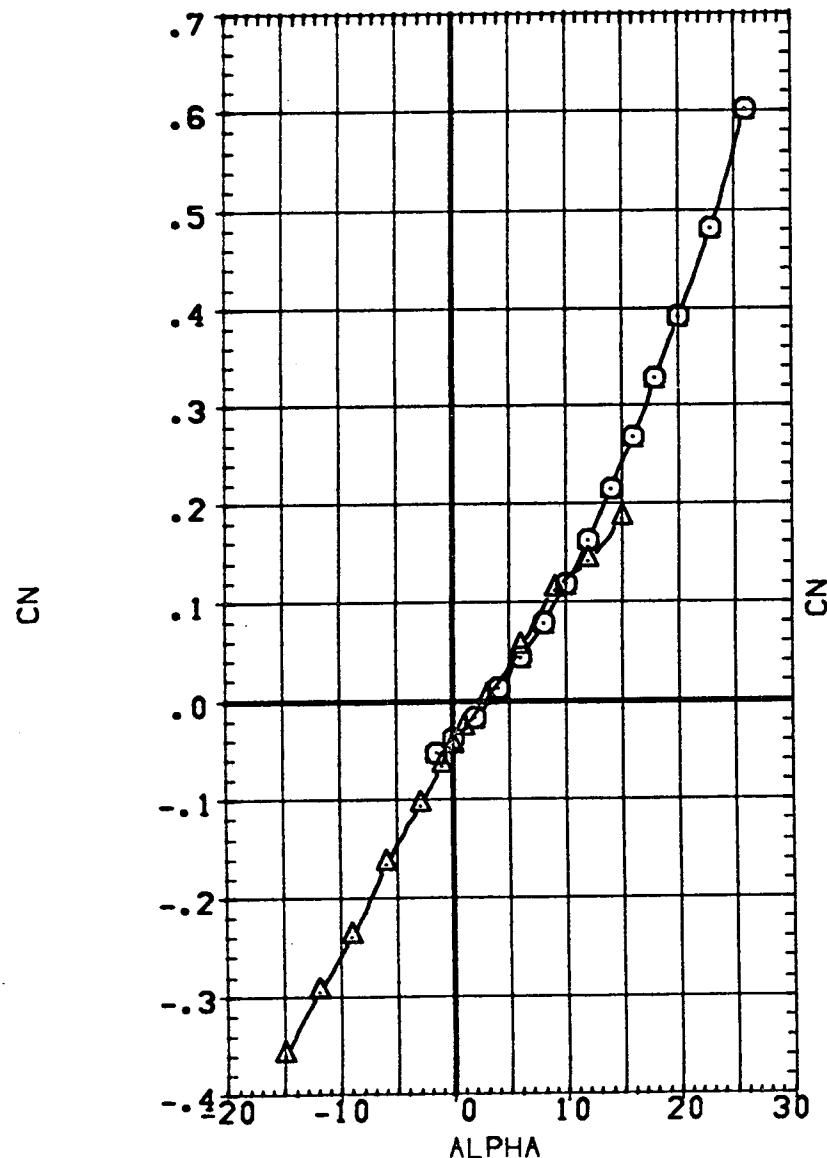
(A)MACH = 20.30

PAGE

5

DATA SET SYMBOL CONFIGURATION DESCRIPTION
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 (SOS031)  LRC 22HE-409, ATP ORBITER + EXTERNAL TANK (T1)

ELEVTR	AILRDN	RUDER	BDFLAP	REFERENCE INFORMATION
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0.000	0.000	0.000	0.000	LREF 2.3400 INCHES
				BREF 4.5300 INCHES
				XMRP 3.8850 INCHES
				YMRP 0.0000 INCHES
				ZMRP 0.0000 INCHES
				SCALE 0.0045 SCALE

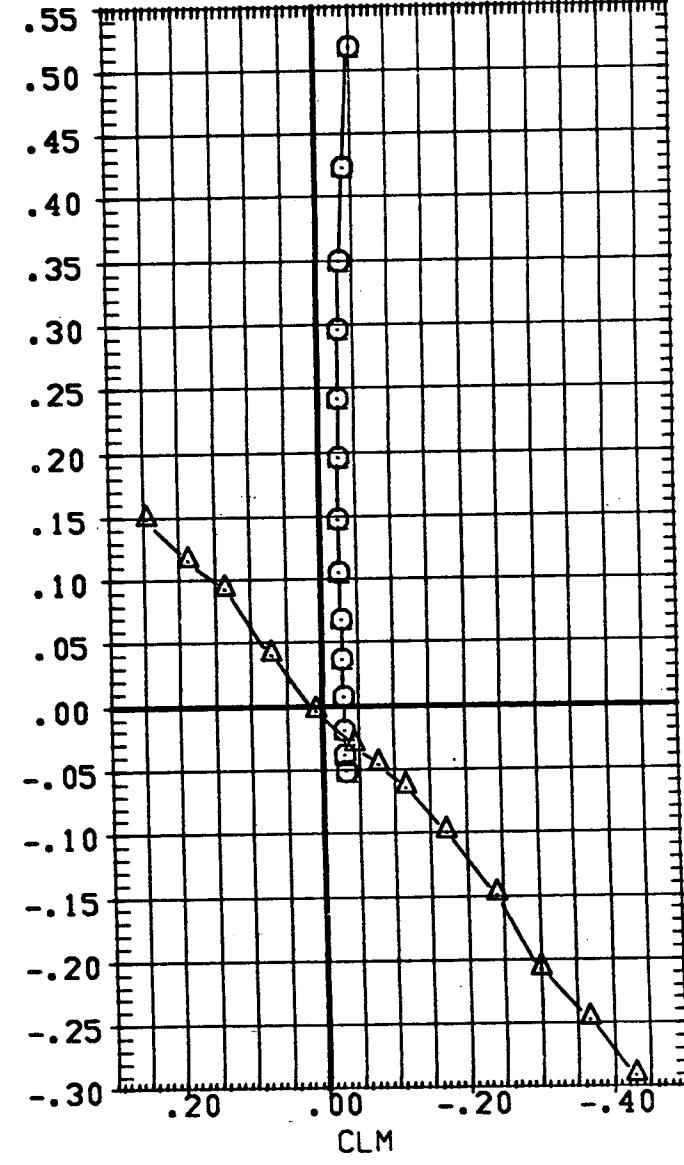
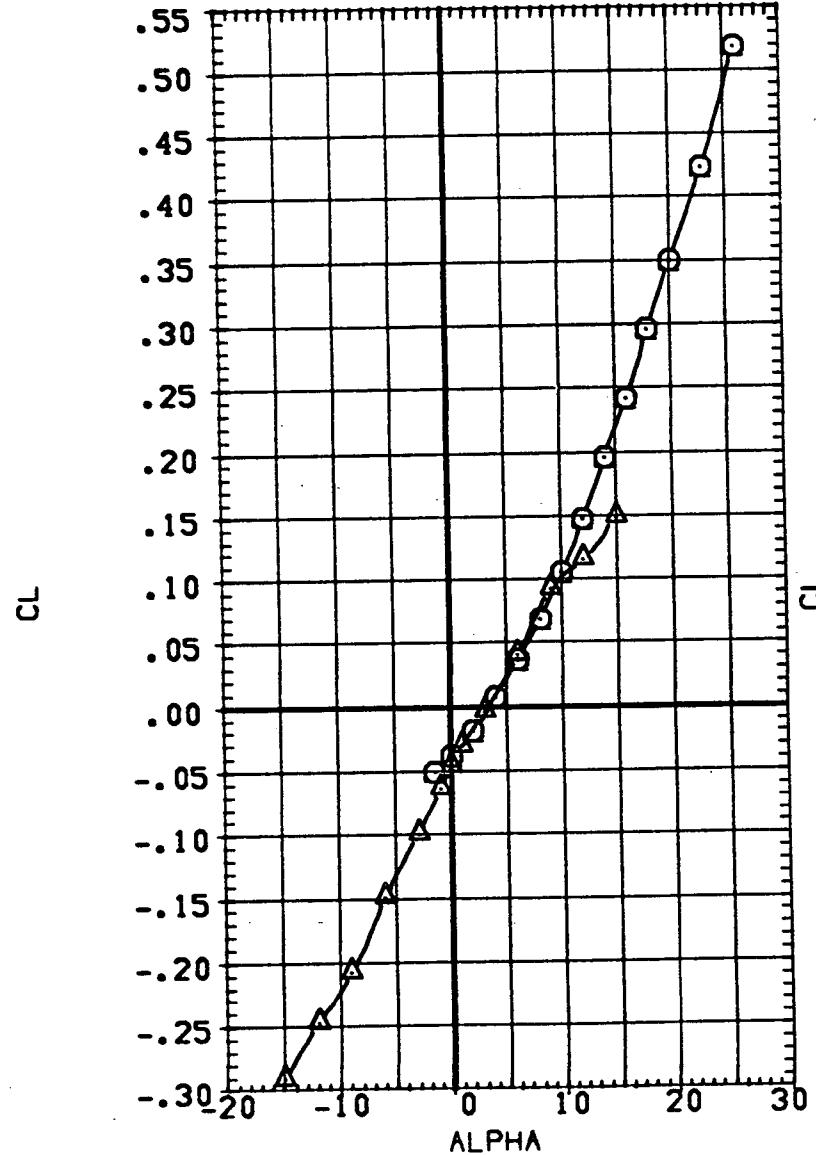


EFFECT OF EXTERNAL TANK ON ORBITER LONGITUDINAL CHARACTERISTICS

(A)MACH = 20.30

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 (S0S031)  LRC 22HE-409, ATP ORBITER + EXTERNAL TANK (T1)

ELEVTR AILRDN RUDDER BDFLAP REFERENCE INFORMATION
 0.000 0.000 0.000 0.000 SREF 9.3900 SQ. IN.
 0.000 0.000 0.000 0.000 LREF 2.3400 INCHES
 BREF 4.5300 INCHES
 XMRP 3.8850 INCHES
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 SCALE 0.0045 SCALE



EFFECT OF EXTERNAL TANK ON ORBITER LONGITUDINAL CHARACTERISTICS

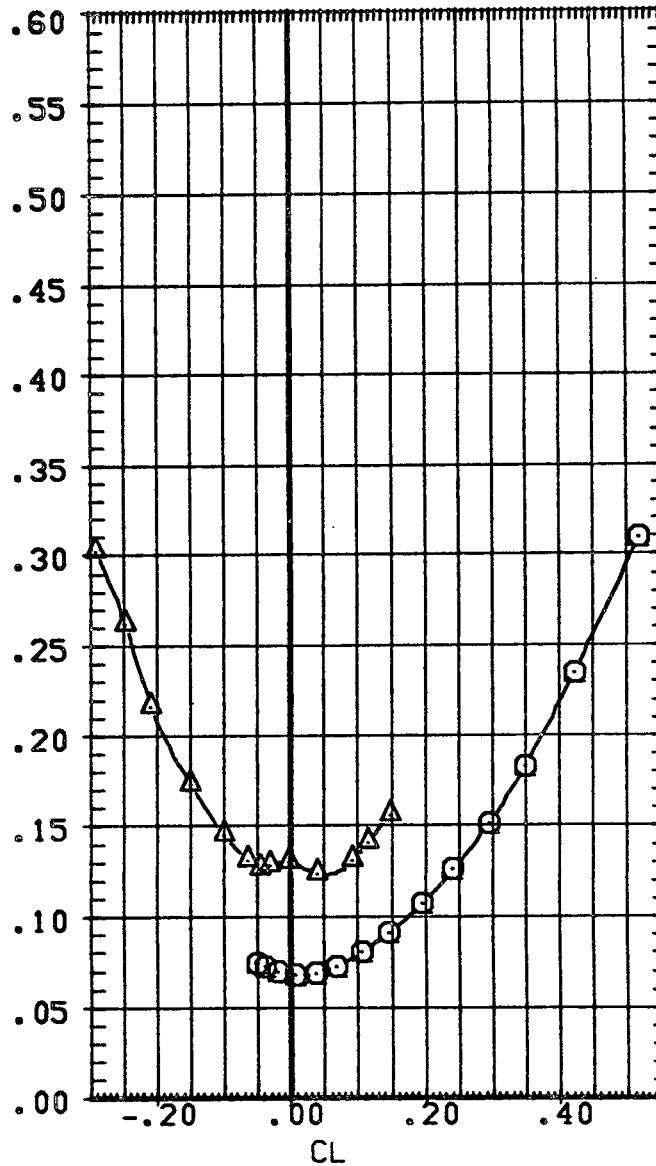
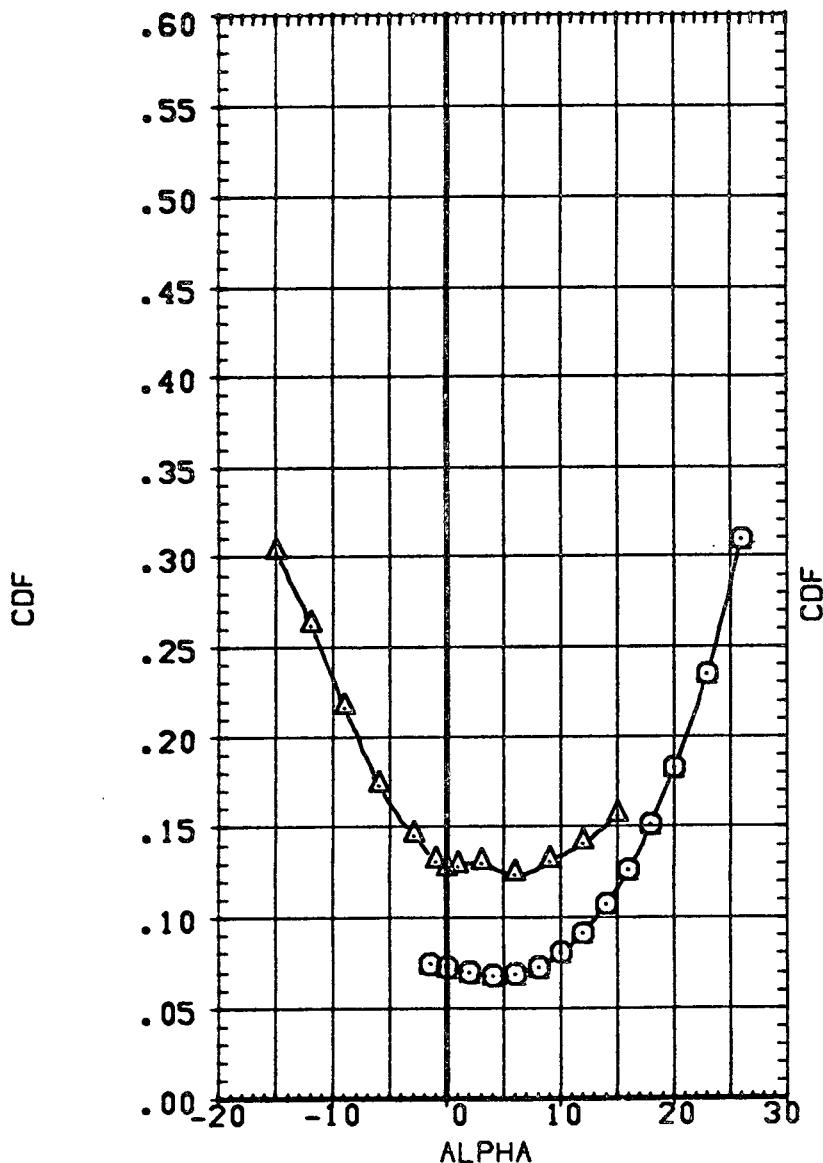
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PAGE

7

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 (SOS031)  LRC 22HE-409, ATP ORBITER + EXTERNAL TANK (T1)

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				BREF 4.5300 INCHES
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				YMRP 0.0000 INCHES
				ZMRP 0.0000 INCHES
				SCALE 0.0045 SCALE



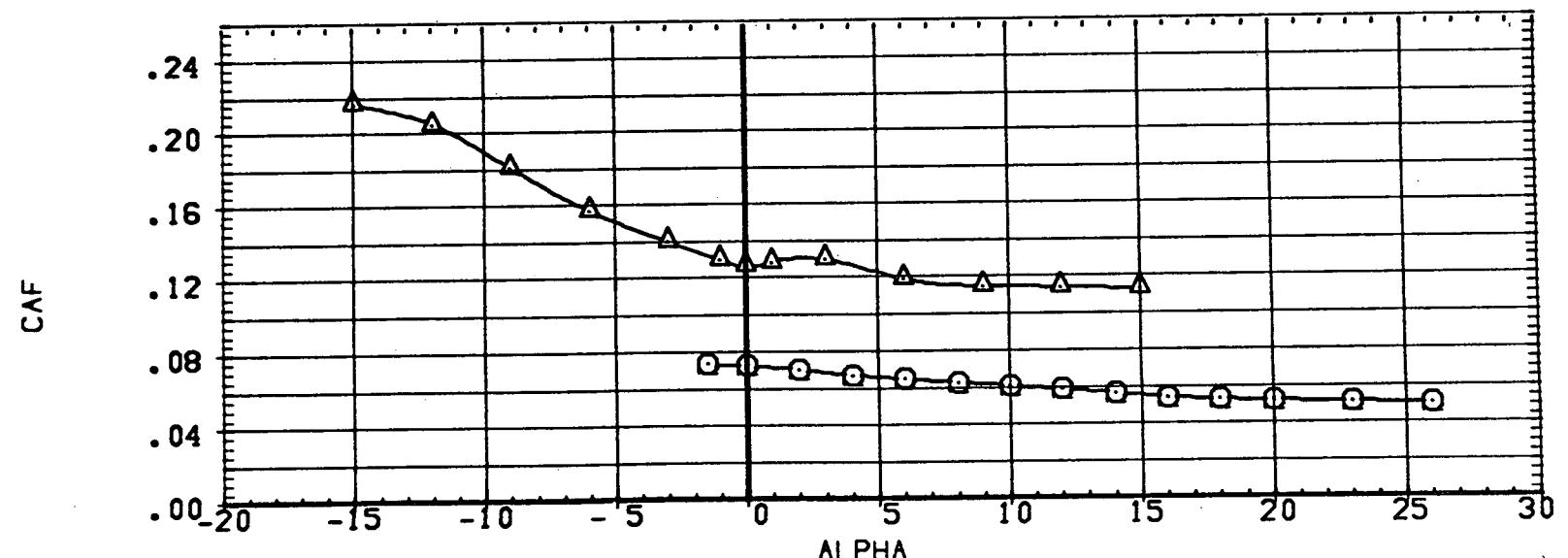
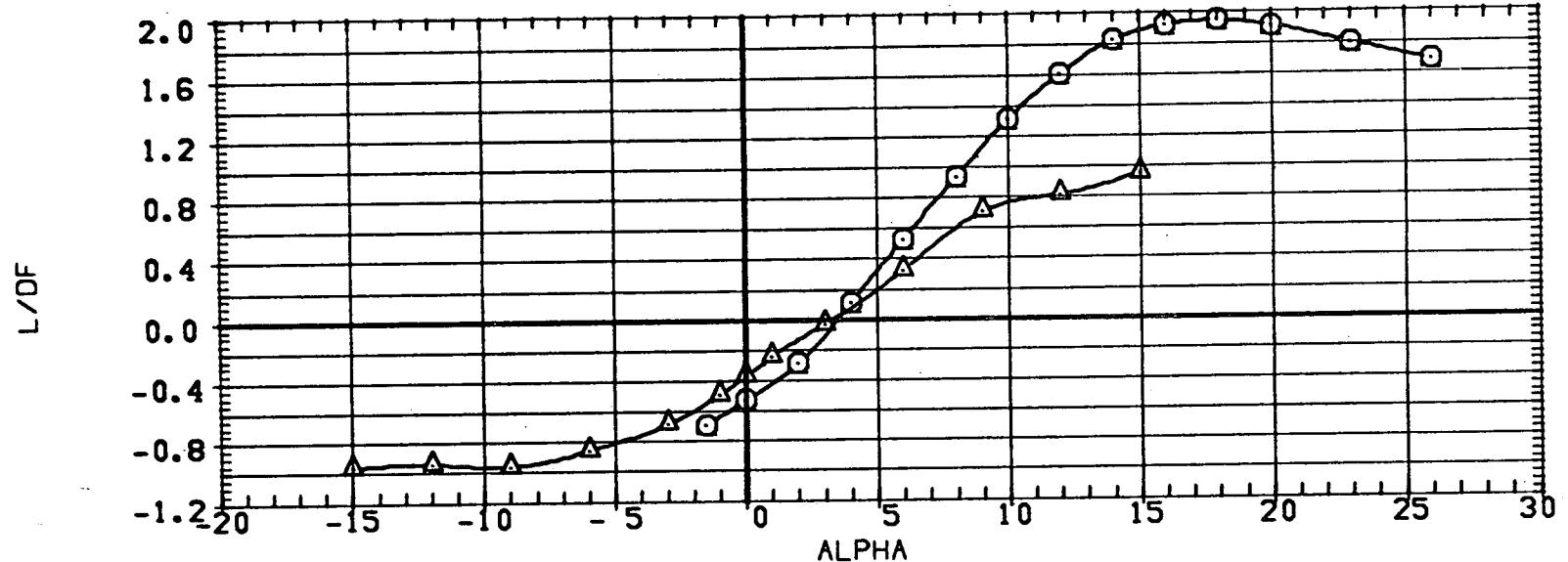
EFFECT OF EXTERNAL TANK ON ORBITER LONGITUDINAL CHARACTERISTICS

(A)MACH = 20.30

PAGE 8

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 (SOS031)  LRC 22HE-409, ATP ORBITER + EXTERNAL TANK (T1)

	ELEVTR	AILRON	RUDER	BDFLAP	REFERENCE	INFORMATION
(SOS020)	0.000	0.000	0.000	0.000	SREF	9.3900 SQ.IN.
(SOS031)	0.000	0.000	0.000	0.000	LREF	2.3400 INCHES
					BREF	4.5300 INCHES
					XMRP	3.8850 INCHES
					YMRP	0.0000 INCHES
					ZMRP	0.0000 INCHES
					SCALE	0.0045 SCALE



EFFECT OF EXTERNAL TANK ON ORBITER LONGITUDINAL CHARACTERISTICS

(A)MACH = 20.30

PAGE

9

LRC 22HE-409. ATP ORBITER + EXTERNAL TANK (T1) (A0SC30)

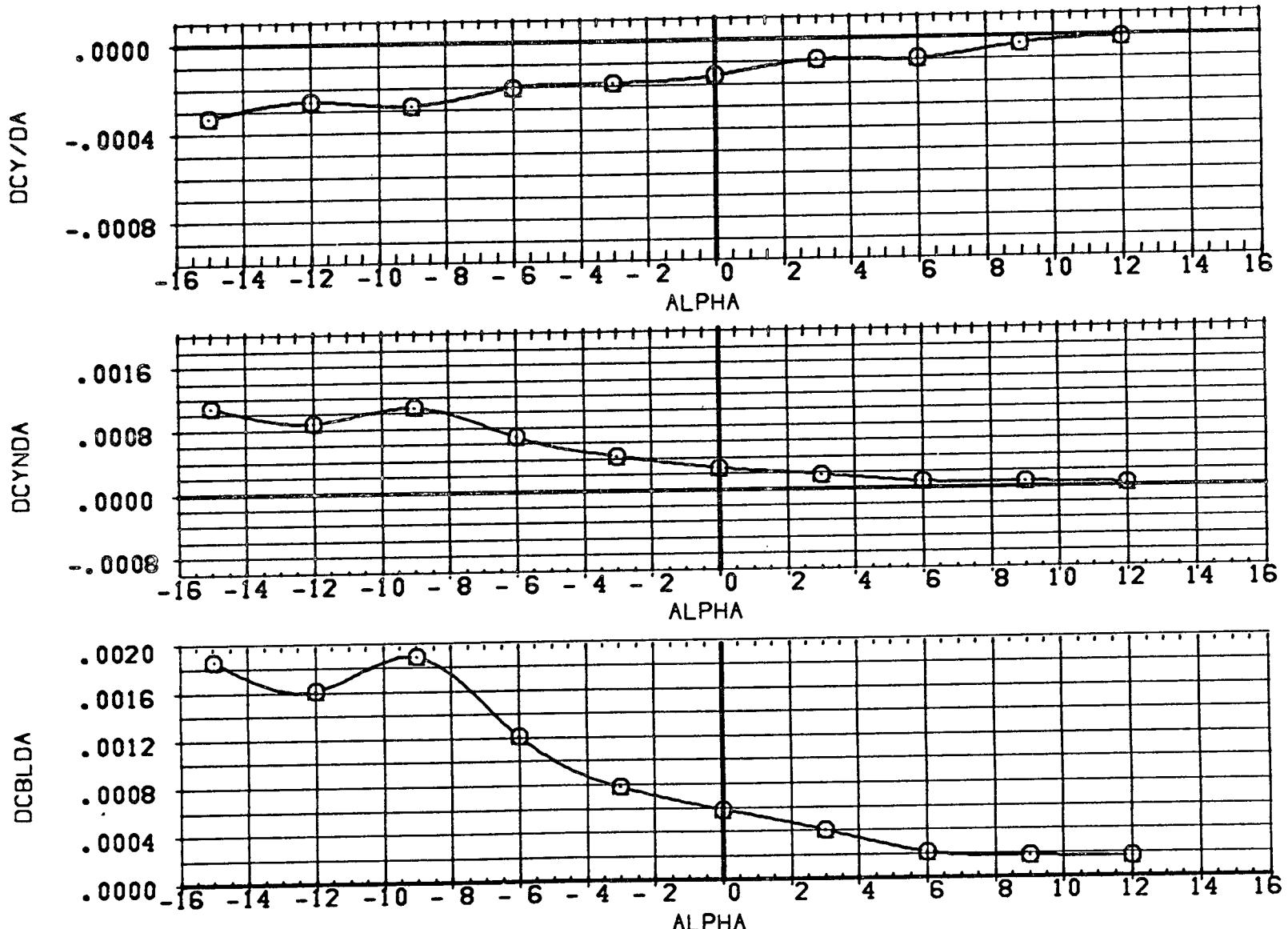
SYMBOL

MACH
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BDFLAP	0.000		

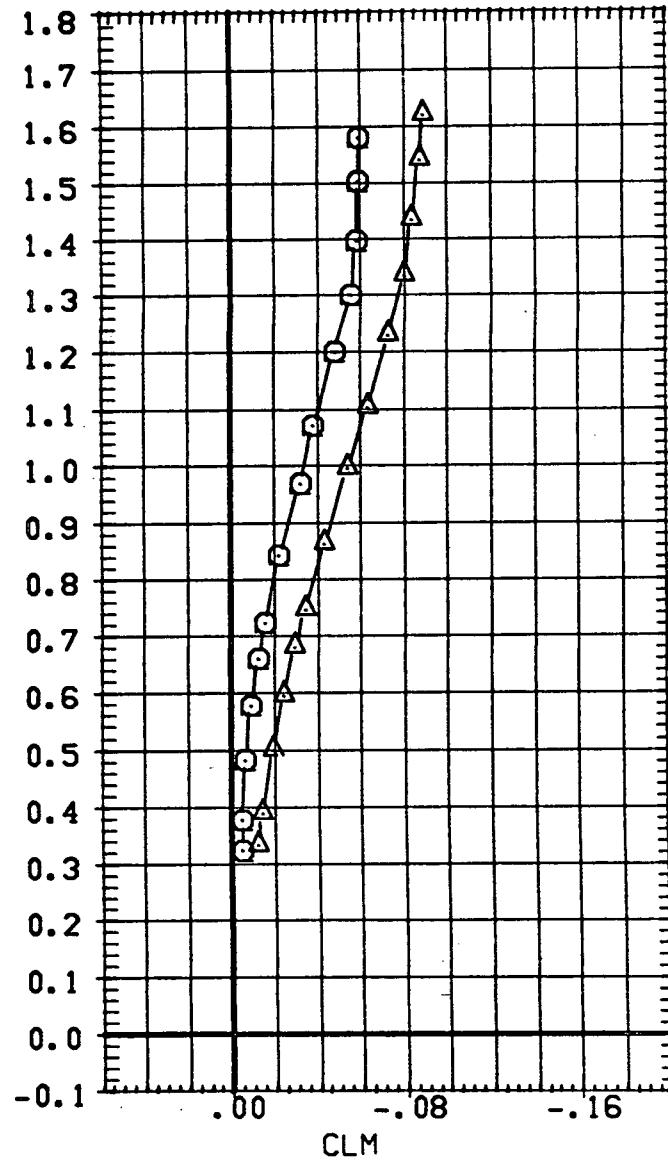
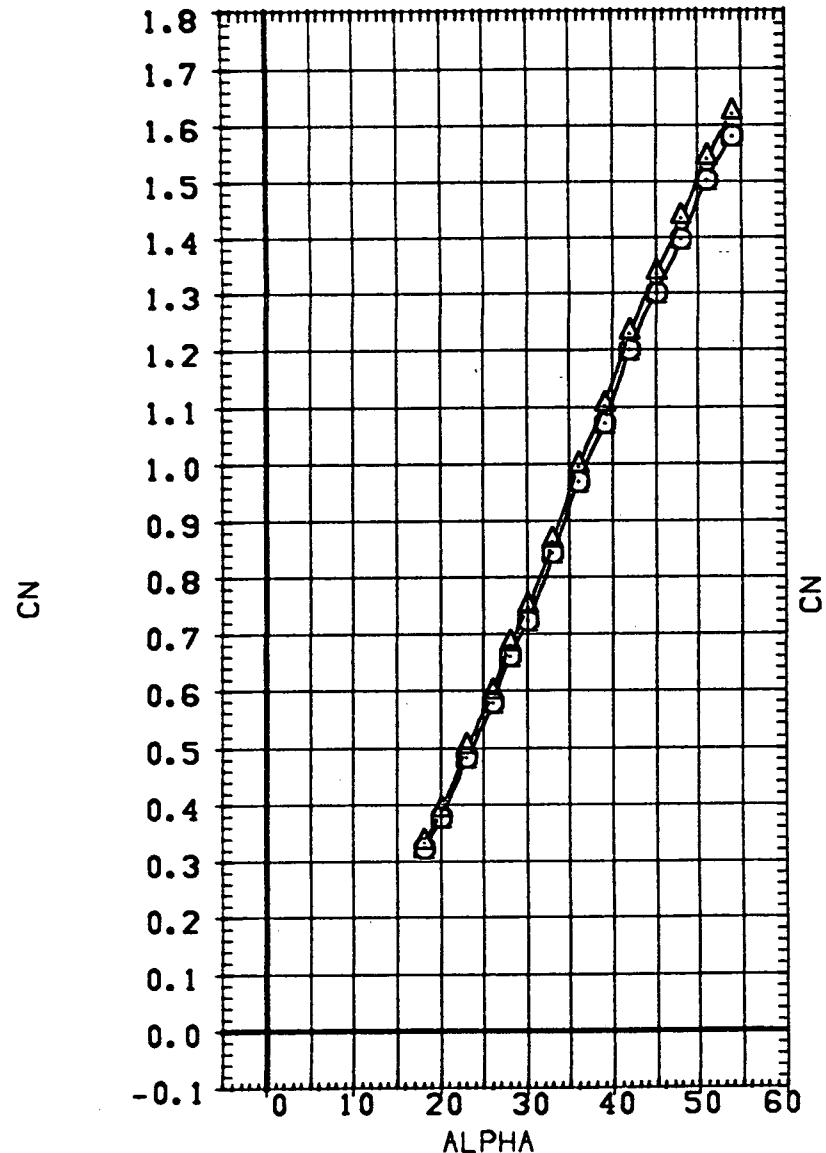
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BREF	4.5300	INCHES
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YMRP	0.0000	INCHES
ZMRP	0.0000	INCHES
SCALE	0.0045	SCALE



AILERON EFFECTIVENESS FOR ORBITER WITH EXTERNAL TANK

DATA SET SYMBOL CONFIGURATION DESCRIPTION
 (SOS002) LRC 22HE-409,ATP ORB (B1C1D1F1M1) (W1X1E1) (V1K1R1)
 (SOS007) LRC 22HE-409,ATP ORB (B1C1D1F1M1) (W1X1E1) (V1K1R1)

ELEVTR	AIRLON	RUDER	BDFLAP	REFERENCE INFORMATION
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-20,000	20.000	0.000	0.000	LREF 2.3400 INCHES
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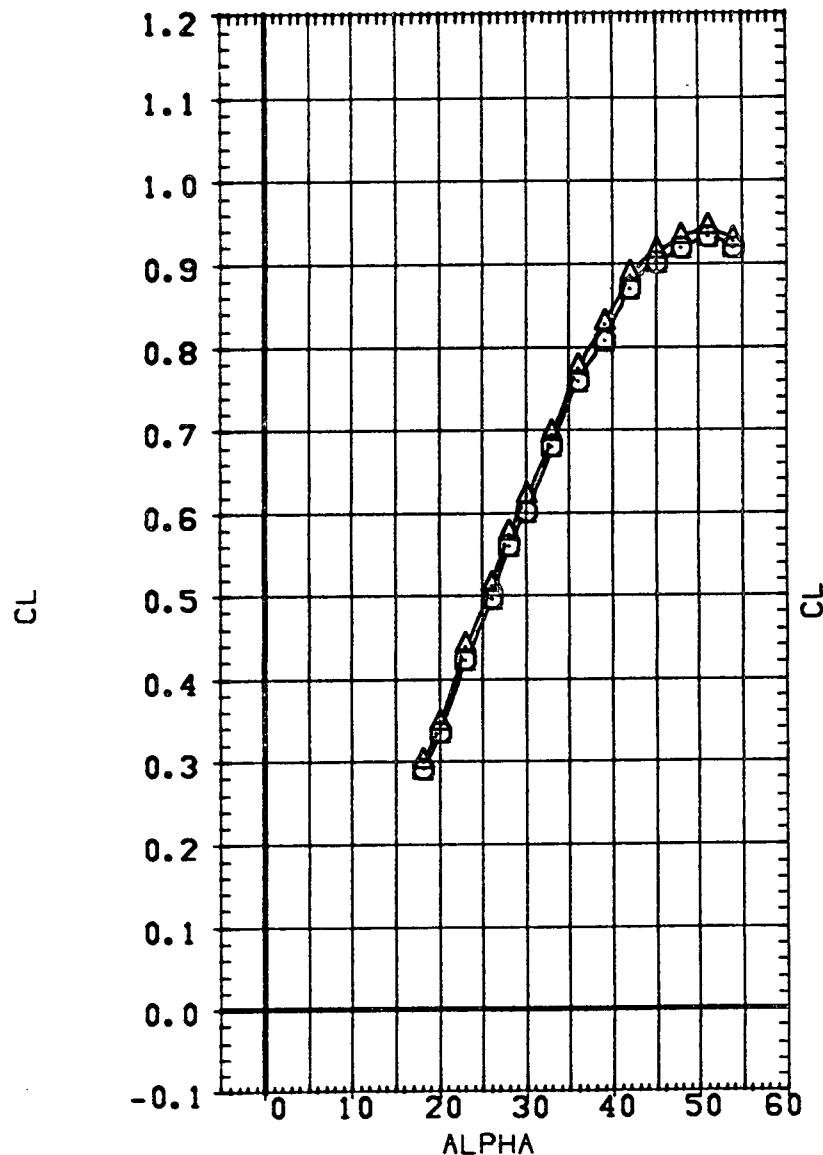


EFFECT OF AILERON DEFLECTION ON LONGITUDINAL CHARACT. OF MODIFIED ORBITER

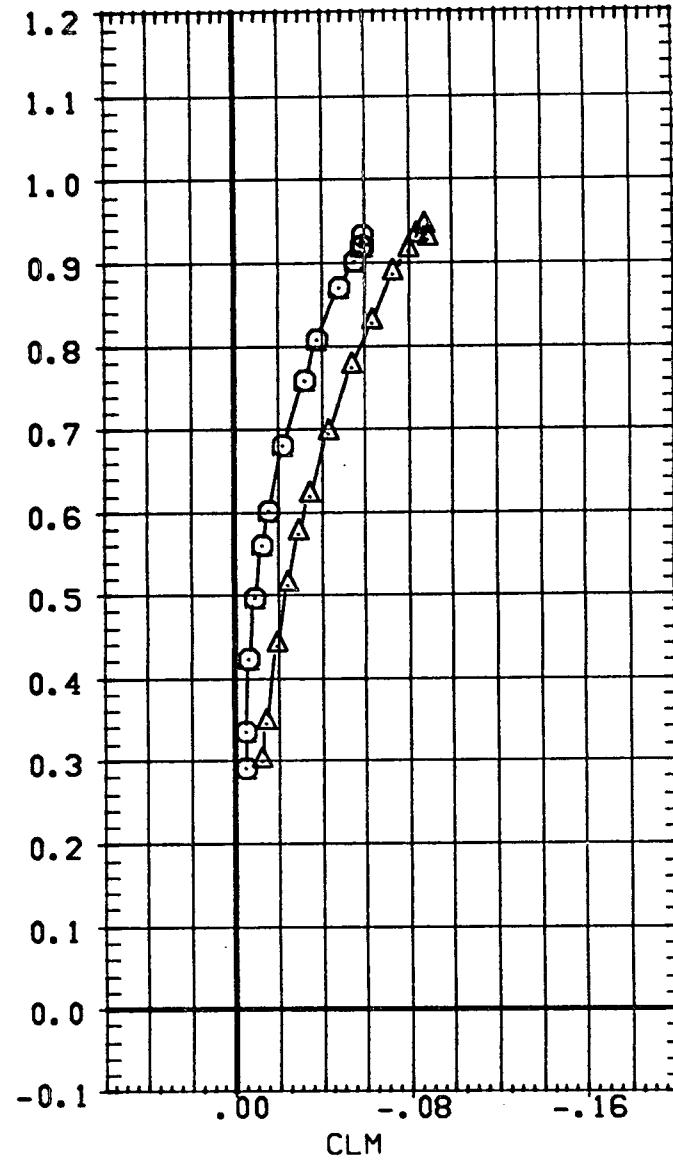
(A)MACH = 20.30

PAGE 11

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(S03007)	LRC 22HE-409,ATP ORB (B1C1D1F1H1) (W1XE1) (V1K1R1)	-20.000	20.000	0.000	0.000	LREF	2.3400 INCHES
						BREF	4.7630 INCHES
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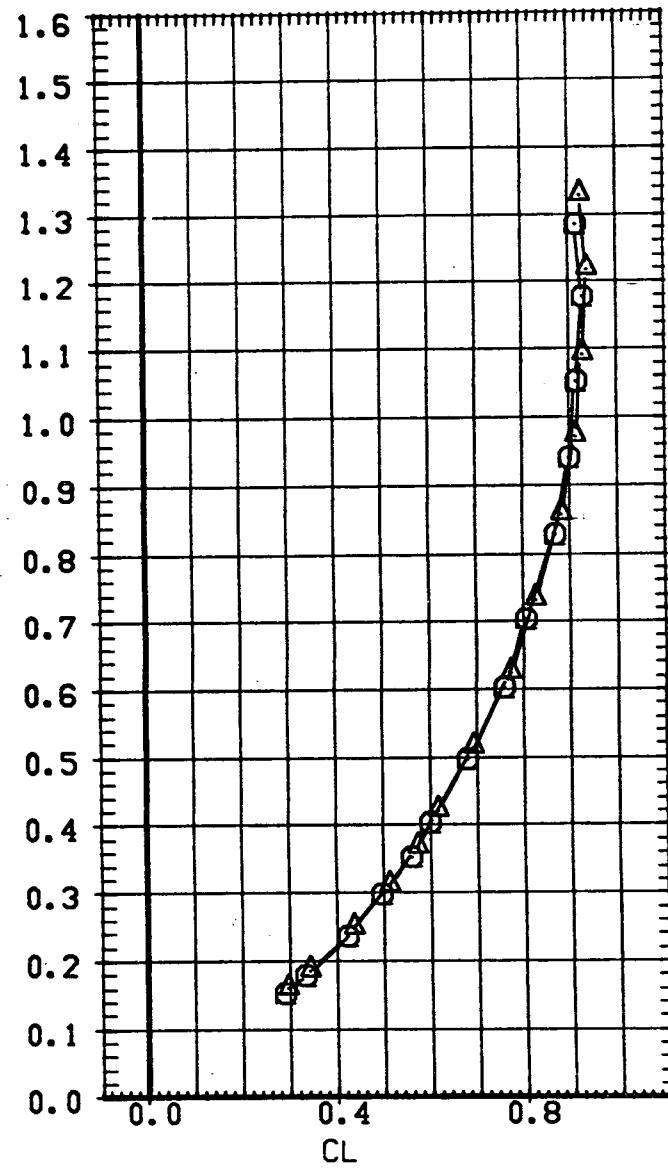
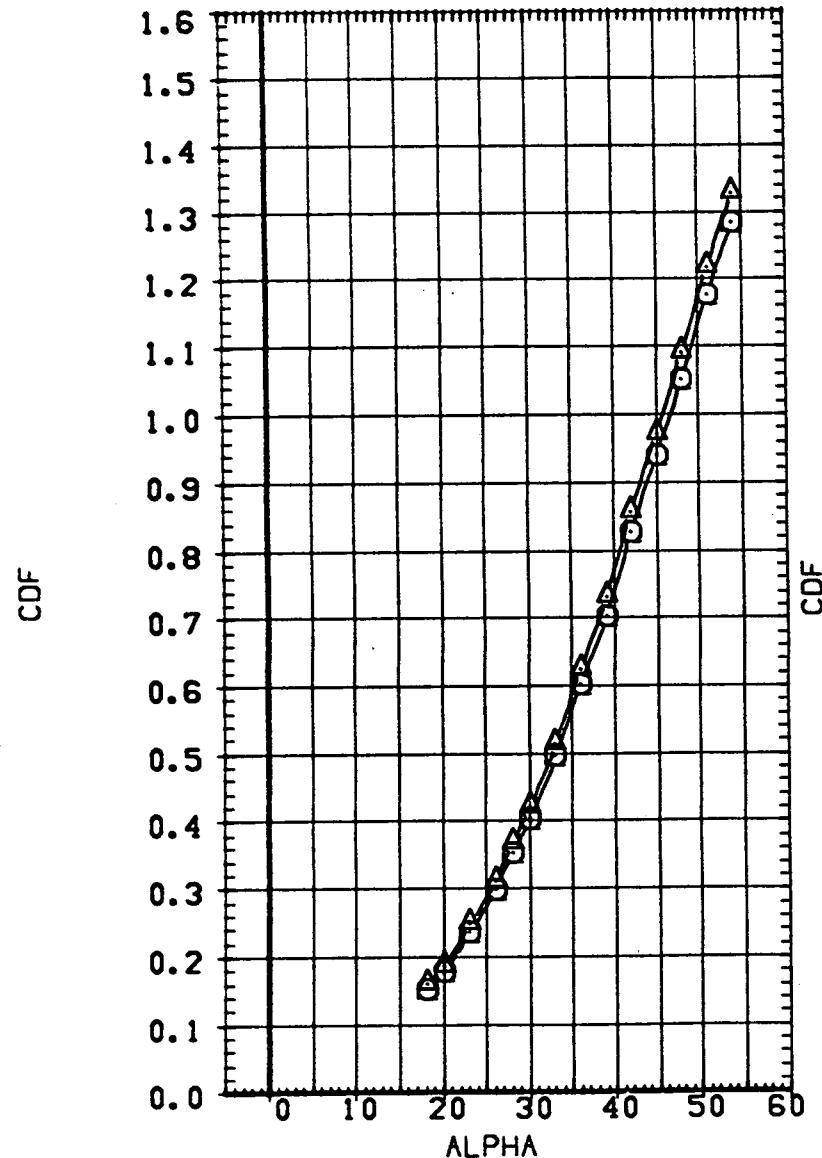


EFFECT OF AILERON DEFLECTION ON LONGITUDINAL CHARACT. OF MODIFIED ORBITER
 (A)MACH = 20.30



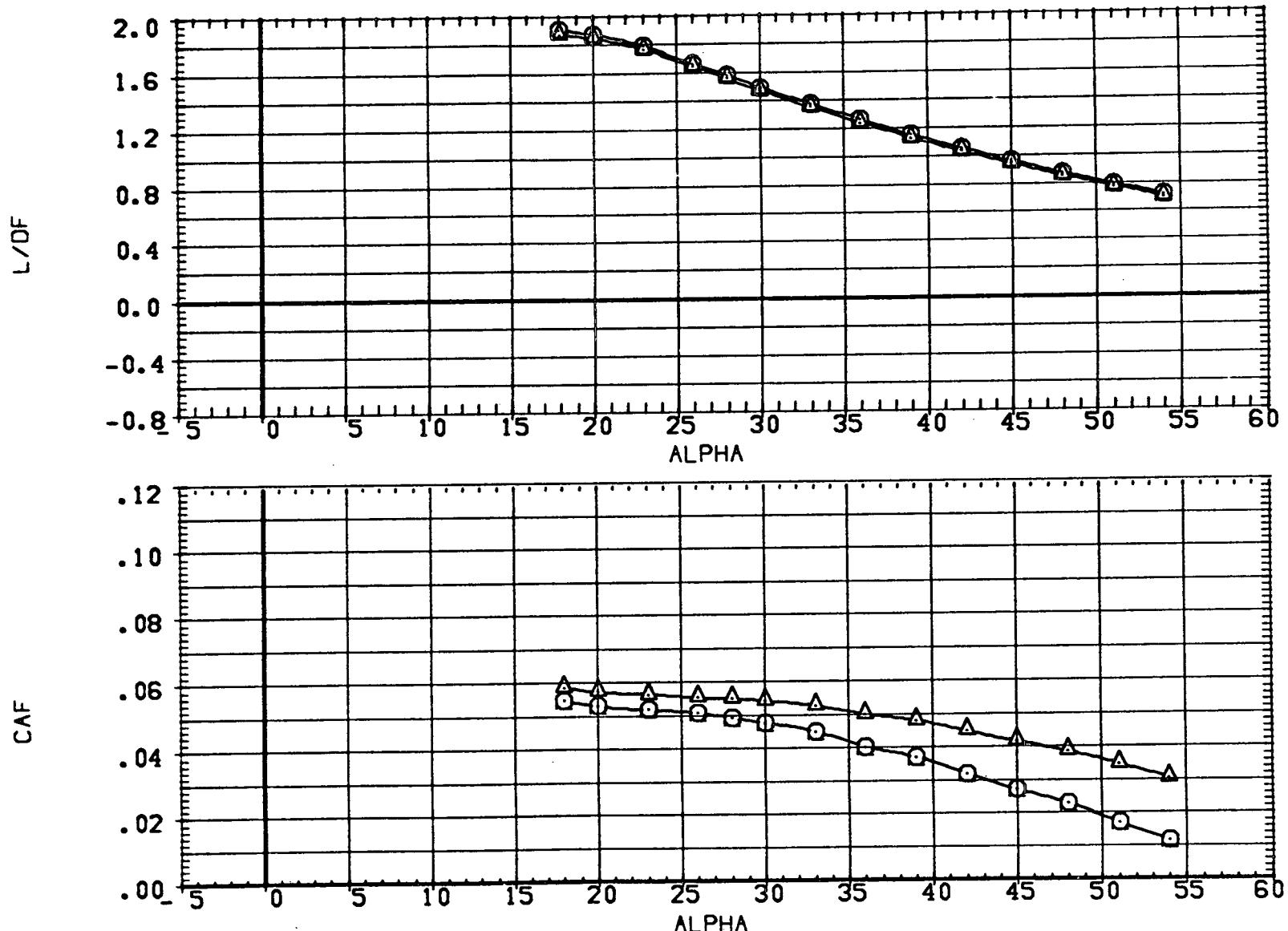
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 (S03007)  LRC 22HE-409, ATP ORB (B1C1D1F1H1) (W1X1) (V1K1R1)

ELEVTR	AILRON	RUDER	BDFLAP	REFERENCE INFORMATION
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				BREF 4.7650 INCHES
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				YMRP 0.0000 INCHES
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EFFECT OF AILERON DEFLECTION ON LONGITUDINAL CHARACT. OF MODIFIED ORBITER
 (A)MACH = 20.30

DATA SET SYMBOL	CONFIGURATION DESCRIPTION	ELEVTR	AILRON	RUDDER	BDFLAP	REFERENCE INFORMATION
(S05002)	LRC 22HE-409,ATP ORB (B1C1D1F1H1) (W1X1E1) (V1K1R1)	-20.000	0.000	0.000	0.000	SREF 9.3900 SQ.IN.
(S05007)	LRC 22HE-409,ATP ORB (B1C1D1F1H1) (W1X1E1) (V1K1R1)	-20.000	20.000	0.000	0.000	LREF 2.3400 INCHES
						BREF 4.7630 INCHES
						XMRP 3.8850 INCHES
						YMRP 0.0000 INCHES
						ZMRP 0.0000 INCHES
						SCALE 0.0045



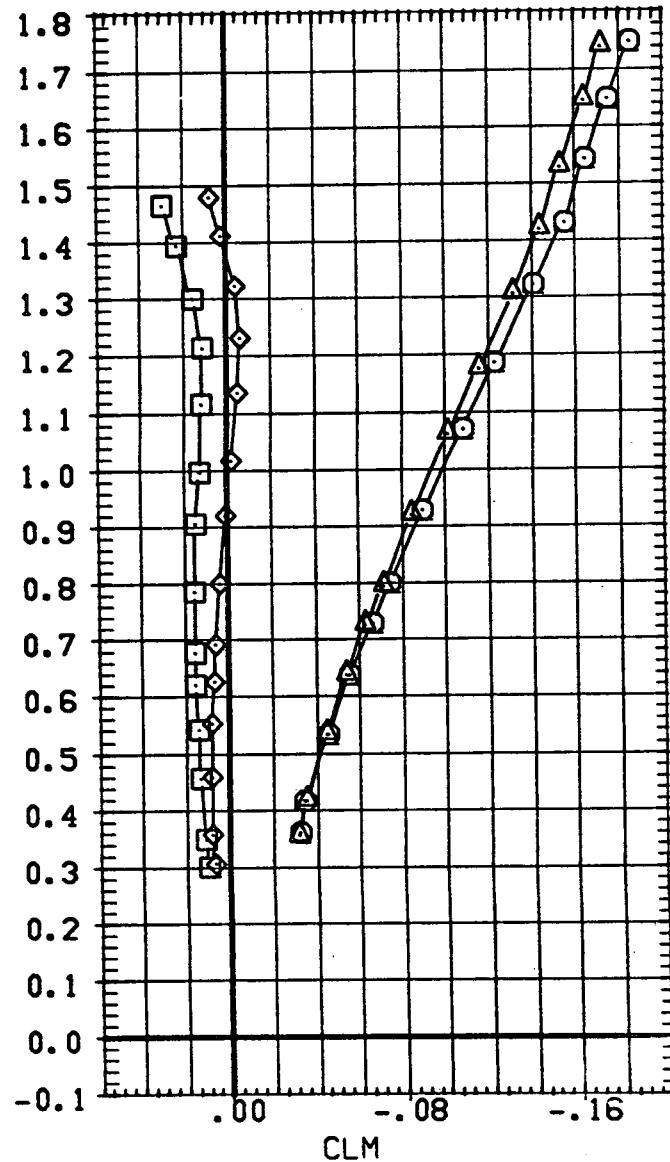
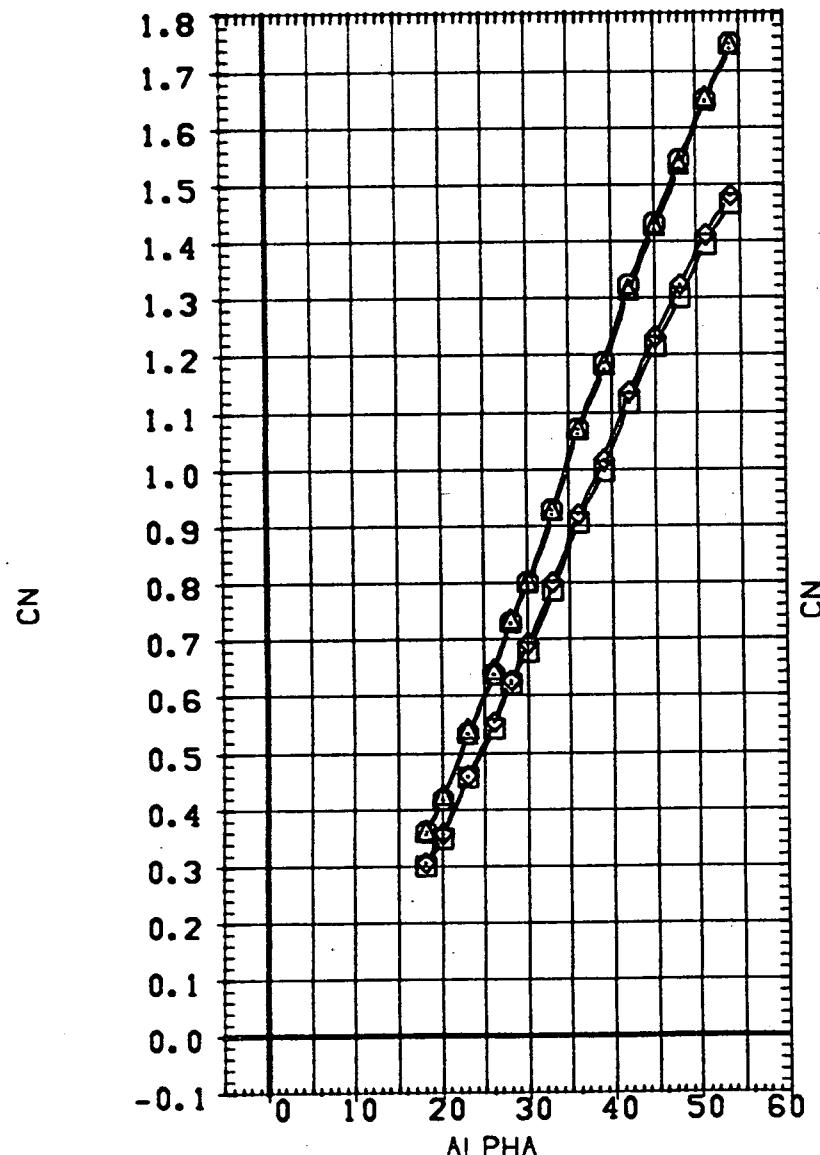
EFFECT OF AILERON DEFLECTION ON LONGITUDINAL CHARACT. OF MODIFIED ORBITER

(A)MACH = 20.30

PAGE 14

DATA SET SYMBOL CONFIGURATION DESCRIPTION
 (S03001)  LRC 22HE-409,ATP ORB (B1C1D1F1M1) (W1XE1) (V1K1R1)
 (S03002)  LRC 22HE-409,ATP ORB (B1C1D1F1M1) (W1XE1) (V1K1R1)
 (S03003)  LRC 22HE-409,ATP ORB (B1C1D1F1M1) (W1XE1) (V1K1R1)
 (S03004)  LRC 22HE-409,ATP ORB (B1C1D1F1M1) (W1XE1) (V1K1R1)

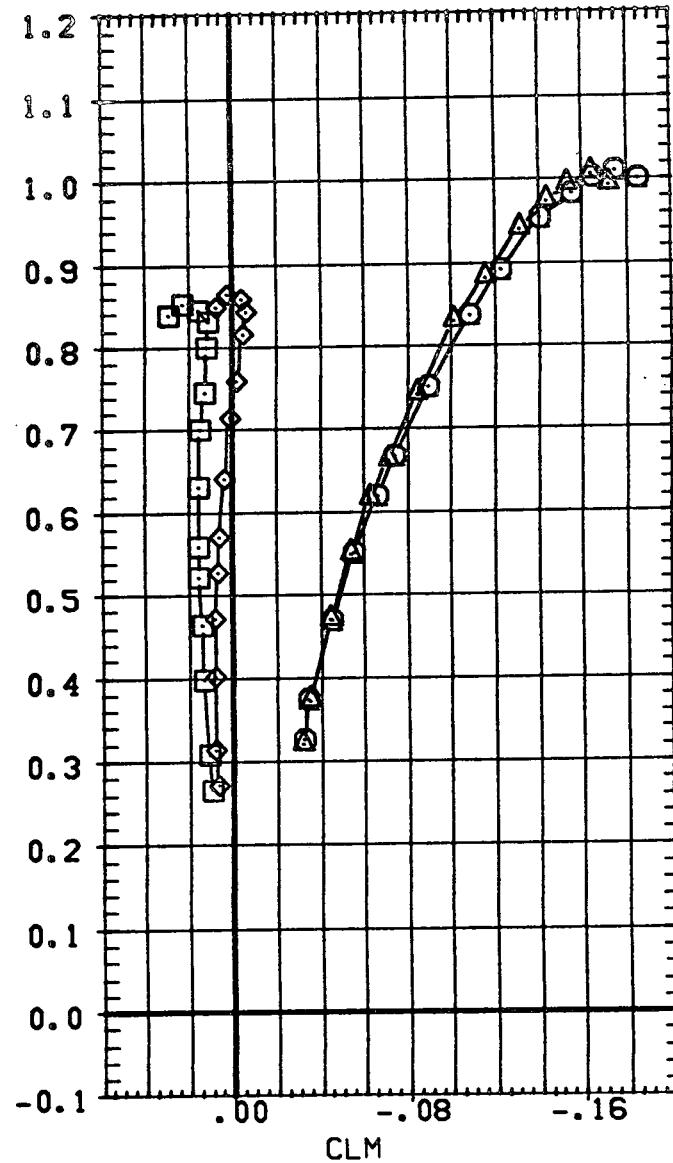
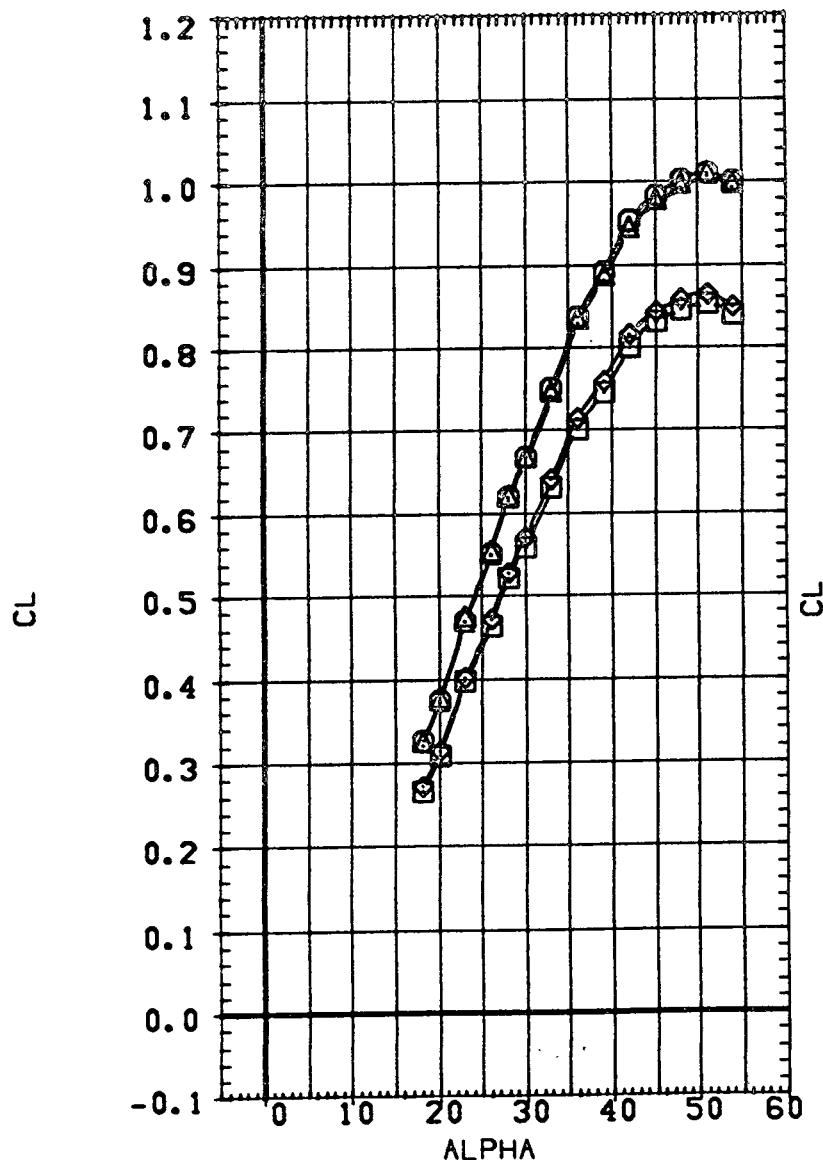
ELEVTR AILRDN RUDDER BDFLAP REFERENCE INFORMATION
 0.000 0.000 0.000 0.000 SREF 9.3900 30. IN.
 0.000 0.000 -10.000 LREF 2.3400 INCHES
 -40.000 0.000 0.000 0.000 BREF 4.7630 INCHES
 -40.000 0.000 0.000 -10.000 XMRP 3.8850 INCHES
 0.000 0.000 0.000 0.000 YMRP 0.0000 INCHES
 0.000 0.000 0.000 0.000 ZMRP 0.0000 INCHES
 SCALE 0.0045



EFFECT OF BODY FLAP ON LONGITUDINAL CHARACTERISTICS OF MODIFIED ORBITER

CARMACH = 20.30

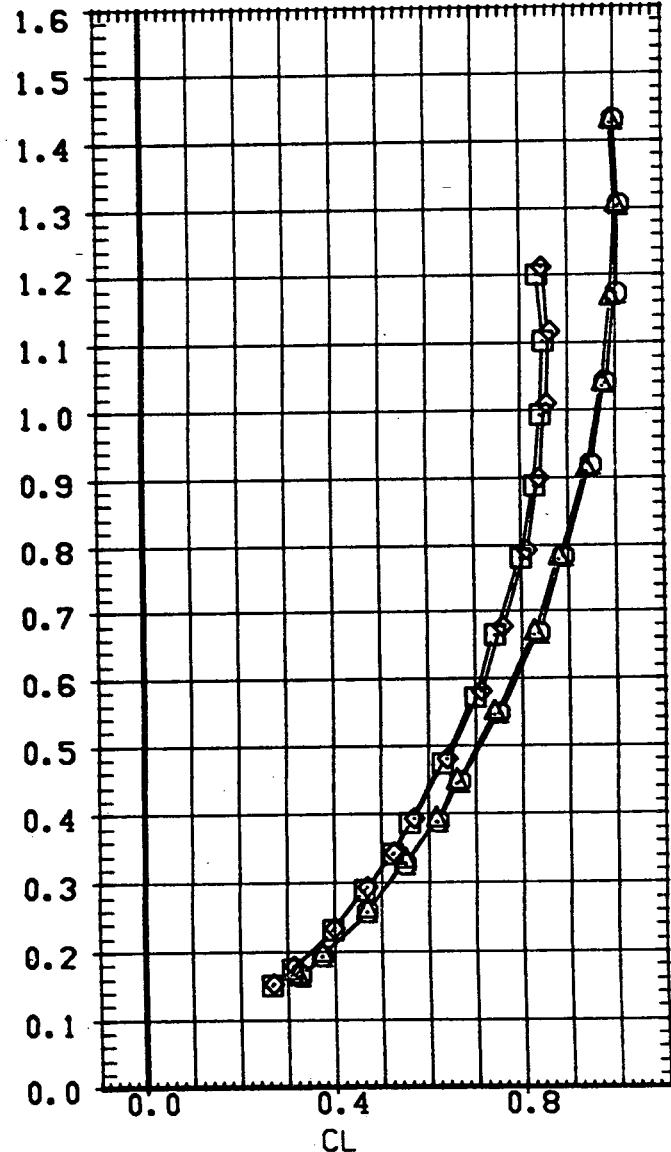
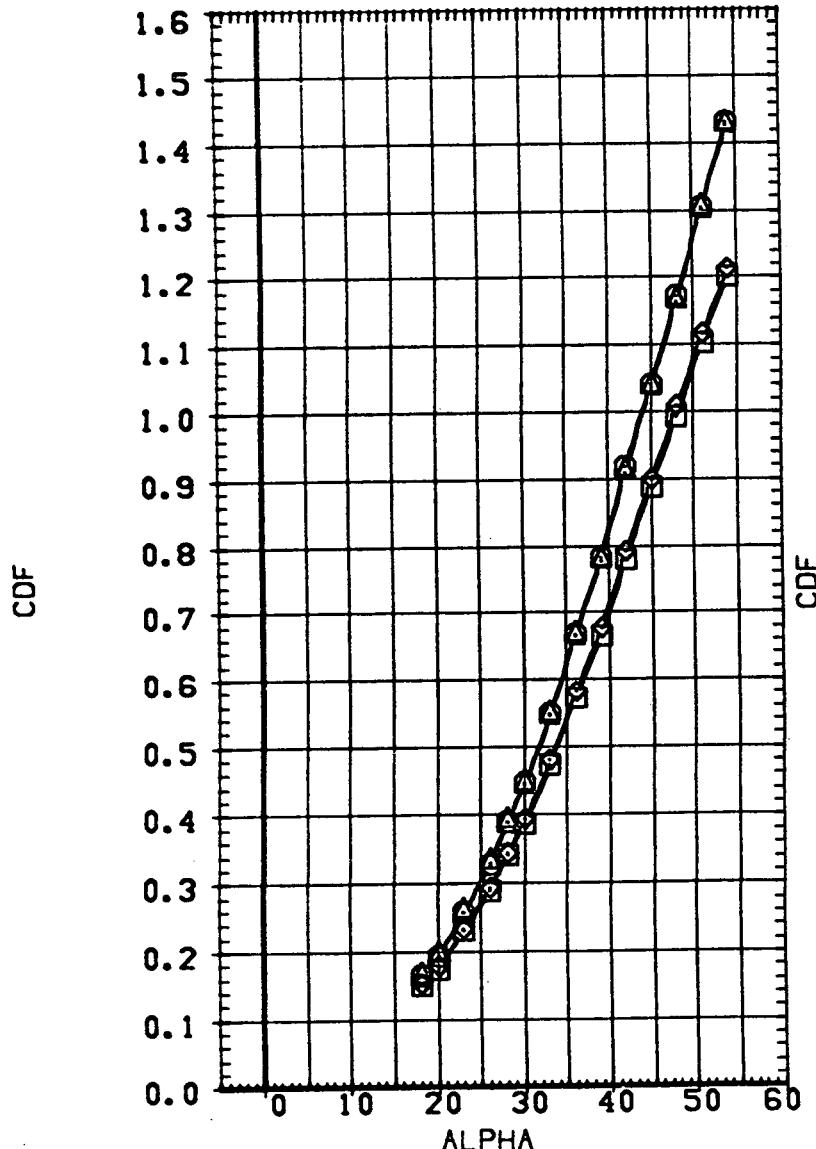
DATA SET SYMBOL	CONFIGURATION DESCRIPTION	ELEVTR	AIRLON	RUDDER	BDFLAP	REFERENCE INFORMATION
(S05001)	LRC 22ME-409,ATP ORB (S1C101F1M1) (W1X21) (V1K1R1)	0.000	0.000	0.000	0.000	SREF 0.3000 00. IN.
(S05002)	LRC 22ME-409,ATP ORB (S1C101F1M1) (W1X21) (V1K1R1)	0.000	0.000	0.000	-18.000	LREF 2.3400 INCHES
(S05003)	LRC 22ME-409,ATP ORB (S1C101F1M1) (W1X21) (V1K1R1)	-40.000	0.000	0.000	0.000	BREF 4.7030 INCHES
(S05004)	LRC 22ME-409,ATP ORB (S1C101F1M1) (W1X21) (V1K1R1)	-40.000	0.000	0.000	-18.000	XMRP 3.0050 INCHES
					ZMRP 0.0000 INCHES	
					SCALE 0.0045	



EFFECT OF BODY FLAP ON LONGITUDINAL CHARACTERISTICS OF MODIFIED ORBITER
(A)MACH = 20.30

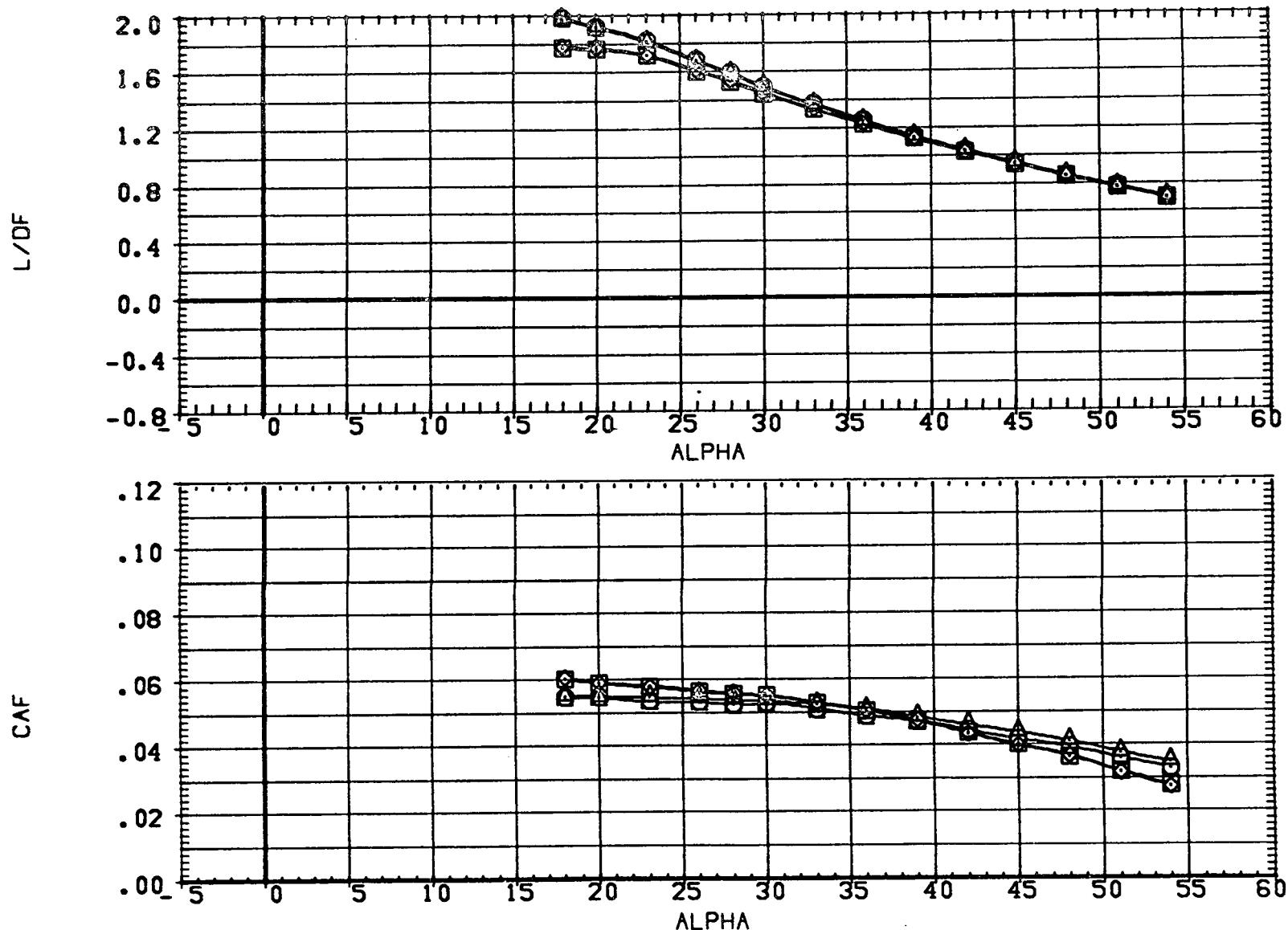
DATA SET SYMBOL CONFIGURATION DESCRIPTION
 (S03001) LRC 22HE-409,ATP ORB (B1C1D1F1M1) (W1X1E1) (V1K1R1)
 (S03005) LRC 22HE-409,ATP ORB (B1C1D1F1M1) (W1X1E1) (V1K1R1)
 (S03003) LRC 22HE-409,ATP ORB (B1C1D1F1M1) (W1X1E1) (V1K1R1)
 (S03004) LRC 22HE-409,ATP ORB (B1C1D1F1M1) (W1X1E1) (V1K1R1)

ELEVTR	AIRLON	RUDER	BDFLAP	REFERENCE INFORMATION
0.000	0.000	0.000	0.000	SREF 9.3900 SQ. IN.
0.000	0.000	-18.000	0.000	LREF 2.3400 INCHES
-40.000	0.000	0.000	0.000	BREF 4.7630 INCHES
-40.000	0.000	0.000	-18.000	XMRP 3.6650 INCHES
				YMRP 0.0000 INCHES
				ZMRP 0.0000 INCHES
				SCALE 0.0045



EFFECT OF BODY FLAP ON LONGITUDINAL CHARACTERISTICS OF MODIFIED ORBITER
 (A)MACH = 20.30

DATA SET SYMBOL	CONFIGURATION DESCRIPTION	ELEVTR	AILRON	RUDER	BDPLAP	REFERENCE INFORMATION
(S03001)	LRC 22ME-409,ATP ORB (B1C1D1F1M1) (W1X21) (V1K1R1)	0.000	0.000	0.000	0.000	SREP 9.3900 SQ.IN.
(S03005)	LRC 22ME-409,ATP ORB (B1C1D1F1M1) (W1X21) (V1K1R1)	0.000	0.000	-18.000	0.000	LREF 2.3400 INCHES
(S03003)	LRC 22ME-409,ATP ORB (B1C1D1F1M1) (W1X21) (V1K1R1)	-40.000	0.000	0.000	0.000	BREP 4.7650 INCHES
(S03004)	LRC 22ME-409,ATP ORB (B1C1D1F1M1) (W1X21) (V1K1R1)	-40.000	0.000	0.000	-18.000	XMRP 3.0050 INCHES
						YMRP 0.0000 INCHES
						ZMRP 0.0000 INCHES
						SCALE 0.0045



EFFECT OF BODY FLAP ON LONGITUDINAL CHARACTERISTICS OF MODIFIED ORBITER

(A)MACH = 20.30

PAGE 18

APPENDIX
TABULATED SOURCE DATA

Page 1

Plotted data tabulations available
on request from the DMS.

DATE 26 MAR 73

SOURCE DATA TABULATION, LARC TEST 22-409

PAGE 1 - a

LRC 22ME-409, ATP ORB (B1C1D1F1M1) (W1X1E1) (V1K1R1)

(R06001) (27 NOV 72)

REFERENCE DATA				PARAMETRIC DATA			
SREF =	9.3900 SQ. IN.	XMRP =	3.8850 INCHES	BETA =	.000	ELEVTR =	.000
LREF =	5.9720 INCHES	YMRP =	.0000 INCHES	AILRON =	.000	RUDDER =	.000
BREF =	4.7630 INCHES	ZMRP =	.0000 INCHES	BOFLAP =	.000		
SCALE =	.0043						

RUN NO. 1/0 RN/L = 4.30 GRADIENT INTERVAL = 18.00/ 30.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	18.000	.00000	.35912	.05468	-.01257	-.00099	.00048	-.00210	.32459	.16317	1.98923
20.300	20.000	.00000	.41690	.05465	-.01352	-.00114	.00049	-.00262	.37306	.19395	1.92354
20.300	23.000	.00000	.53330	.05334	-.01780	-.00161	.00054	-.00334	.47006	.25747	1.82569
20.300	26.000	.00000	.63939	.05316	-.02175	-.00209	.00053	-.00368	.55138	.32808	1.68064
20.300	28.000	.00000	.72930	.05241	-.02601	-.00253	.00054	-.00498	.61933	.38866	1.59349
20.300	30.000	.00000	.80118	.05260	-.02901	-.00245	.00058	-.00463	.66754	.44614	1.49625
20.300	33.000	.00000	.92817	.05098	-.03503	-.00310	.00066	-.00606	.75066	.54828	1.36913
20.300	36.000	.00000	1.06938	.04891	-.04247	-.00329	.00065	-.00647	.83640	.66814	1.25183
20.300	39.000	.00000	1.18583	.04718	-.04815	-.00370	.00070	-.00745	.89167	.78293	1.13915
20.300	42.000	.00000	1.32226	.04442	-.05526	-.00406	.00084	-.00816	.95291	.91777	1.03828
20.300	45.000	.00000	1.43161	.04161	-.06095	-.00471	.00087	-.00910	.98288	1.04173	.94351
20.300	48.000	.00000	1.54297	.03928	-.06450	-.00480	.00090	-.00937	1.00326	1.17293	.85535
20.300	51.000	.00000	1.64921	.03596	-.06846	-.00471	.00101	-.01038	1.00993	1.30430	.77431
20.300	54.000	.00000	1.74621	.03291	-.07257	-.00399	.00114	-.01013	.99977	1.43205	.69814
	GRADIENT	.00000	.03737	-.00021	-.00142	-.00014	.00001	-.00023	.02917	.02370	-.04129

LRC 22ME-409,ATP CRB (28C101F1H1) (MAX1) (V1K1R1)

(106002) (27 NOV 72)

REFERENCE DATA

XREP = 9.3900 SQ. IN. XMRP = 3.8630 INCHES
 LREP = 9.9720 INCHES YMRE = .0000 INCHES
 BREP = 4.7650 INCHES ZMRP = .0000 INCHES
 SCALE = .0045

PARAMETRIC DATA

BETA = .000 ELEVTR = -20.000
 AILRDN = .000 RUDDER = .000
 BDFLAP = .000

RUN NO. 2/0 RVAL = 4.30 GRADIENT INTERVAL = 10.00/30.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	18.000	.00000	.32225	.05465	-.00168	.00078	-.00026	.00013	.28959	.15156	1.91072
20.300	20.000	.00000	.37510	.05300	-.00175	.00079	-.00024	.00004	.33435	.17810	1.87735
20.300	22.000	.00000	.48059	.05163	-.00259	.00079	-.00034	.00047	.42213	.23549	1.79259
20.300	24.000	.00000	.57772	.05036	-.00366	.00068	-.00034	.00080	.49704	.29876	1.66354
20.300	26.000	.00000	.66045	.04932	-.00509	.00045	-.00069	.00071	.55999	.35361	1.56365
20.300	28.000	.00000	.72248	.04769	-.00612	.00062	-.00074	.00135	.60184	.40254	1.49512
20.300	30.000	.00000	.84191	.04490	-.00872	.00043	-.00096	.00129	.68163	.49620	1.37371
20.300	32.000	.00000	.96859	.04032	-.01273	.00018	-.00112	.00152	.75991	.60194	1.26243
20.300	34.000	.00000	1.07051	.03710	-.01484	.00024	-.00131	.00184	.80859	.70253	1.15097
20.300	42.000	.00000	1.20079	.03194	-.01687	.00017	-.00151	.00256	.87099	.82722	1.05290
20.300	45.000	.00000	1.30221	.02711	-.02186	-.00022	-.00172	.00276	.90163	.93997	.95921
20.300	46.000	.00000	1.39753	.02284	-.02281	-.00022	-.00176	.00349	.91816	1.05385	.87124
20.300	51.000	.00000	1.50144	.01692	-.02320	-.00031	-.00178	.00361	.93174	1.17749	.79130
20.300	54.000	.00000	1.58027	.01169	-.02304	.00008	-.00183	.00387	.91940	1.28534	.71530
	GRADIENT	.00000	.03395	-.00053	-.00037	-.00002	-.00005	.00010	.02662	.02113	-.03542

LRC 22-409, ATP ORB (B1C1D1F1H1) (W1X1E1) (V1K1R1)

(ROS003) (27 NOV 72)

REFERENCE DATA

SRDP = 9.3900 SQ.IN. XMRP = 3.8850 INCHES
 LRDP = 5.9720 INCHES YMRP = .0000 INCHES
 BRDP = 4.7630 INCHES ZMRP = .0000 INCHES
 SCALE = .0045

PARAMETRIC DATA

BETA = .000 ELEVTR = -40.000
 AILRON = .000 RUDDER = .000
 BOFLAP = .000

RUN NO. 3/0 RN/L = 4.30 GRADIENT INTERVAL = 18.00/30.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	18.000	.00000	.30460	.06058	.00259	.00071	.00016	-.00069	.27097	.15174	1.78577
20.300	20.000	.00000	.35600	.05910	.00321	.00043	.00009	-.00069	.31432	.17730	1.77280
20.300	23.000	.00000	.46003	.05797	.00333	.00037	-.00007	-.00046	.40081	.23311	1.71938
20.300	26.000	.00000	.53185	.05658	.00315	.00016	-.00018	-.00037	.47120	.29277	1.60943
20.300	28.000	.00000	.62600	.05569	.00268	.00009	-.00029	-.00039	.52835	.34400	1.53587
20.300	30.000	.00000	.69154	.05500	.00234	-.00003	-.00040	-.00010	.57139	.39341	1.45242
20.300	33.000	.00000	.79921	.05294	.00153	-.00020	-.00051	-.00032	.64144	.47968	1.33722
20.300	36.000	.00000	.91936	.05024	.00026	-.00036	-.00072	-.00009	.71425	.58103	1.22929
20.300	39.000	.00000	1.01662	.04763	-.00071	-.00033	-.00082	-.00015	.76009	.67680	1.12307
20.300	42.000	.00000	1.13574	.04340	-.00199	-.00068	-.00090	.00029	.81498	.79221	1.02874
20.300	45.000	.00000	1.23129	.03981	-.00249	-.00110	-.00110	.00034	.84250	.89880	.93736
20.300	48.000	.00000	1.32462	.03665	-.00147	-.00114	-.00109	.00032	.85910	1.00891	.85152
20.300	51.000	.00000	1.41198	.03175	.00083	-.00103	-.00120	.00068	.86391	1.11730	.77321
20.300	54.000	.00000	1.47994	.02730	.00292	-.00080	-.00123	.00104	.84780	1.21334	.69874
	GRADIENT	.00000	.03266	-.00045	-.00003	-.00006	-.00005	.00005	.02549	.02025	-.02843

LRC 22K2-409, ATP ORD (B1C1D1F1M1) (M1K1) (V1K1R1)

(R0G004) (27 NOV 72)

REFERENCE DATA

XREP = 5.3900 50. IN. XMRP = 5.0650 INCHES
 LREP = 5.3720 INCHES YMRP = .0000 INCHES
 BREP = 4.7650 INCHES ZMRP = .0000 INCHES
 SCALE = .0040

PARAMETRIC DATA

BETA = .000 ELEVTR = -40.000
 AILRDN = .000 RUDDER = .000
 BOFLAP = -16.000

RUN NO. S/0 RNVL = 4.50 GRADIENT INTERVAL = 10.00/30.00

MACH	ALPHA	BETA	CN	CAF	CLM	CLL	CYN	CY	CL	CDF	L/D ²
20.300	18.000	.00000	.29982	.06009	.00387	.00046	-.00011	-.00042	.26543	.14943	1.77932
20.300	20.000	.00000	.34926	.05883	.00446	.00034	-.00015	-.00063	.30807	.17476	1.76286
20.300	25.000	.00000	.45546	.05772	.00515	.00016	-.00025	-.00102	.39670	.23109	1.71660
20.300	26.000	.00000	.54263	.05629	.00560	.00012	-.00032	-.00057	.46304	.28847	1.60914
20.300	26.000	.50000	.62158	.05564	.00599	.00000	-.00037	-.00076	.52270	.34094	1.53310
20.300	30.000	.00000	.67728	.03493	.00594	-.00007	-.00051	-.00017	.55906	.38620	1.44759
20.300	33.000	.00000	.73580	.03207	.00592	-.00017	-.00067	-.00002	.63023	.47232	1.33434
20.300	36.000	.00000	.90411	.03044	.00569	-.00063	-.00088	-.00059	.70179	.57229	1.22642
20.300	39.000	.00000	.99762	.04728	.00504	-.00071	-.00098	-.00013	.74534	.68437	1.12104
20.300	42.000	.00000	1.11558	.04363	.00476	-.00088	-.00117	-.00071	.79981	.77089	1.02686
20.300	45.000	.00000	1.21464	.04001	.00428	-.00129	-.00137	-.00045	.83073	.88731	.93624
20.300	48.000	.00000	1.30163	.03646	.00603	-.00140	-.00147	-.00037	.84400	.99185	.85093
20.300	51.000	.00000	1.39406	.03192	.00682	-.00146	-.00157	-.00031	.85250	1.10348	.77256
20.300	54.000	.00000	1.43508	.02763	.01147	-.00140	-.00164	-.00014	.83880	1.20151	.69812
	GRADIENT	.00000	.03216	-.00042	.00018	-.00004	-.00003	.00001	.02509	.01993	-.02791

DATE 26 MAR 73

SOURCE DATA TABULATION, LARC TEST 22-409

PAGE 5

LRC 22ME-409, ATP ORB (B1C1D1F1H1) (W1X1E1) (V1K1R1)

(ROS003) (27 NOV 72)

REFERENCE DATA				PARAMETRIC DATA			
BREP =	9.3900 SQ.IN.	XMRP =	3.8850 INCHES	BETA =	.000	ELEVTR =	.000
UREP =	5.9720 INCHES	YMRP =	.0000 INCHES	AILRON =	.000	RUDDER =	.000
BREP =	4.7630 INCHES	ZMRP =	.0000 INCHES	BOFLAP =	-18.000		
SCALE =	.0043						

RUN NO. 6/0 RN/L = 4.30 GRADIENT INTERVAL = 10.00/30.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	18.000	.00000	.35437	.05498	-.01233	-.00012	-.00023	-.00025	.32003	.16180	1.97802
20.300	20.000	.00000	.41563	.05469	-.01377	-.00025	-.00021	-.00012	.37179	.19374	1.91905
20.300	23.000	.00000	.53290	.05451	-.01744	-.00074	-.00034	-.00002	.46924	.25840	1.81592
20.300	26.000	.00000	.63765	.05419	-.02127	-.00083	-.00043	.00031	.54954	.32632	1.67377
20.300	28.000	.00000	.72593	.05363	-.02469	-.00098	-.00043	.00035	.61569	.38834	1.58545
20.300	30.000	.00000	.79498	.05344	-.02791	-.00109	-.00054	.00110	.66175	.44377	1.49119
20.300	33.000	.00000	.91861	.05230	-.03305	-.00148	-.00061	.00033	.74192	.54417	1.36341
20.300	36.000	.00000	1.06118	.05079	-.03966	-.00204	-.00076	.00066	.82866	.66484	1.24640
20.300	39.000	.00000	1.17479	.04844	-.04519	-.00225	-.00093	.00058	.88250	.77697	1.13583
20.300	42.000	.00000	1.30767	.04601	-.05164	-.00215	-.00098	.00109	.94115	.90933	1.03500
20.300	45.000	.00000	1.42055	.04370	-.05643	-.00253	-.00101	.00138	.97358	1.03538	.94031
20.300	48.000	.00000	1.52868	.04106	-.06015	-.00303	-.00102	.00170	.99237	1.16351	.85291
20.300	51.000	.00000	1.64442	.03763	-.06418	-.00307	-.00107	.00200	1.00562	1.30164	.77258
20.300	54.000	.00000	1.73791	.03482	-.06746	-.00270	-.00102	.00236	.99335	1.42646	.69637
	GRADIENT	.00000	.03722	-.00013	-.00131	-.00008	-.00003	.00010	.02901	.02364	-.04105

DATE 26 MAR 73

SOURCE DATA TABULATION, LARC TEST 22-400

PAGE 6

LRC 22ME-409, ATP ORB (B1C1D1F1H1) (W1E1) (V1K1R1)

(R05006) (27 NOV 72)

REFERENCE DATA

STEP = 9.3900 SQ.IN. XMRP = 3.6850 INCHES
 LREP = 5.9720 INCHES YMRP = .0000 INCHES
 BREP = 4.7630 INCHES ZMRP = .0000 INCHES
 SCALE = .0045

PARAMETRIC DATA

BETA = .000 ELEVTR = -30.000
 AILRDN = 10.000 RUDDER = .000
 BOFLAP = .000

RUN NO. T/0 RN/L = 4.30 GRADIENT INTERVAL = 10.00/30.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/D ^F
20.300	18.000	.00000	.31291	.05781	.00041	.00345	.00119	-.00077	.27973	.15168	1.84426
20.300	20.000	.00000	.36471	.05572	.00086	.00342	.00110	-.00019	.32332	.17604	1.81602
20.300	23.000	.00000	.47121	.03529	.00048	.00350	.00086	-.00056	.41215	.23501	1.75375
20.300	26.000	.00000	.56397	.05408	-.00023	.00375	.00058	-.00027	.48318	.29583	1.63332
20.300	28.000	.00000	.64477	.05307	-.00026	.00430	.00043	.00072	.54438	.34956	1.55733
20.300	30.000	.00000	.70462	.05193	-.00198	.00445	.00029	.00078	.58423	.39732	1.47041
20.300	33.000	.00000	.81980	.04967	-.00373	.00497	.00007	.00111	.66049	.48615	1.35305
20.300	36.000	.00000	.94311	.04637	-.00596	.00367	-.00016	.00127	.73573	.59186	1.24308
20.300	39.000	.00000	1.05138	.04336	-.00805	.00645	-.00035	.00201	.78977	.69534	1.13581
20.300	42.000	.00000	1.17108	.03674	-.01057	.00731	-.00049	.00220	.84436	.81240	1.03935
20.300	45.000	.00000	1.27057	.03420	-.01213	.00790	-.00061	.00242	.87424	.92261	.94758
20.300	48.000	.00000	1.36989	.03087	-.01226	.00899	-.00077	.00325	.89369	1.03868	.86041
20.300	51.000	.00000	1.46040	.02560	-.01089	.00992	-.00084	.00406	.89916	1.15106	.78116
20.300	54.000	.00000	1.54139	.02125	-.00918	.01098	-.00102	.00453	.88883	1.25949	.70570
	GRADIENT	.00000	.03323	-.00047	-.00020	.00009	-.00008	.00013	.02598	.02066	-.03165

DATE 26 MAR 73

SOURCE DATA TABULATION, LARC TEST 22-409

PAGE 7

LRC 22ME-409, ATP CRB (B1C1D1F1H1) (W1X1E1) (V1K1R1)

(ROS007) (27 NOV 72)

REFERENCE DATA

SREF = 9.3900 SQ.IN. XMRP = 3.8850 INCHES
 LREF = 5.9720 INCHES YMRP = .0000 INCHES
 BREF = 4.7630 INCHES ZMRP = .0000 INCHES
 SCALE = .0045

PARAMETRIC DATA

BETA = .000 ELEVTR = -20.000
 AILRDN = 20.000 RUDDER = .000
 BOFLAP = .000

RUN NO. 4/0 RN/L = 4.30 GRADIENT INTERVAL = 18.00/ 30.00

MACH	ALPHA	BETA	CN	CAF	CLW	CBL	CYN	CY	CL	CDF	L/DF
20.300	18.000	.00000	.33179	.05854	-.00485	.00905	.00062	.00027	.29747	.15820	1.88031
20.300	20.000	.00000	.38668	.05728	-.00553	.00993	.00026	.00108	.34396	.18815	1.84778
20.300	23.000	.00000	.49915	.05644	-.00755	.01168	-.00021	.00185	.43742	.24699	1.77101
20.300	26.000	.00000	.59638	.05534	-.00954	.01357	-.00070	.00256	.51176	.31117	1.64462
20.300	28.000	.00000	.67971	.05494	-.01157	.01508	-.00104	.00283	.57436	.36762	1.56238
20.300	30.000	.00000	.74529	.05426	-.01364	.01638	-.00135	.00350	.61830	.41965	1.47336
20.300	33.000	.00000	.86223	.05273	-.01695	.01859	-.00192	.00435	.69442	.51384	1.35144
20.300	36.000	.00000	.99366	.05007	-.02126	.02122	-.00257	.00557	.77446	.62457	1.23998
20.300	39.000	.00000	1.10304	.04808	-.02481	.02332	-.00309	.00587	.82696	.73153	1.13046
20.300	42.000	.00000	1.23094	.04477	-.02860	.02535	-.00359	.00675	.88481	.85692	1.03254
20.300	45.000	.00000	1.33359	.04159	-.03151	.02719	-.00413	.00755	.91358	.97240	.93951
20.300	48.000	.00000	1.43348	.03866	-.03293	.02895	-.00466	.00882	.93045	1.09116	.85272
20.300	51.000	.00000	1.53881	.03469	-.03419	.03183	-.00517	.00975	.94145	1.21771	.77313
20.300	54.000	.00000	1.61950	.03048	-.03470	.03342	-.00577	.01076	.92726	1.32812	.69818
	GRADIENT	.00000	.03497	-.00034	-.00073	.00062	-.00016	.00025	.02728	.02194	-.03456

LRC 22ME-409, ATP CRB (B1C1D1F1H1) (W1X1E1) (V1K1R1)

(ROS008) (27 NOV 72)

REFERENCE DATA

SREF = 9.3900 SQ.IN. XMRP = 3.8850 INCHES
 LREF = 5.9720 INCHES YMRP = .0000 INCHES
 BREF = 4.7630 INCHES ZMRP = .0000 INCHES
 SCALE = .0045

PARAMETRIC DATA

BETA = -3.000 ELEVTR = .000
 AILRDN = .000 RUDDER = .000
 BOFLAP = .000

RUN NO. 8/0 RN/L = 4.30 GRADIENT INTERVAL = 18.00/ 30.00

MACH	ALPHA	BETA	CN	CAF	CLW	CBL	CYN	CY	CL	CDF	L/DF
20.300	18.023	-2.85304	.35420	.05661	-.01308	.00184	.00629	.00310	.31930	.16342	1.95385
20.300	20.025	-2.81693	.41896	.05620	-.01488	.00212	.00607	-.00023	.37439	.19627	1.90749
20.300	23.026	-2.76132	.52367	.05546	-.01633	.00269	.00614	-.00491	.46025	.25589	1.79859
20.300	26.031	-2.69615	.63975	.05494	-.02307	.00324	.00634	-.01029	.55074	.33012	1.66827
20.300	28.033	-2.64656	.73263	.05423	-.02754	.00352	.00656	-.01496	.62121	.39219	1.58394
20.300	30.034	-2.59776	.81563	.05397	-.03154	.00381	.00669	-.01677	.67910	.45496	1.49266
20.300	33.036	-2.51567	.93688	.05328	-.03736	.00415	.00731	-.02519	.75637	.55542	1.36181
20.300	36.037	-2.42667	1.06493	.05152	-.04391	.00431	.00768	-.03117	.83085	.66819	1.24344
20.300	39.038	-2.33102	1.20462	.04915	-.05099	.00461	.00812	-.03783	.90470	.79690	1.13527
20.300	42.039	-2.22698	1.33631	.04687	-.05794	.00487	.00842	-.04417	.96108	.92965	1.03381
20.300	45.039	-2.12084	1.44179	.04464	-.06258	.00490	.00863	-.05038	.98721	1.03175	.93864
20.300	48.039	-2.00669	1.56217	.04236	-.06660	.00505	.00877	-.05626	1.01301	1.18995	.85130
20.300	51.038	-1.88744	1.66959	.03903	-.07143	.00519	.00699	-.06074	1.01948	1.32276	.77072
	GRADIENT	.02043	.03793	-.00023	-.00142	.00017	.00003	-.00177	.02995	.02270	-.03772

H.E.T. 409 NAR ATP CRB(B1C1D1F1M1) (W1E1) (V1K1R1)

(ROS015) (20 NOV 72)

REFERENCE DATA

SREF = 9.3900 SQ.IN. XMRP = 3.6850 INCHES
 LREF = 9.9720 INCHES YMRP = .0000 INCHES
 BREF = 4.5300 INCHES ZMRP = .0000 INCHES
 SCALE = .0045 SCALE

PARAMETRIC DATA

BETA = .000 ELEVTR = .000
 AILRDN = .000 RUDDER = .000
 BOFLAP = .000

RUN NO. 15/0 RN/L = 4.30 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	18.000	.00000	.32012	.05034	-.01203	-.00133	.00036	-.00325	.28884	.14699	1.96504
20.300	20.000	.00000	.38606	.04908	-.01352	-.00172	.00034	-.00325	.34788	.17885	1.94511
20.300	23.000	.00000	.49208	.04785	-.01685	-.00218	.00031	-.00343	.43426	.23632	1.63760
20.300	26.000	.00000	.60386	.04661	-.02113	-.00274	.00026	-.00427	.52681	.30880	1.70597
20.300	28.000	.00000	.67854	.04539	-.02437	-.00290	.00018	-.00395	.57781	.35864	1.61113
20.300	30.000	.00000	.75737	.04464	-.02806	-.00320	.00010	-.00445	.63358	.41734	1.51813
20.300	33.000	.00000	.87935	.04235	-.03375	-.00354	-.00004	-.00483	.71442	.51445	1.38871
20.300	36.000	.00000	.99721	.03993	-.03965	-.00396	-.00016	-.00505	.78329	.61845	1.26655
20.300	39.000	.00000	1.12219	.03648	-.04628	-.00400	-.00024	-.00559	.84915	.73456	1.15399
20.300	42.000	.00000	1.23764	.03288	-.05292	-.00403	-.00035	-.00582	.89775	.85258	1.05298
20.300	45.000	.00000	1.36106	.02946	-.05948	-.00431	-.00043	-.00599	.94158	.98324	.95763
20.300	48.000	.00000	1.46662	.02569	-.06313	-.00445	-.00055	-.00629	.96227	1.10710	.86916
20.300	51.000	.00000	1.55815	.02209	-.06678	-.00519	-.00060	-.00662	.96341	1.22481	.78658
20.300	54.000	.00000	1.64796	.01745	-.07192	-.00498	-.00061	-.00680	.95453	1.34348	.71049
	GRADIENT	.00000	.03602	-.00090	-.00178	-.00010	-.00003	-.00011	.01985	.03422	-.03703

DATE 26 MAR 73

SOURCE DATA TABULATION, LARC TEST 22-409

PAGE 9

HE.T. 409 MAR ATP ORB(B1C1D1F1H1) (W1E1) (V1K1R1)

(ROS016) (20 NOV 72)

REFERENCE DATA

SREF = 9.3900 SQ.IN. XMRP = 3.6650 INCHES
 LREF = 5.9720 INCHES YMRP = .0000 INCHES
 BREF = 4.5300 INCHES ZMRP = .0000 INCHES
 SCALE = .0045 SCALE

PARAMETRIC DATA

BETA = .000 ELEVTR = -20.000
 AILRDN = .000 RUDDER = .000
 BDFLAP = .000

RUN NO. 16/0 RN/L = 4.30 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	16.000	.00000	.28496	.05108	-.00143	-.00128	.00016	-.00306	.25523	.13664	1.86792
20.300	20.000	.00000	.34692	.04952	-.00092	-.00147	.00015	-.00359	.30906	.16518	1.87103
20.300	23.000	.00000	.43973	.04790	-.00093	-.00184	.00013	-.00357	.38608	.21591	1.78813
20.300	26.000	.00000	.54275	.04560	-.00145	-.00237	.00003	-.00420	.46783	.27891	1.67734
20.300	28.000	.00000	.60682	.04399	-.00218	-.00255	-.00004	-.00456	.51513	.32372	1.59128
20.300	30.000	.00000	.67512	.04258	-.00307	-.00294	-.00010	-.00500	.56338	.37443	1.50462
20.300	33.000	.00000	.78293	.03878	-.00314	-.00350	-.00028	-.00545	.63550	.45894	1.38470
20.300	36.000	.00000	.89089	.03482	-.00728	-.00371	-.00032	-.00586	.70028	.55183	1.26902
20.300	39.000	.00000	1.00117	.02957	-.00990	-.00414	-.00053	-.00652	.75945	.65303	1.16296
20.300	42.000	.00000	1.10994	.02416	-.01306	-.00412	-.00058	-.00657	.80868	.76065	1.06315
20.300	45.000	.00000	1.21239	.01856	-.01607	-.00457	-.00078	-.00707	.84417	.87041	.96985
20.300	48.000	.00000	1.31632	.01325	-.01734	-.00481	-.00086	-.00725	.87094	.98708	.88234
20.300	51.000	.00000	1.39614	.00816	-.01692	-.00512	-.00096	-.00756	.87228	1.09014	.80016
20.300	54.000	.00000	1.46851	.00199	-.01679	-.00538	-.00102	-.00757	.86156	1.18922	.72448
	GRADIENT	.00000	.03402	-.00138	-.00056	-.00012	-.00004	-.00013	.01814	.03019	-.03432

H.E.T. 409 MAR ATP CRB(B1C1D1F1H1) (W1E1) (V1K1R1)

(ROS017) (20 NOV 72)

REFERENCE DATA

XREP = 9.3900 50.IN. XMRP = 3.8850 INCHES
 LREP = 5.9720 INCHES YMRP = .0000 INCHES
 BREP = 4.5300 INCHES ZMRP = .0000 INCHES
 SCALE = .0045 SCALE

PARAMETRIC DATA

BETA = .000 ELEVTR = -40.000
 AILRON = .000 RUDDER = .000
 BDFLAP = .000

RUN NO. 17/0 RNVL = 4.30 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	CN	CAP	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	18.000	.00000	.27227	.05859	.00269	-.00119	-.00007	-.00297	.24084	.13986	1.72204
20.300	20.000	.00000	.33295	.05572	.00305	-.00126	-.00004	-.00300	.29381	.16623	1.76747
20.300	23.000	.00000	.42378	.05358	.00312	-.00153	.00002	-.00321	.36916	.21490	1.71778
20.300	26.000	.00000	.52790	.05201	.00284	-.00163	-.00001	-.00372	.45168	.27816	1.62379
20.300	28.000	.00000	.58911	.05109	.00275	-.00208	-.00007	-.00401	.49616	.32168	1.54240
20.300	30.000	.00000	.65368	.04966	.00233	-.00226	-.00015	-.00445	.54127	.36984	1.46352
20.300	33.000	.00000	.76272	.04739	.00143	-.00240	-.00026	-.00465	.61386	.45515	1.34869
20.300	36.000	.00000	.66687	.04455	.00036	-.00273	-.00034	-.00499	.67512	.54557	1.23746
20.300	39.000	.00000	.97037	.04080	-.00033	-.00283	-.00048	-.00539	.72844	.64238	1.13397
20.300	42.000	.00000	1.07286	.03709	-.00192	-.00281	-.00060	-.00523	.77247	.74545	1.03625
20.300	45.000	.00000	1.16838	.03313	-.00276	-.00267	-.00076	-.00615	.80274	.84959	.94485
20.300	48.000	.00000	1.26687	.02869	-.00282	-.00304	-.00093	-.00610	.82757	.96229	.86000
20.300	51.000	.00000	1.33539	.02522	-.0025	-.00309	-.00110	-.00671	.82079	1.05367	.77898
20.300	54.000	.00000	1.41267	.02094	.00080	-.00300	-.00118	-.00633	.81340	1.15518	.70414
	GRADIENT	.00000	.03267	-.00102	-.00015	-.00005	-.00003	-.00011	.01705	.02912	-.03176

DATE 26 MAR 73

SOURCE DATA TABULATION, LARC TEST 22-409

PAGE 11

HE.T. 409 NAR ATP CRB(B1C1D1F1H1) (W1E1) (V1K1R1)

(ROS020) (20 NOV 72)

REFERENCE DATA

SREF = 9.3900 SQ.IN. XMRP = 3.8850 INCHES
 LREF = 5.9720 INCHES YMRP = .0000 INCHES
 BREF = 4.5300 INCHES ZMRP = .0000 INCHES
 SCALE = .0045 SCALE

PARAMETRIC DATA

BETA = .000 ELEVTR = .000
 AILRDN = .000 RUDDER = .000
 BDFLAP = .000

RUN NO. 20/0 RN/L = 4.30 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	-1.500	.00000	-.05319	.07313	-.01279	.00086	.00047	-.00500	-.05126	.07450	-.68800
20.300	.000	.00000	-.03601	.07225	-.01252	.00076	.00027	-.00476	-.03801	.07225	-.52615
20.300	2.000	.00000	-.01753	.06986	-.01187	.00035	-.00012	-.00336	-.01995	.06921	-.28630
20.300	4.000	.00000	.01209	.06696	-.01197	.00024	-.00020	-.00227	.00739	.06764	.10925
20.300	6.000	.00000	.04392	.06482	-.01150	.00009	-.00024	-.00125	.03691	.06906	.53442
20.300	8.000	.00000	.07767	.06253	-.01112	-.00017	-.00023	-.00093	.06821	.07273	.93786
20.300	10.000	.00000	.11793	.06078	-.01078	-.00039	-.00017	-.00079	.10558	.08033	1.31429
20.300	12.000	.00000	.16273	.05863	-.01057	-.00056	-.00004	-.00047	.14698	.09118	1.61198
20.300	14.000	.00000	.21531	.05657	-.01082	-.00085	-.00009	-.00041	.19523	.10698	1.82488
20.300	16.000	.00000	.26706	.05426	-.01128	-.00101	-.00012	-.00001	.24176	.12577	1.92230
20.300	18.000	.00000	.32797	.05293	-.01190	-.00123	-.00008	-.00034	.29556	.15168	1.94655
20.300	20.000	.00000	.39055	.05215	-.01310	-.00151	-.00003	-.00085	.34916	.18258	1.91240
20.300	22.000	.00000	.48104	.05119	-.01567	-.00181	-.00007	.00151	.42280	.23508	1.79857
20.300	24.000	.00000	.60126	.05057	-.02014	-.00251	-.00019	.00229	.51824	.30902	1.67703
GRADIENT	.00000	.01174	-.00114	.00017	-.00012	-.00013	.00052	.01054	-.00127	.14311	

HE.T. 409 NAR ATP CRB(B1C1D1F1H1) (W1E1) (V1K1R1)

(ROS026) (20 NOV 72)

REFERENCE DATA

SREF = 9.3900 SQ.IN. XMRP = 3.8850 INCHES
 LREF = 5.9720 INCHES YMRP = .0000 INCHES
 BREF = 4.5300 INCHES ZMRP = .0000 INCHES
 SCALE = .0045 SCALE

PARAMETRIC DATA

BETA = -4.500 ELEVTR = .000
 AILRDN = .000 RUDDER = .000
 BDFLAP = .000

RUN NO. 26/0 RN/L = 4.30 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	-1.505	-4.46847	-.05490	.07425	-.01250	-.00016	.06687	.04048	-.05293	.07567	-.69953
20.300	.000	-4.47000	-.04020	.07253	-.01239	-.00001	.00734	.03931	-.04020	.07253	-.55425
20.300	2.006	-4.46727	-.01666	.06927	-.01216	-.00027	.00721	.03899	-.01928	.06864	-.28084
20.300	4.012	-4.45909	.00633	.06707	-.01208	-.00007	.00738	.03700	.00362	.06749	.05363
20.300	6.018	-4.44546	.03770	.06558	-.01178	.00067	.00745	.03572	.03061	.06917	.44259
20.300	8.024	-4.42841	.07398	.06383	-.01140	.00120	.00748	.03429	.06434	.07354	.87499
20.300	10.030	-4.40196	.11341	.06203	-.01135	.00165	.00765	.03300	.10087	.08063	1.24791
20.300	12.036	-4.37213	.15567	.06064	-.01145	.00199	.00781	.03181	.13961	.09177	1.52127
20.300	14.041	-4.33696	.20567	.05886	-.01184	.00239	.00802	.03106	.18524	.10700	1.73121
20.300	16.046	-4.29651	.26179	.05661	-.01220	.00262	.00812	.02966	.23595	.12677	1.86129
20.300	18.051	-4.25081	.32268	.05534	-.01301	.00306	.00790	.02897	.28965	.15260	1.89007
GRADIENT	.00172	.01152	-.00134	.00008	-.00000	-.00007	.00058	.01031	-.00152	.13737	

DATE 26 MAR 73

SOURCE DATA TABULATION, LARC TEST 22-409

PAGE 12

ME.T. 409 NAR ATP ORB(B1C1D1F1H1) (W1E1) (V1K1R1)

(ROS027) (20 NOV 72)

REFERENCE DATA

SREF = 9.3900 SQ.IN. XMRP = 3.6650 INCHES
 LREF = 5.9720 INCHES YMRP = .0000 INCHES
 BREF = 4.5300 INCHES ZMRP = .0000 INCHES
 SCALE = .0045 SCALE

PARAMETRIC DATA

BETA = -2.250 ELEVTR = .000
 AILRDN = .000 RUDDER = .000
 BDFLAP = .000

RUN NO. 27/0 RN/L = 4.30 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	16.013	-2.13982	.33185	.03165	-.01160	.00123	.00464	.00941	.29961	.15174	1.97454
20.300	20.014	-2.11424	.39581	.05027	-.01281	.00137	.00444	.00810	.35470	.18270	1.94147
20.300	23.016	-2.07105	.48412	.04888	-.01510	.00159	.00416	.00715	.42647	.23427	1.82044
20.300	26.017	-2.02219	.59781	.04693	-.01691	.00158	.00389	.00463	.51684	.30440	1.69725
20.300	28.018	-1.98652	.67548	.04590	-.02211	.00169	.00378	.00266	.57475	.35783	1.60622
20.300	30.019	-1.94843	.74220	.04437	-.02505	.00169	.00359	.00166	.62045	.40973	1.51428
20.300	33.020	-1.88686	.85390	.04226	-.03059	.00167	.00333	-.00054	.69295	.50075	1.38381
GRADIENT		.01678	.03497	-.00061	-.00125	.00003	-.00009	-.00067	.02656	.02315	-.04055

LRC 22HE-409, ATP ORBITER + EXTERNAL TANK (T1)

(ROS030) (27 NOV 72)

REFERENCE DATA

SREF = 9.3900 SQ.IN. XMRP = 3.6650 INCHES
 LREF = 5.9720 INCHES YMRP = .0000 INCHES
 BREF = 4.5300 INCHES ZMRP = .0000 INCHES
 SCALE = .0045 SCALE

PARAMETRIC DATA

BETA = .000 ELEVTR = .000
 AILRDN = 20.000 RUDDER = .000
 BDFLAP = .000

RUN NO. 30/0 RN/L = 4.30 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	CN	CAF	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	-15.000	.00000	-.46763	.26830	-.15914	.04237	.02242	-.00659	-.38226	.38019	-1.00543
20.300	-12.000	.00000	-.38804	.24827	-.11945	.03672	.01614	-.00573	-.32794	.32352	-1.01365
20.300	-9.000	.00000	-.33805	.22941	-.09039	.04260	.02274	-.00796	-.29801	.27947	-1.06634
20.300	-6.000	.00000	-.23109	.18695	-.07677	.02698	.01425	-.00618	-.21023	.21008	-1.00096
20.300	-3.000	.00000	-.14733	.15877	-.05643	.01740	.00878	-.00547	-.13882	.16627	-.83494
20.300	-1.000	.00000	-.10040	.14447	-.03651	.01382	.00742	-.00488	-.09787	.14620	-.65940
20.300	.000	.00000	-.07669	.13995	-.02253	.01250	.00659	-.00487	-.07669	.13995	-.54800
20.300	1.000	.00000	-.05898	.13825	-.00939	.01150	.00592	-.00584	-.06138	.13720	-.44738
20.300	3.000	.00000	-.02040	.13801	.00948	.00865	.00201	-.00548	-.02759	.13675	-.20176
20.300	6.000	.00000	.04042	.12183	.03133	.00442	-.00134	-.00580	.02746	.12538	.21903
20.300	9.000	.00000	.10091	.11625	.05592	.00313	-.00240	-.00621	.08148	.13060	.62390
20.300	12.000	.00000	.13251	.11525	.07661	.00271	-.00375	-.00774	.10565	.14028	.75311
20.300	15.000	.00000	.18220	.15817	.09449	.00278	-.01173	.00113	.13506	.19994	.67549
GRADIENT		.00000	.02111	-.00342	.01124	-.00143	-.00109	-.00005	.01851	-.00488	.10608

DATE 26 MAR 73

SOURCE DATA TABULATION, LARC TEST 22-409

PAGE 13

LRC 22ME-409, ATP ORBITER + EXTERNAL TANK (T1)

(ROS031) (27 NOV 72)

REFERENCE DATA

SREP = 9.3900 SQ.IN. XMRP = 3.8650 INCHES
 LREP = 5.9720 INCHES YMRP = .0000 INCHES
 BREP = 4.9300 INCHES ZMRP = .0000 INCHES
 SCALE = .0045 SCALE

PARAMETRIC DATA

BETA = .000 ELEVTR = .000
 AILRDN = .000 RUDDER = .000
 BOFLAP = .000

RUN NO. 31/0 RNL = 4.30 GRADIENT INTERVAL = -5.00/ 5.00

MACH	ALPHA	BETA	CN	CAP	CLM	CBL	CYN	CY	CL	CDF	L/DF
20.300	-15.000	.00000	-.35943	.21634	-.16820	.00522	.00050	-.00004	-.29119	.30200	-.96420
20.300	-12.000	.00000	-.29567	.20474	-.14377	.00455	.00045	-.00061	-.24664	.26174	-.94229
20.300	-9.000	.00000	-.23910	.18051	-.11753	.00495	.00134	-.00235	-.20792	.21569	-.96399
20.300	-6.000	.00000	-.16597	.15674	-.09439	.00284	.00060	-.00214	-.14867	.17323	-.85823
20.300	-3.000	.00000	-.10670	.13992	-.06733	.00168	.00018	-.00178	-.09924	.14532	-.68290
20.300	-1.000	.00000	-.06653	.12964	-.04519	.00117	.00070	-.00196	-.06425	.13078	-.49132
20.300	.000	.00000	-.04622	.12580	-.03003	.00089	.00115	-.00171	-.04622	.12580	-.36745
20.300	1.000	.00000	-.02826	.12827	-.01700	.00058	.00094	-.00260	-.03049	.12776	-.23866
20.300	3.000	.00000	.00291	.12938	.00358	.00056	-.00151	-.00365	-.00396	.12935	-.03063
20.300	6.000	.00000	.05290	.11831	.02843	.00016	-.00279	-.00391	.04024	.12319	.32663
20.300	9.000	.00000	.11134	.11444	.05368	-.00034	-.00344	-.00355	.09206	.13045	.70574
20.300	12.000	.00000	.14156	.11363	.07369	-.00057	-.00432	-.00758	.11484	.14058	.81686
20.300	15.000	.00000	.18406	.11246	.09596	-.00081	-.00467	-.00799	.14868	.15626	.95150
	GRADIENT	.00000	.01834	-.00165	.01205	-.00023	-.00024	-.00031	.01598	-.00255	.11047